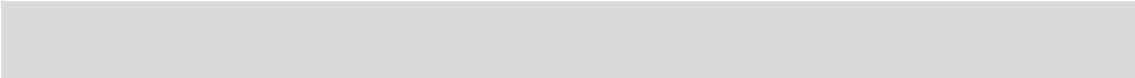


DELTA CITY WASTEWATER MASTER PLAN

76 North 200 West
Delta, UT 84624

March 2019

PREPARED BY:
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DELTA CITY WASTEWATER MASTER PLAN

March 2019

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EXECUTIVE SUMMARY

The Delta City Wastewater System serves an estimated population of 3,580 residents and approximately 1,041 connections, including approximately 908 residential, 105 commercial and 28 institutional connections.

The wastewater collection system is comprised of approximately 143,088 feet of sewer pipe, including approximately 42,936 feet of vitrified clay pipe, 14,227 feet of asbestos cement pipe, 21,717 feet of concrete pipe, and 52,478 feet of PVC pipe. It is estimated that the original parts of the system, primarily comprised of clay and asbestos cement pipe, are between 60 and 100 years old. Flow meter readings at the wastewater lagoons indicate that at times, the flow into the lagoons exceeds the total water usage on the system, indicating a significant level of infiltration and inflow into the existing collection system from groundwater and stormwater.

There are currently six lift stations operating in the collection system. Most of the wastewater in the system is pumped at least two times, and wastewater from some of the collection zones in the system is pumped three times before reaching the lagoons. Lift Station A and Lift Station C are currently in need of repair and rehabilitation.

A hydraulic model of the collection system was developed to analyze the capacity of the existing collection system under current and future peak loadings. The model indicated that the pipes in the system are generally sized with sufficient capacity, although there are isolated pipe segments that do not provide sufficient capacity to support current and future peak loadings or that suffer from negligible or negative slopes.

The wastewater treatment system is comprised of a series of nine lagoon cells that provide a total of 100 acres and over 144,000,000 gallons of lagoon capacity. The estimated lagoon area required to achieve a mass balance under current system flows is approximately 38 acres, and the estimated area required to support the estimated 20-year projected system flows is approximately 47 acres.

Recommended system improvements in the Capital Improvement Plan are outlined by geographic location based on the lift station zoning. The pre-construction recommendation is to have a video inspection of the entire collection system completed. Improvements to the system should be completed in order of priority based on the results and observations of the video inspection. Improvements to Zone A include bypassing Lift Station A and replacing approximately 43,200 feet of clay pipe, asbestos cement pipe, and concrete pipes and manholes. Zone B and C improvements include replacing the force main line between Lift Station B and the lagoons, upgrading Lift Station C, and include replacing approximately 17,860 feet of clay pipe and asbestos cement pipe and associated manholes with these zones. Improvements to Zones D and E consist of replacing approximately 16,725 feet of concrete pipe and associated manholes. Zone F improvements include upgrading Lift Station F and installing a new force main line from Lift Station F to connect to the new force main interceptor from Lift Station B. Actual quantities and prioritization of pipe replacement will be determined based on the results of the sewer video inspection.

The Engineer's Opinion of Probable Cost for the completed improvements is approximately \$18,882,336. The estimated cost presented in this report represent present value cost assuming the recommended projects are constructed at once. If the City chooses to phase the projects over several years, it is anticipated the actual cost of improvements will be higher due to the loss of project efficiencies and rising construction costs.

1.0 INTRODUCTION

1.1 PURPOSE

The purpose of this Wastewater Master Plan is to evaluate the existing sewer collection and treatment systems. The master plan will identify recommended improvements to resolve existing deficiencies, project future system loadings based on the projected growth, identify system improvements required to support future growth, and develop a capital improvement plan that outlines the potential costs and recommended schedule for implementing recommended improvements over the 20-year planning period.

2.0 POPULATION ANALYSIS AND PROJECTED GROWTH

Delta City has grown at a modest rate throughout its history. The average annual growth rate, with major fluctuations, for the past century from 1910 to 2010 has been 2.03%. The current estimated population of Delta is 3,580.

While estimated growth rates are susceptible to change, it is necessary to project a community's growth over the duration of the planning period in order to estimate the increased demands and loadings on the community's infrastructure. Required improvements and expansions can then be planned for in a responsible and systematic manner. In developing a projected growth rate for this study, projections from the Utah Governor's Office of Management and Budget (GOMB) and data from historical Census estimates were reviewed. The GOMB projects an average annual growth rate of 0.38% for Delta City between the years 2020 and 2040. Census estimates between 2000 and 2016 indicate an actual average growth rate of 0.56% during this period. For the purposes of this study, a projected average annual growth rate of 1.00% will be used for the 20-year planning period. Table 2.1 shows the projected population growth for this period.

Table 2.1: Delta City 20 Year Population Growth Projection

| Year | Projected Population |
|-------------|-----------------------------|
| 2018 | 3,580 |
| 2023 | 3,762 |
| 2028 | 3,954 |
| 2033 | 4,156 |
| 2038 | 4,368 |

It is projected that most of the growth during the planning period will occur within the existing sewer service area and will be serviced by the existing sewer collection system.

3.0 SYSTEM USER ANALYSIS

3.1 CURRENT WASTEWATER CONNECTIONS AND ERC’S

In this plan, reference will be made to Equivalent Residential Connections (ERC’s). One ERC is defined as the amount of wastewater discharged to the system by an average single-family residential connection. ERC’s can be used to compare the wastewater flows produced by commercial, industrial, and institutional entities to a single residential connection. A detailed explanation for the determination of ERC equivalent values for the various connection types is included in Appendix A.

There are currently 1,041 sewer connections on the Delta collection system. Table 3.1 shows the current connection types and ERC equivalents for the Delta System.

Table 3.1: Delta City Connections by Type and ERC Multipliers

| EXISTING | | | |
|---------------------------------|-------------|----------------|-------------|
| | Connections | ERC/Connection | ERC's |
| Residential | 908 | 1 | 908 |
| Commercial | 105 | 1.5 | 158 |
| Government/Institutional | 28 | 5.0 | 140 |
| Total | 1041 | | 1206 |

The average number of residents per ERC is estimated by dividing the estimated 2018 population of 3,580 by the number of residential connections, which gives a rounded average of 4 residents per ERC.

3.2 PROJECTED WASTEWATER CONNECTIONS AND ERC’S

The number of wastewater ERC’s expected at the end of the 20-year planning period can be calculated using the compound interest formula and inserting the projected growth rate of 1.00% and the existing number of wastewater ERC’s.

The projected number of residential ERC’s for the planning period is calculated with the compound interest formula as follows:

$$F = ERC \times (1 + r)^t$$

$$F = 1,206 \text{ ERCs} \times (1 + 0.01)^{20} = 1,470 \text{ ERC}$$

Table 3.2: 20-Year Projected ERC’s shows the projected number of ERC’s for each category.

Table 3.2: 20-Year Projected Connections by Type and ERC Multipliers

| FUTURE (20 YR) | | | |
|---------------------------------|-------------|----------------|-------------|
| | Connections | ERC/Connection | ERC's |
| Residential | 1108 | 1 | 1108 |
| Commercial | 128 | 1.5 | 192 |
| Government/Institutional | 34 | 5.0 | 170 |
| Total | 1270 | | 1470 |

4.0 FLOW DATA EVALUATION AND FLOW CRITERIA

4.1 CURRENT CONDITIONS

Delta City measures the influent to the sewer lagoons to document the actual flows into the lagoons and to estimate the system flows in the collection system. The monthly totals and daily averages for 2017 are shown in Table 4.1.

Table 4.1: Delta City Collection System Flows for 2017

| 2017 | Flows (gal) | Days/Month | Avg Gal/Day | Avg gpcpd |
|--------------|--------------------|-------------------|--------------------|------------------|
| Jan | 12,830,000 | 31 | 413,870.97 | 116.78 |
| Feb | 12,830,000 | 28 | 458,214.29 | 129.29 |
| Mar | 13,554,000 | 31 | 437,225.81 | 123.37 |
| Apr | 9,880,000 | 30 | 329,333.33 | 92.92 |
| May | 9,301,000 | 31 | 300,032.26 | 84.66 |
| Jun | 8,072,000 | 30 | 269,066.67 | 75.92 |
| Jul | 7,773,000 | 31 | 250,741.94 | 70.75 |
| Aug | 7,956,000 | 31 | 256,645.16 | 72.41 |
| Sep | 8,091,000 | 30 | 269,700.00 | 76.10 |
| Oct | 7,636,000 | 31 | 246,322.58 | 69.50 |
| Nov | 7,436,000 | 30 | 247,866.67 | 69.94 |
| Dec | 8,369,000 | 31 | 269,967.74 | 76.17 |
| Total | 113,728,000 | | Average: | 88.15 |

Based on the growth rate discussed in Section 2.0, the estimated population in 2017 was 3,544 residents. Using this estimated population and the measured flow data, Delta City's annual average per capita flow rate was calculated to be 88.15 gallons per capita per day (gpcpd), which includes groundwater infiltration and surface water inflows. Utah Code R317-3-2 provides design requirements for new sewers, including the average daily per capita flow rate of 100 gallons per capita per day (gpcpd). With the current estimate of 4 residents per ERC, the average per ERC flow rate is 400 gallons per day.

Section R317-3-2 also provides design flows of 400 gpcpd for sizing laterals and collector sewers, and 250 gpcpd for sizing interceptors and outfall sewers. These values equate to 1,200 gallons per ERC per day for laterals and collectors, and 750 gallons per ERC per day for interceptors and outfall sewers.

4.2 FUTURE CONDITIONS

Based on the population projection outlined in Section 3.0, the estimated population will be 4,368 residents in the year 2038. Using an annual average daily flow of 100 gpcpd, the assumed average daily flow for the 20-year design period is 0.437 MGD, or roughly 303 gpm. Peaking flows of 1,200 gallons per ERC per day for laterals and collectors, and 750 gallons per ERC per day for interceptors and outfall sewers still apply with the projected 20-year condition.

5.0 COLLECTION SYSTEM

The Delta City collection system piping is comprised of laterals, collector sewers, interceptor sewers, and the outfall sewer line. Each segment of piping is connected by manholes, and lower elevation areas of the system are lifted to the interceptors and outfall lines using lift stations and force mains. Brief descriptions of these elements are provided as follows:

Lateral – A sewer lateral line is the pipe that connects a private property to the publicly owned sewer line. The portion of the sewer lateral from the building to the property line is typically owned and maintained by the property owner, while the section from the property line to the main line is typically owned and maintained by the utility provider. A cleanout is typically installed at or near the property line. The typical residential sewer lateral is 4” in diameter.

Collector – A collector sewer line is the line to which the sewer laterals are connected. Also referred to as a branch line. The collector carries the wastewater from the laterals to the interceptor lines.

Interceptor & Outfall – Interceptor and outfall lines may be used somewhat interchangeably. The interceptor line(s) receive wastewater from one or many collector lines and carry the wastewater to a treatment plant. The outfall is described as the discharge point of the collection system to the treatment system.

Lift Station – Lift stations, also called pump stations, are used for pumping wastewater from a lower to a higher elevation, particularly where the elevation of the source is not sufficient for gravity flow into the downstream sections of the collection system.

5.1 PIPELINES

The Delta City collection system consists of approximately 131,358 linear feet of gravity sewer line, 11,730 linear feet of pressurized sewer line, and 345 manholes that are 4 feet in diameter and vary from 4 to 14 feet in depth. The gravity sewer is comprised of sections of vitrified clay pipe (VCP), asbestos cement pipe (transite), concrete pipe, and PVC pipe ranging in diameter from 6” to 15”. A summary of the pipe types and sizes is provided in Table 5.1.1 and Table 5.1.2. See Exhibit 1 maps for piping sizes and types.

Table 5.1.1: Summary of Gravity Pipe Material

| Summary of Gravity Pipe Material | | |
|---|---------------------|--------------------------|
| Material | Total length | % of total system |
| Clay Tile | 42,936 | 33% |
| Concrete | 21,717 | 17% |
| Transite | 14,227 | 11% |
| PVC | 52,478 | 40% |
| % Total | 131,358 | 100% |

Table 5.1.2: Summary of Gravity Pipe Sizes

| Summary of Gravity Pipe Sizes | | |
|--------------------------------------|---------------------|--------------------------|
| Pipe Diameter (inches) | Total length | % of total system |
| 6 | 555 | 0% |
| 8 | 101,392 | 77% |
| 10 | 20,139 | 15% |
| 12 | 6,856 | 5% |
| 15 | 2,416 | 2% |
| % Total | 131,358 | 100% |

Aging collection system infrastructure should also be a consideration when assessing the condition and capacity of the system to support current and future growth. Table 5.1.3 provides a summary of estimated pipe age for portions of the collection system for which dated construction drawings were available.

Table 5.1.3: Summary of Gravity Pipe Aging

| Summary of Pipe Aging | | |
|--------------------------------|---------------------|--------------------------|
| Pipe Type & Age | Total length | % of total system |
| PVC: 0-30 Years | 22,890 | 17% |
| Concrete: 30-50 Years | 12,761 | 10% |
| Clay Tile, Transite: 60+ Years | 39,456 | 30% |
| Total | 75,107 | 57% |

5.1.1 System General History

It is generally understood that groundwater drains were installed throughout the original sections of Delta City prior to the establishment of the sanitary system. The drains were installed to drain groundwater and irrigation water from the City to the river. The ground drain system was comprised of perforated or open joint pipe that encouraged inflow from the ground. It is believed that the original sanitary collection was through these existing drainage pipes, allowing the sanitary sewage to collect with the groundwater and irrigation water and empty into the river. Only after the construction of the lagoons (original date unknown) was the sewage diverted to the lagoons instead of the river.

It is possible that the older portions of the existing collection system are comprised of the original groundwater drain system. Lift stations and force main pipelines were introduced in order to divert the wastewater to the lagoon. As the City grew and additional sanitary connections were needed, additional pipelines of differing pipe types were added to the system.

The sewer flow data can be compared against the metered culinary water winter usage to estimate the amount of groundwater infiltration and stormwater inflow into the collection system. Table 5.1.4 shows a comparison of the metered culinary water usage with the measured sewer flows for December 2016 – March 2017, and December 2017.

Table 5.1.4: Delta City Culinary Winter Usage Comparison with Sewer Flows

| 20016-2017 | Water Usage (gal) | WW Flows | Difference |
|-------------------|--------------------------|-----------------|-------------------|
| Dec (2016) | 9,339,000 | 9,831,000 | -492,000.00 |
| Jan | 12,102,000 | 12,830,000 | -728,000.00 |
| Feb | 10,246,000 | 12,830,000 | -2,584,000.00 |
| Mar | 12,923,000 | 13,554,000 | -631,000.00 |
| Dec (2017) | 10,078,000 | 8,369,000 | 1,709,000.00 |

The sewer collection system flows were moderately to significantly higher than the culinary water usage between December 2016 and March 2017, indicating a high amount of infiltration/inflow during this period. It is interesting to note that the sewer flows were approximately 1,709,000 gallons less than the culinary water usage in December 2017, which may indicate that the infiltration or inflows were no longer occurring due to dry conditions or other factors. It is also noted that Delta City performed emergency sewer lining procedures on failing portions of the sewer main that runs under Main Street in the fall of 2017, which may be a contributing factor to the reduction in sewer flows after that period. Another possible contributing factor is the extremely dry early winter that Delta experienced in winter of 2017-2018, which may have influenced the groundwater table and the surface water runoffs.

5.1.2 Existing Gravity Pipe Materials

As mentioned in Section 5.1, the Delta City sanitary collection system is comprised of various materials. Most of the known system has been in the ground for more than 60 years. This older pipe consists of materials such as vitrified clay pipe, concrete pipe, and transite. Each of the different pipe materials have their own strengths and weaknesses as summarized below, which can have an impact on the life expectancy of the pipeline.

- **Vitrified Clay Pipe (VCP)**
 - VCP is brittle and will fail within a few years if not installed and bedded correctly, or in conditions of shifting soil.
 - VCP is susceptible to root intrusion at the joints and service connections and pipe collapses when the integrity of the pipe is compromised.
 - The life expectancy of VCP when installed correctly, is approximately 50 years.
- **Concrete Pipe**
 - Concrete pipe is susceptible to corrosion from hydrogen sulfide gas which is commonly generated in collection system pipes. Corrosion can be as high as one-inch of thickness lost per year in highly corrosive applications.
 - Corrosion typically occurs in the top and sides of the pipe that are not submerged, leaving “topless” sections of pipe. In these situations, cavities typically form in the surrounding soils and the pipe is susceptible to collapse.
 - The life expectancy of concrete pipe is less than 50 years in sanitary sewer collection systems.
- **Transite**
 - Transite is an asbestos-cement product, where the asbestos fiber was used to provide tensile strength.
 - The use of transite pipe was phased out in the 1970’s due to the carcinogenic asbestos fibers.
 - Transite pipe is obsolete and difficult to repair due to the lack of available fittings and couplings.
 - The life expectancy of transite pipe is approximately 50 years.

5.1.3 Recommended Pipeline Improvements

The pipeline material's age and the condition of the pipes in the existing system play a substantial role in the infiltration experienced in the system. It is recommended that the City consider replacing all VCP and transite pipe with PVC SDR 35. It is also recommended that the City complete a video inspection of the entire Delta Sanitary System to identify locations of failing concrete pipes. Failing pipelines should be replaced with PVC sewer pipe, which is the current standard for sanitary sewer pipe.

5.2 MANHOLES

As mentioned above, there are an estimated 345 manholes in Delta City's existing collection system. The manholes are typically 4 feet in diameter and vary in depth from 2.75 feet to 14 feet deep, although there are a few larger and deeper manholes in the system.

There are approximately 45 locations where the pipeline ends without a known manhole or cleanout to access the line. Manholes are needed for inspection, cleaning, and removal of obstructions in the sewer line. They also help with the ventilation of the sewer system, reducing the impact of H₂S gas.

5.2.1 Recommended Manhole Improvements

It is recommended that pipeline ends without sewer access have manholes installed. It is also recommended that manholes be replaced in the locations of pipeline replacement.

5.3 LIFT STATIONS

Delta City has six lift stations in the wastewater collection system. The lift stations and associated collection zones are shown on Exhibit 5. A description of each lift station is provided as follows.

5.3.1 Lift Station A

Lift Station A is located on the southeast corner of 400 South and 300 West. This lift station utilizes two 5 hp submersible pumps.

Site visit observations include:

- The pump rails were determined to be in adequate condition, but there was severe concrete deterioration within the wet well.
- It was reported that the gravity lines downstream from Lift Station A are in poor condition.
- Valves may need to be exercised, blasted, and recoated.

Recommended Lift Station A Improvements:

Currently, all the wastewater coming from Zone A meets at the southeast corner of 400 South and 300 West (Lift Station A), where it is pumped east into Zone B. With the redesign of approximately 1,600 linear feet of existing pipeline between Lift Station A and Lift Station F, it appears to be feasible to bypass Lift Station A and redirect the flows to Lift Station F.

It is recommended that the City eliminate Lift Station A to reduce system operation and maintenance costs and provide additional system efficiencies by reducing the number of times the wastewater from Zone A is pumped.

5.3.2 Lift Station B

Lift Station B is located south of 400 South, at 300 East, and serves approximately two-thirds of the city. The station includes two 20 hp submersible pumps and a bypass wet well.



Figure 1: Lift Station A

Station B was observed to be in good operational condition with the exception of the force main between Station B and the lagoons, which has experienced recent failures. The City recently installed a new gravity line to the east of Station B to allow Station B flows to be diverted to Station E in the event of future force main failure between Station B and the lagoons.

Recommended Lift Station B Improvements:

Due to the observed problems, it is recommended this force main should be replaced between Lift Station B and the lagoons.

5.3.3 Lift Station C

Lift Station C is located at 200 E and Main Street on the north side of the intersection. Lift Station C currently has two submersible pumps of differing size, 3 hp and 5 hp.

Site visit observations included the following items:

- The flanged ductile fittings are significantly corroded.
- Access stairs significantly corroded.
- The valve vault is paved over and inaccessible.
- The depth probe is not installed vertically.
- There is no backup wet well, or alternative force main under Hwy 6.



Figure 2: Lift Station C

It has been reported that this pump station can't keep up when the West Millard Swimming Pool is drained.

Recommended Lift Station C Improvements:

It is recommended that the City consider a full replacement of the lift station and valve vault. The new lift station should be sized to meet the projected demands of the zone it is serving, including the West Millard Swimming Pool. It is also recommended that the City install a complete backup well with backup pump and controls. The City may consider relocating the station to the south side of the intersection if a feasible location can be identified. Otherwise, a backup force main should be directionally drilled under Hwy 6.

5.3.4 Lift Station D

Lift Station D, located just east of the corner of 200 North and 420 East, consists of two 5 horsepower submersible pumps. The pumps are run on single-phase power and reside in a newly rebuilt wet well. Lift Station D was rebuilt approximately 5 years ago and is in good operating condition.

5.3.5 Lift Station E

Lift Station E is located in the southeast end of town, at approximately 1500 East and 750 South. The lift station consists of two 10 horsepower pumps.

Site visit observations included:

- The conduit for the control wiring and motor conductors has been broken outside the building, exposing wires.
- The ductile iron fittings in the wet well show corrosion
- The lift station has a simplex backup; however, there is no back up pump presently installed.



Figure 3: Lift Station E

Recommended Lift Station E Improvements:

It is recommended that the City keep a backup pump available for use as needed. Station valves should be exercised and blasted and recoated if necessary, and maintenance items should be addressed.

5.3.6 Lift Station F

Located at the southwest corner of town at approximately 320 W Shadow Run Road, Lift Station F consists of two 5 hp pumps. Because of the location and demand, the pump only runs a couple of days a week.

Site visit observations included:

- The pump rails are in good condition.
- The original controls and generator are in place.
- The flanged ductile iron pipe within the wet well is corroding.
- There is some differential settling evident under the concrete surrounding the wet well.

Recommended Lift Station F Improvements:

If the City decides to bypass and eliminate Station A, Station F will need to be replaced with an upgraded lift station and new force main to connect with the new Lift Station B force main.

5.3.7 General Recommendations for All Stations

A detailed performance analysis of each lift station is recommended in order to identify actual pumping capacity and efficiencies, and to identify and prioritize recommendations for repairs or replacement of lift station components.

5.3.8 Additional Options

In addition to the recommendations stated above, there are alternatives available to the City that they may chose to pursue in the future.

- **Bypass Lift Station B.** Lift Station B currently serves approximately two-thirds of the city; however, if the City chooses to eliminate Lift Station A and bypass the flows to Zone F, the demand at Lift Station B would decrease considerably. With that in consideration, a redesign of approximately 7,100 linear feet of sanitary pipeline to the south of Lift Station B and then east to Lift Station E would enable the bypass of Station B. The flow from Zone B would be redirected to Zone E, then pumped through Lift Station E to the treatment lagoons.

If the City chooses to eliminate Lift Station B and redirect Zone B to Lift Station E, Station E will need to be upgraded to accommodate the additional flows. It is also recommended that the force main from Station E to the lagoons be replaced at the same time.

- **Bypass Lift Station C and D.** It may also be possible to eliminate Station C and Station D by installing deep interceptor lines to carry the flow to Station B or Station E. A threshold survey would be required in these zones to determine the actual required depth of the deep interceptors and possible reconfiguration of the collection zones. The wet wells at Station B and Station E would also need to be lowered to accommodate the deeper lines.

6.0 COLLECTION SYSTEM ANALYSIS

6.1 COLLECTION SYSTEM MODEL

The existing and future Delta City wastewater collection systems were evaluated using H2OMap Sewer, a hydraulic modeling computer program. The H2OMap Sewer model is a mathematical representation of the pipes, manholes, and wastewater flows found in the wastewater collection system. The use of the collection system model allows for different scenarios to be developed along with a means to check how changes to one portion of the system will affect the system as a whole. For example, potential upgrades can be modeled prior to construction to determine if they will provide the adequate capacity or not, which can provide major cost savings to the City when upgrades are needed. Using a collection system model also provides the ability to determine the effect that a subdivision or major customer may pose on system and what upgrades may be necessary for that user. Essentially, the system model allows the City to be proactive rather than reactive to changes in the system.

The model was created after survey data was collected on the existing system. Manhole rim elevations were collected, then the lids were lifted, and a measurement taken from the rim to the flow line. Pipe inverts were calculated by subtracting the manhole depth from the rim elevations.

In Section 5.2—Manholes, it discusses that there are 45 locations where the existing pipeline ends without access to a known manhole or cleanout. In order to run the H2OMap Sewer model, manholes were added in the model at these locations. It was assumed that the slope of the existing pipe is the minimum of 0.0033 ft/ft.

The existing lift stations were then added to the system, based on the information from the site visit. Pump capacity and efficiencies were estimated in the absence of actual model specific pump specifications.

6.1.1 Lift Station Zoning

The Delta City sanitary system has six lift stations, which assist in conveying the wastewater to the treatment lagoons southeast of the city. The current condition of each of the lift stations was discussed in Section 5.3 of this report, along with a discussion of recommendations for improvements.

The purpose of this section is to better identify the portion of the system that feeds the different lift stations. To better illustrate the zoning, please refer to Figure 6.1 – Delta City Sewer Zoning and the zoning maps provided in Exhibit 3. These zoning sections were estimated based on the slope of pipes and direction of flow. Figure 6.1 also illustrates the locations of the lift stations with regard to the entire system. It is interesting to note that wastewater from Zone D is pumped three times before it reaches the lagoons (Station D, Station C, Station B).

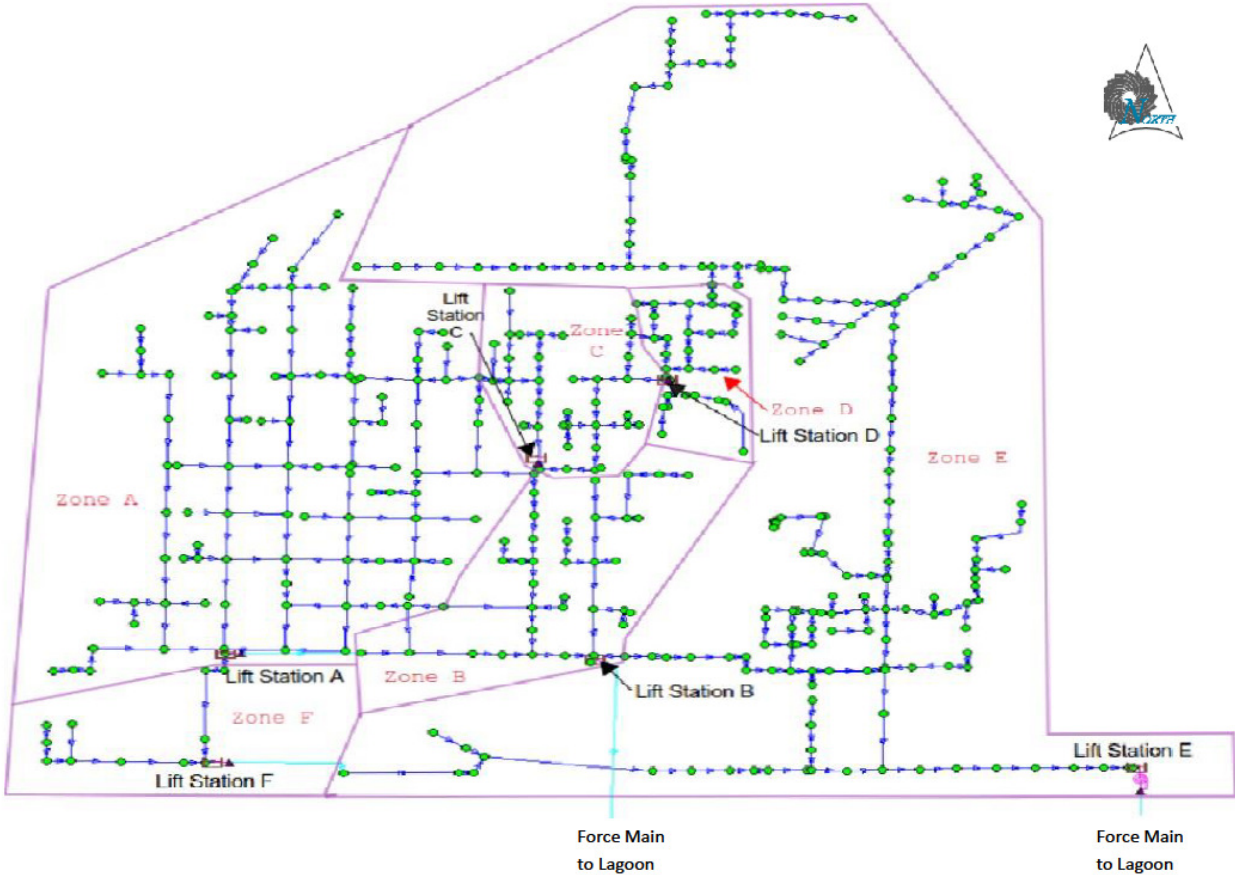


Figure 6.1: Delta City Sewer Zoning

6.1.2 System Slopes

As mentioned above, survey data for the manhole rim elevations were collected and pipe inverts obtained by measuring down from the existing manhole rims. It was through this method that existing pipe slopes were estimated. Upon reviewing the system as a whole, it was noted that the slopes of the pipes throughout the entire system are very minimal, and in some segments, negative slopes were observed. The pipeline slopes vary from 0.00% to 3.60%, with the majority of the system experiencing slopes between 0.20% and 0.50%.

Utah Code R317-3-2 provides a table with minimum slopes based on pipe size to achieve the required minimum velocity of 2 feet per second when flowing full. These minimum slopes are shown in Table 6.1 below. It is important to note that the slopes listed below are minimum slopes; slopes greater than these are desirable.

Table 6.1: Minimum Sewer Slopes by Pipe Size

| Sewer Size inch | Minimum Slope |
|--------------------|------------------|
| 8 | 0.334% |
| 10 | 0.248% |
| 12 | 0.194% |
| 15 | 0.144% |
| 18 | 0.113% |
| 21 | 0.092% |
| 24 | 0.077% |
| 27 | 0.066% |

6.1.3 System Depth

As mentioned above, survey data for the manhole rim elevations were collected and pipe inverts obtained by measuring down from the existing manhole rims. These distances varied in depth from 2.75 feet to 15 feet deep, with the majority of the system having an invert between six and eleven feet below the existing manhole rim.

6.2 EXISTING COLLECTION SYSTEM ANALYSIS

In order to determine what portions of the system are in need of improvement, the software program H2OMap Sewer was used to model the existing system for current needs. The system was modeled with the current design flows as described in Section 4.1—Current Flow Criteria, which was estimated to about 0.358 MGD, or an average flowrate of 248 gpm. The existing flow was applied to the system based on a visual estimation of loading conditions by attempting to estimate the number of connections that feed into each collector. The outlet flow of the model was then compared to the estimated design flow rate to verify the sum of the loadings applied to the individual manholes equaled the total design flow. As previously mentioned, a peaking factor of four (4.0) for the collector pipelines and two and a half (2.5) for the interceptor pipelines was applied to the system load, per State guidelines.

While analyzing the model for the existing wastewater system, there were ten locations that were identified to have negative slopes and another twelve segments with virtually no slope.

The results of the existing system are located in Appendix B, as Model Scenario 1A and Model Scenario 1B. Model Scenario 1A displays the results of the existing wastewater system with the peaking factor of 2.5 for interceptor pipelines. Model Scenario 1B displays the results of the existing wastewater system with a peaking factor of 4.0. The data highlighted in red specify locations where either the slope of the pipe was in question or the capacity exceeded 90%.

According to the results shown on Model Scenario 1A and 1B, there are three segments of collector pipe and two segments of interceptor pipe that are at or close to maximum capacity, and approximately ten pipe segments that may be installed with negligible or negative slopes. These areas are shown in Exhibit 4 for reference.

6.3 20-YEAR ANTICIPATED COLLECTION SYSTEM ANALYSIS

The system was also modeled for the 20-year anticipated flow conditions. In modeling the 20-year projection, it was assumed that the majority of the growth would occur within the existing City limits, with additional growth assumed at the edges of town for a more conservative approach. By applying the increase throughout, the model tests the system to determine if it is adequate for the projected future growth.

The estimated design flow rate in 2038 is 0.437 MGD, or roughly 303.5 gpm. Peaking flows of 1,200 gallons per ERC per day for laterals and collectors, and 750 gallons per ERC per day for interceptors and outfall sewers were applied as discussed in Section 4.0.

After running the model with the 20-year anticipated demands, several interceptor and collector pipes were identified as having capacity or slope deficiencies. Model Scenario 2A and Model Scenario 2B in Appendix B reflect the results of the H2OMap Sewer model using the 20-year projected flow rates with the existing collection system. The data highlighted in red indicates locations where either the slope of the pipe was in question or the capacity exceeded 90%. These areas are shown in Exhibit 4 for reference.

6.4. RECOMMENDATIONS

Reviewing the elemental data for the existing sewer system, there were ten locations that were identified to have negative slopes and another twelve segments with no substantial slope.

The hydraulic model identified two locations as being loaded above 100% of capacity under current day flows, and another four locations as being loaded above 100% capacity under 20-year projected flows. To be loaded above the available capacity indicates that these sections of pipe would become pressurized under these peak demands that were used to model the system. These segments of pipe are portions of the interceptor pipes just upstream from Lift Station E and Lift Station B. If the City chooses to redesign the system to eliminate Lift Station B (see Section 6.1.4.2), the capacity problems experienced in these locations can be addressed as part of that project.

7.0 TREATMENT SYSTEM

The Delta City wastewater treatment system is comprised of a series of total containment lagoons located southeast of Delta (approximately 2000 East and 1500 South). The lagoon layout is shown in Exhibit 2. As illustrated on the lagoon outline, the lagoon system includes nine separate cells. The different cells are cycled in and out of use in a rotation. For example, Cells 1A and 2A were recently taken out of the system, allowing them to dry. In turn, Cell 1 has recently started receiving wastewater and is currently at three-fourths its capacity and rising. It is assumed that once capacity in Cell 1 is reached, the City will cycle in another of the nine cells.

The existing lagoon system is total containment, meaning that it does not discharge to a body of water or the surrounding land. As such, no discharge permit or treatment limits are currently required for the lagoons. It is understood that the lagoons were built in the mid-1980’s using a clay liner to control infiltration. The clay liner in dry cells could potentially dry out and crack; therefore, the City should routinely check the liner condition in the dry cells prior to returning wastewater to them. If the liner cracks, the cells will allow excess leakage and will not meet standards.

Table 7.1 is a summary analysis of the existing lagoon system.

Table 7.1: Lagoon Analysis Summary

| | Total Surface Area (Acres) | Total Lagoon Area (Sq Ft) | Top of Dike Elevation | High Water Elevation | Bottom Elevation | Total Depth (ft) | Max Water Depth (ft) | Volume (gal) |
|--------------|----------------------------|---------------------------|-----------------------|----------------------|------------------|------------------|----------------------|--------------------|
| Cell 1 | 20.20 | 878,158 | 4,622.60 | 4,619.60 | 4,616.60 | 6.00 | 3.00 | 18,583,657 |
| Cell 2 | 9.00 | 388,714 | 4,622.00 | 4,619.00 | 4,614.00 | 8.00 | 5.00 | 13,026,254 |
| Cell 3 | 9.00 | 390,968 | 4,622.00 | 4,619.00 | 4,614.00 | 8.00 | 5.00 | 13,099,904 |
| Cell 4 | 6.90 | 299,615 | 4,621.70 | 4,618.70 | 4,613.70 | 8.00 | 5.00 | 9,034,972 |
| Cell 5 | 8.90 | 385,044 | 4,621.40 | 4,618.40 | 4,613.40 | 8.00 | 5.00 | 12,882,245 |
| Cell 6 | 9.00 | 389,188 | 4,621.40 | 4,618.40 | 4,613.40 | 8.00 | 5.00 | 13,030,761 |
| Cell 1A | 10.30 | 447,399 | 4,621.90 | 4,618.90 | 4,612.90 | 9.00 | 6.00 | 17,682,436 |
| Cell 2A | 13.40 | 581,326 | 4,621.85 | 4,618.85 | 4,612.85 | 9.00 | 6.00 | 23,549,799 |
| Cell 3A | 13.30 | 578,269 | 4,621.80 | 4,618.80 | 4,612.80 | 9.00 | 6.00 | 23,473,134 |
| TOTAL | 100.00 | | | | | | | 144,363,161 |

7.1 HYDRAULIC BALANCE

The calculations of the required lagoon area (A) is based on the water balance calculation: Water In = Water Out. Water entering the lagoons comes through two means: inflow from the City and precipitation. The water leaving the lagoons does so by percolation and evaporation. The annual water balance equation is as follows:

$$\text{Annual Inflow} + \text{Precipitation (A)} = \text{Percolation (A)} + \text{Evaporation (A)}$$

Lagoons losses due to percolation into the ground are calculated with the formula $Q=KiA$ where:

- Q = flow (inch/day/unit area)
- K = Permeability Constant (inches/day)
- i = Hydraulic gradient (water depth/liner thickness)
- A = Area (acres)

7.1.1 *Current Hydraulic Balance*

Based on the current population of 3,580 the water balance equation was calculated to determine the necessary lagoon area for treatment. The maximum hydraulic conductivity of the lagoon bottom as set by the Department of Water Quality shall not exceed 1.0×10^{-6} , which equates to a permeability constant of 0.034 inches per day.

Therefore, the percolation into the ground is related to the lagoon area by the following:

$$Q = KiA$$

$$Q = 0.034 \times 6 \times A = 0.204A$$

Annual precipitation was based off the Delta, Utah monthly climate summary, with a period of record between 1938-2005. Pan evaporation data was gathered from the Western Regional Climate Center for Milford, Utah, with a period of record between 1906-2005. The design parameters for the water balance equation are as follows:

- Annual Precipitation (ft/yr) = 0.66
- Annual Percolation @ .204 in/day (ft/yr) = 6.21
- Annual Evaporation (ft/yr) = 4.89
- Annual Inflow (gal/yr) = 130,670,000
- Annual Inflow (Ac-ft/yr) = 401

Using the water balance formula mentioned above, the required lagoon area (A) for the current system can be determined as follows:

$$\text{Annual Inflow} + \text{Precipitation}(A) = \text{Percolation}(A) + \text{Evaporation}(A)$$

$$\frac{401 \text{ ac} - \text{ft}}{\text{year}} + \frac{0.66 \text{ ft}(A)}{\text{year}} = \frac{6.21 \text{ ft}(A)}{\text{year}} + \frac{4.89 \text{ ft}(A)}{\text{year}}$$

$$\frac{401 \text{ ac} - \text{ft}}{\text{year}} = \frac{-0.66 \text{ ft}(A)}{\text{year}} + \frac{6.21 \text{ ft}(A)}{\text{year}} + \frac{4.89 \text{ ft}(A)}{\text{year}}$$

$$\frac{401 \text{ ac} - \text{ft}}{\text{year}} = \frac{10.44 \text{ ft}(A)}{\text{year}}$$

$$A = 38.41 \text{ acres}$$

Based on the current demands put on the existing sanitary system, the City currently requires lagoon surface area of at least 38.41 acres to properly treat the wastewater. The existing treatment lagoon system has an excess capacity for the City's current needs.

7.1.2 *Projected Hydraulic Balance*

The 20-year projected population of Delta City was estimated at 4,368. The design parameters for the water balance equation as described in Section 7.1.1 are as follows for the 20-year projected influent:

- Annual Precipitation (ft/yr) = 0.66
- Annual Percolation @ .204 in/day (ft/yr) = 6.21
- Annual Evaporation (ft/yr) = 4.89
- Annual Inflow (gal/yr) = 159,432,000
- Annual Inflow (Ac-ft/yr) = 489.28

Using the water balance formula mentioned above, the required lagoon area (A) for the current system can be determined as follows:

$$\text{Annual Inflow} + \text{Precipitation}(A) = \text{Percolation}(A) + \text{Evaporation}(A)$$

$$\frac{489.28 \text{ ac} - ft}{\text{year}} + \frac{0.66 \text{ ft}(A)}{\text{year}} = \frac{6.21 \text{ ft}(A)}{\text{year}} + \frac{4.89 \text{ ft}(A)}{\text{year}}$$

$$\frac{489.28 \text{ ac} - ft}{\text{year}} = \frac{-0.66 \text{ ft}(A)}{\text{year}} + \frac{6.21 \text{ ft}(A)}{\text{year}} + \frac{4.89 \text{ ft}(A)}{\text{year}}$$

$$\frac{489.28 \text{ ac} - ft}{\text{year}} = \frac{10.44 \text{ ft}(A)}{\text{year}}$$

$$A = 46.87 \text{ acres}$$

The projected system should require a lagoon surface area of at least 46.87 acres to provide the necessary volume capacity. As mentioned in Section 7.0, the existing lagoon has an approximate total surface area of 100 acres. Based on the parameters mentioned above, the existing treatment lagoons are adequately sized for the 20-year planning period.

7.2 STRUCTURE AND FLUME

The influent currently enters the treatment lagoon through a ramp flume and headworks structure. It was noted during the April 2018 field visit that there was build up at the flume that is potentially affecting the accuracy of the measurements. It is recommended that the structure be cleaned out, and that calibration tests be performed on the flume to check the accuracy of the readings.

7.3 TREATMENT SYSTEM RECOMMENDATIONS

After reviewing the sizing requirements for treatment lagoon needs, it has been established that the existing lagoon system is adequate for the 20-year planning period. It is recommended that the City routinely check clay liners of the dry cells. Cracked liners would require rehabilitation to recreate a water tight liner to meet the seepage requirements set by the State. Additionally, the headworks structure should be cleaned out and calibration tests shall be performed on the flume to check the accuracy of the readings.

8.0 CAPITAL IMPROVEMENTS PLAN

The Capital Improvements Plan provides a summary of recommended improvements to the system and an engineer's opinion of probable costs for the proposed improvements based on the current estimated value of the improvements. The recommended improvements are listed below in order of an estimated priority, based on the anticipated condition of the system. Once the collection system video inspection is completed, the improvements may be better prioritized based on the current condition of the system.

8.1 PRE-CONSTRUCTION RECOMMENDATIONS

A critical step in determining the appropriate phasing of system improvements will be to perform a detailed investigation of the existing system and a detailed performance analysis of the current lift stations. Therefore, it is recommended that the City have the full collection system cleaned and then have a sewer video inspection performed as soon as possible to identify the current condition of the existing pipes and manholes. It is also recommended that the City have a performance evaluation, such as a LiftShield diagnostic assessment completed on each of the lift stations that will remain in operation.

The engineer's opinion of probable cost for the sewer system cleaning and video inspection is \$196,500. Actual costs may vary based on the contractor's current rates at the time of inspection.

8.2 RECOMMENDED SYSTEM IMPROVEMENTS

The improvements in this section are grouped by zones for simplicity. Though the recommended improvements below are grouped by their geographic zone, the City can determine the priority of the improvements once the collection system video inspection is completed. As a means of cost savings and efficiency, certain improvements should occur in sequence or concurrently. These improvements are noted as such.

Zone A

- **Bypass Lift Station A.** With the redesign of approximately 1,600 linear feet of pipeline between Lift Station A and Lift Station F, the City could eliminate Lift Station A, bypassing the flow to Lift Station F. If the City chooses to eliminate Lift Station A, Lift Station F will need to be redesigned and upgraded to handle the increased flow. It is also recommended that the Lift Station A Bypass project happen concurrently or prior to any pipe redesign that may happen in Zone A.
- **Replace all VCP, transite, and concrete pipe in Zone A.** This represents the replacement of approximately 43,200 feet of sewer mains, 102 manholes, 531 service connections and cleanouts, and the replacement of all sewer laterals from the property line to the sewer main. The engineer's opinion of probable cost also includes the necessary pavement repairs associated with the replacement of sewer mains within City streets.

Zones B and C

- **Replace force main from Lift Station B to the lagoons.** The replacement of approximately 8,300 linear feet of new force main.
- **Upgrade Lift Station C.** As discussed in Section 5.3.3, a full replacement of Lift Station C should be considered. The lift station should be sized to meet the projected demands of the zone, including the West Millard Swimming Pool.

- **Replace all VCP, transite, and concrete pipe in Zone B and Zone C.** This represents the replacement of approximately 17,860 feet of sewer mains, 60 manholes, 184 service connections and cleanouts, and the replacement of all sewer laterals from the property line to the sewer main. The engineer’s opinion of probable cost also includes the necessary pavement repairs associated with the replacement of sewer mains within City streets.

Zones D and E

- **Replace all VCP, transite, and concrete pipe in Zone D and Zone E.** This represents the replacement of approximately 16,725 feet of sewer mains, 83 manholes, 209 service connections and cleanouts, and the replacement of all sewer laterals from the property line to the sewer main. The engineer’s opinion of probable cost also includes the necessary pavement repairs associated with the replacement of sewer mains within City streets. The concrete pipe in Zone D and Zone E serve some of the more recently developed areas in Delta, and as such may still be in serviceable condition. Improvements in these zones should be based on the results of the sewer video inspection and may not be necessary for many years.

Zones F

- **Upgrade Lift Station F.** Lift Station F will need to be redesigned and sized to meet the combined projected demand of Zones A and F if the City decides to bypass and eliminate Station A. With this improvement project, a new adequately sized force main will be required. The proposed force main would connect to the proposed force main conveying wastewater from Lift Station B to the existing lagoon.

The components of the recommended system improvements and the respective engineer’s opinion of probable cost are summarized in Table 8.2. The complete engineer’s opinion of probable cost is included in Appendix C. The total cost shown in the engineer’s opinion of probable cost represent the estimated present-day cost if all the recommended improvements were completed in a single project. This includes the general project items and the incidentals and professional services. Actual construction will likely take place in phases established by the results and observations from the sewer video inspection; therefore, the actual total cost will vary based on phasing.

Table 8.2: Summary of Recommended System Improvements

| Recommended Improvements | |
|---|----------------------|
| MOBILIZATION (5%) | \$ 810,000 |
| NEW GRAVITY MAIN - STATION A TO STATION F | \$ 215,280 |
| LIFT STATION F UPGRADES | \$ 305,000 |
| NEW FORCE MAIN FROM STATION F TO STATION | \$ 223,000 |
| SEWER REPLACEMENT - ZONE A | \$ 6,302,927 |
| NEW FORCE MAIN FROM STATION B TO LAGOONS | \$ 345,100 |
| LIFT STATION C UPGRADES | \$ 195,000 |
| SEWER REPLACEMENT - ZONE B & C | \$ 2,383,065 |
| SEWER REPLACEMENT - ZONE D & E- CITY STREET | \$ 2,302,075 |
| GENERAL PROJECT ITEMS | \$ 428,000 |
| CONTINGENCY | \$ 2,701,889 |
| INCIDENTALS & PROFESSIONAL SERVICES | \$ 2,671,000 |
| TOTAL | \$ 18,882,336 |

9.0 USER RATE ANALYSIS & PROJECT FUNDING OPTIONS

The current sewer rate is \$22.00 per ERC (single family residence). The approved budget for FY 2019 indicates that the actual operating expenses for the year ending June 30, 2018 were \$366,545. \$93,718 of this expense is listed as depreciation, leaving a net operating expense of \$272,827. With 1,206 ERC's billed, the average monthly sewer rate would need to be \$18.85 just to cover the actual operating expenses.

The FY 2019 budget projects that the operating expenses for the year ending June 30, 2019 will be \$650,974. \$100,000 of this expense is listed as depreciation, leaving a net operating expense of \$550,974. The average user rate would need to be \$38.07 to cover this expense with user fees. It is noted that the increase from FY 2018 to FY 2019 is due to a large projected capital outlay, additional contractual services, and additional materials and supplies, all of which may be related to the current master planning and proposed system investigation recommendations.

The funding agencies that could be approached for funding assistance for all or part of the cost of the improvements include the Water Quality Board, Permanent Community Impact Fund Board (CIB), USDA-Rural Development (RD), and the United States Army Corps of Engineers (USACE).

The CIB and the Water Quality Board consider a community's Median Adjusted Gross Income (MAGI) when determining the percentage of loan and grant to approve for a sewer improvement project. The maximum affordable sewer bill as determined by the Division of Water Quality is 1.4% of the monthly MAGI. Delta City's 2017 MAGI is \$43,944, and the corresponding maximum affordable sewer bill is \$51.27. Once a community has taken on enough debt to require the average rate to meet the maximum affordable sewer bill, the community then qualifies for grant funding from the CIB and Water Quality Board. However, it should be noted that the maximum affordable sewer bill is not a cap, and higher rates may be required if the funding agencies do not have the grant funds available or choose not to allocate the grant funds to the community to keep the rates below the 1.4%.

The USDA-RD also considers the median income for the community, but only to determine the funding structure for which the community qualifies. Delta City qualifies for the USDA-RD poverty category, which makes the City eligible for up to 45% grant, although the actual availability of grant funds does not always match the amount for which the community is eligible. The USDA-RD also requires that the community's rates are as high as "similar systems".

USACE 595 program funds are federal grant funds that may be awarded in conjunction with other project funding. In order to apply for 595 funds, the community must first make application to all other state and federal funding agencies for which the community qualifies. The 595 funds, if awarded, provide supplemental grant funds as a 75% match to the community's contribution.

As noted above, the City may choose to approach a single funding agency for all of the improvements, or a combination of agencies for a single or multiple phase project approach. Two sample funding scenarios are provided in Appendix D to demonstrate the possible range of required sewer rates to support the proposed improvements described in Section 8.0.

The first scenario assumes that the City obtains funding from the USDA-RD for the full amount of \$18,882,336 at 45% grant and 55% loan at 2.75% over 40 years. The resulting required average sewer rate would be \$59.83.

The second scenario assumes that the City obtains 70% of the project funding from USDA-RD at 45% grant and 55% loan, and the other 30% of the project funding from the Water Quality Board at 20% grant and 10% loan at 1% over 30 years. The resulting required average sewer rate for this scenario would be \$54.49, which is slightly higher than the 1.4% maximum affordable sewer rate. It is noted that other agencies, such as CIB or USACE could be approached to supplement the funding with additional grant funds to keep the average sewer rate below the maximum affordable sewer rate as well.

If the City decides to phase the projects over several years, it is anticipated that the resulting end average sewer rate will be higher than if the improvements are all done at once due to the loss of project efficiencies and rising construction costs, although the more gradual increase in sewer rates may make this a more feasible alternative for the City.

EXHIBIT 1

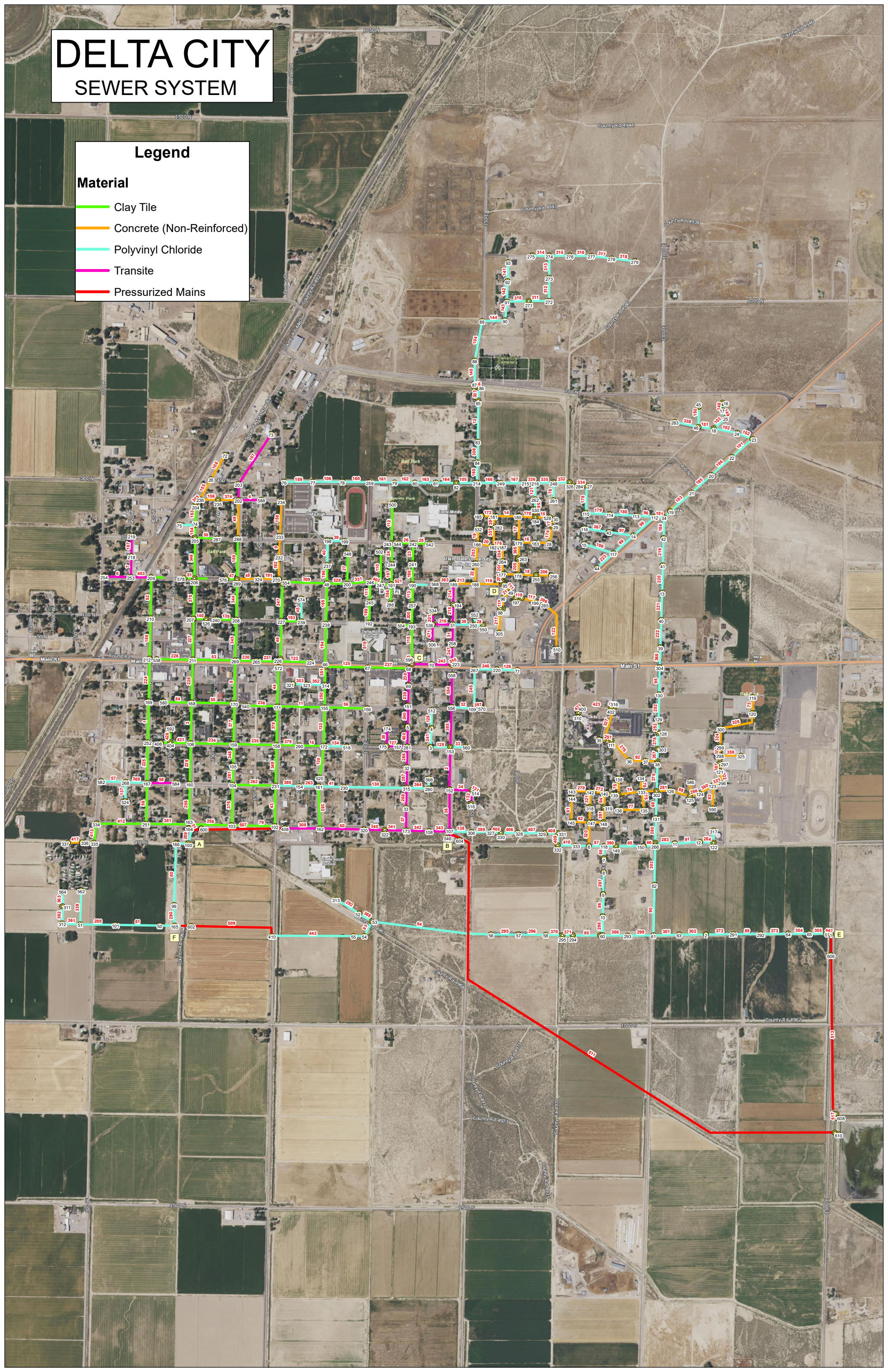
Existing Collection System Overview

DELTA CITY SEWER SYSTEM

Legend

Material

- Clay Tile
- Concrete (Non-Reinforced)
- Polyvinyl Chloride
- Transite
- Pressurized Mains



DELTA CITY SEWER SYSTEM

Legend
SEWER MAINS

DIAMETER

- 6"
- 8"
- 10"
- 12"
- 15"
- PRESSURE MAIN

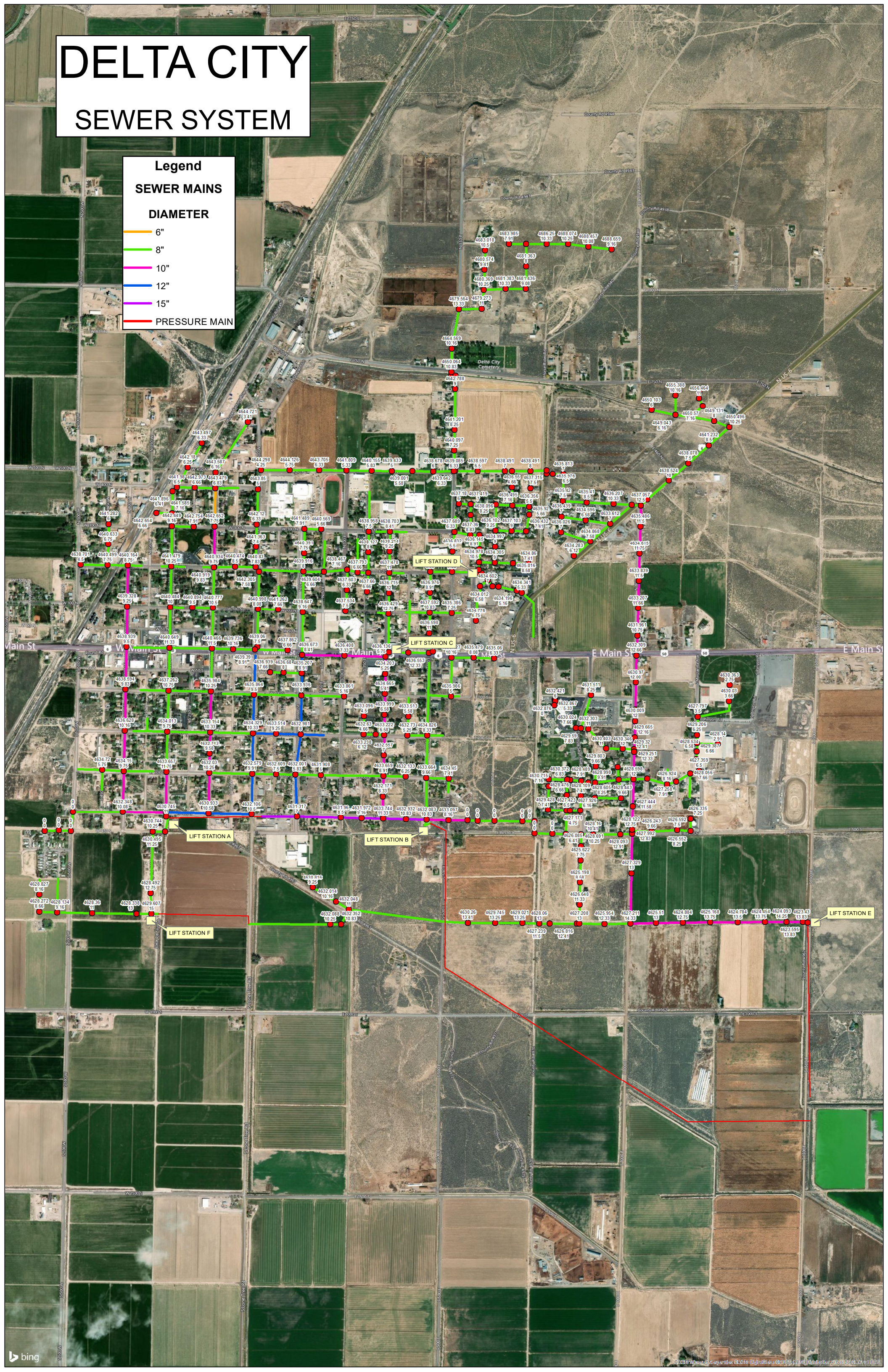


EXHIBIT 2

Existing Lagoon System Overview



SCALE: 1"=300'



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Delta City

Wastewater Lagoons



25 EAST 500 NORTH
FILLMORE, UTAH 84631
TEL 435.743.6151 • FAX 435.743.7900
www.sunrise-eng.com

EXHIBIT 3

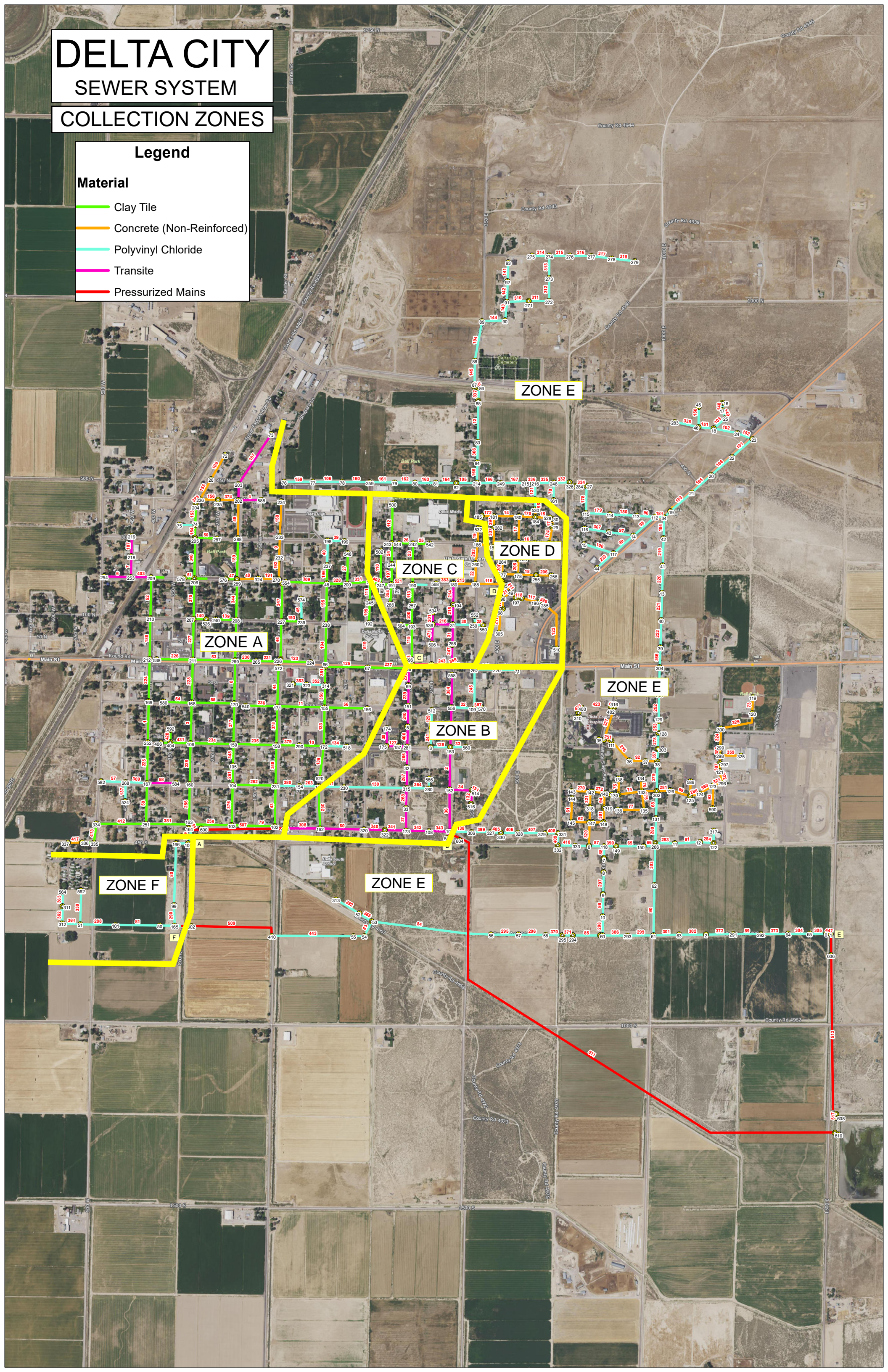
Collection System Zone Maps

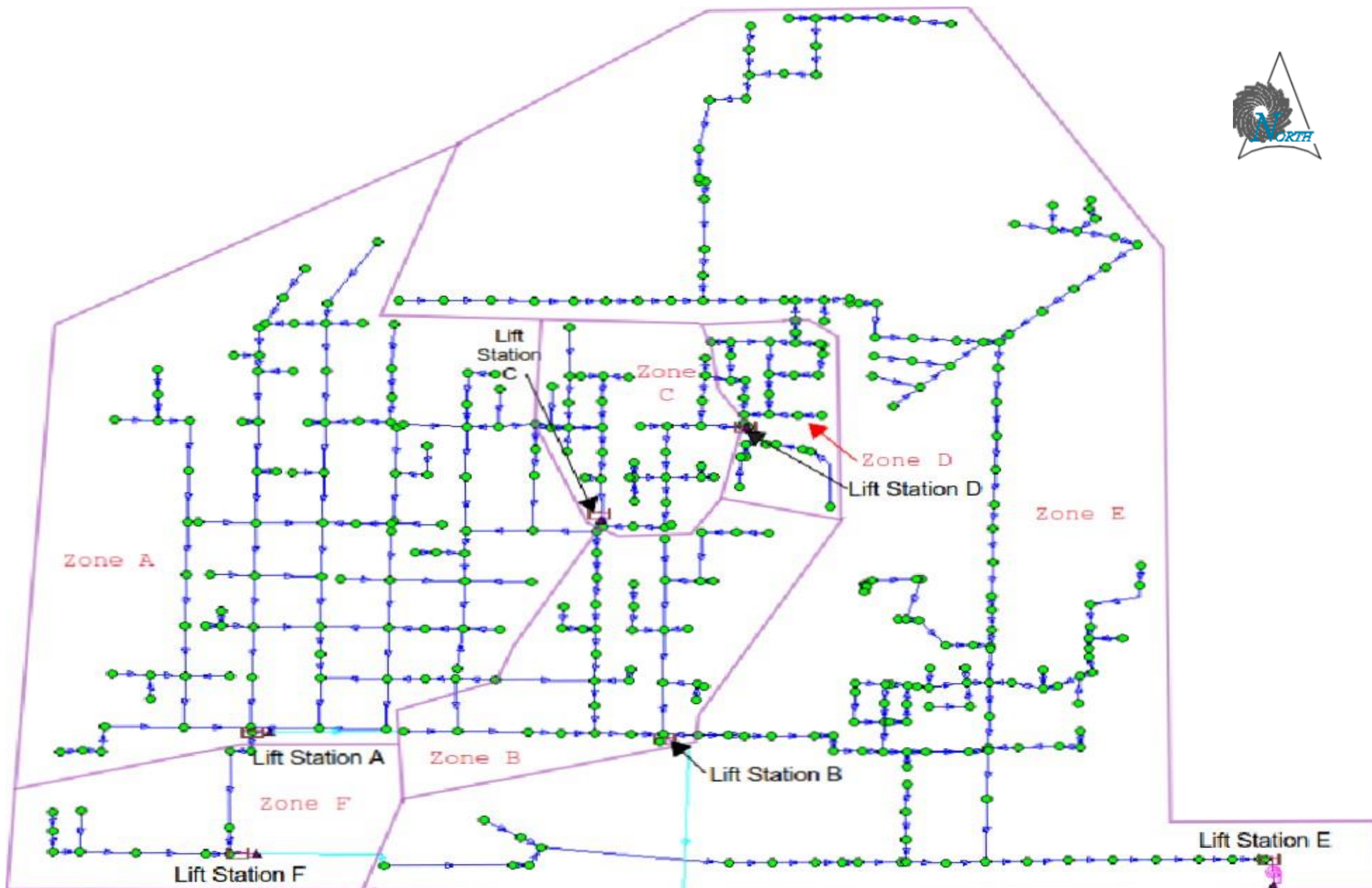
DELTA CITY SEWER SYSTEM COLLECTION ZONES

Legend

Material

- Clay Tile
- Concrete (Non-Reinforced)
- Polyvinyl Chloride
- Transite
- Pressurized Mains





Force Main
to Lagoon

Force Main
to Lagoon

EXHIBIT 4

Sewer Model Pipe Slope and Capacity Deficiencies

DELTA CITY SEWER SYSTEM

PIPES WITH POSSIBLE NEGATIVE SLOPES OR CAPACITY ISSUES - 2038

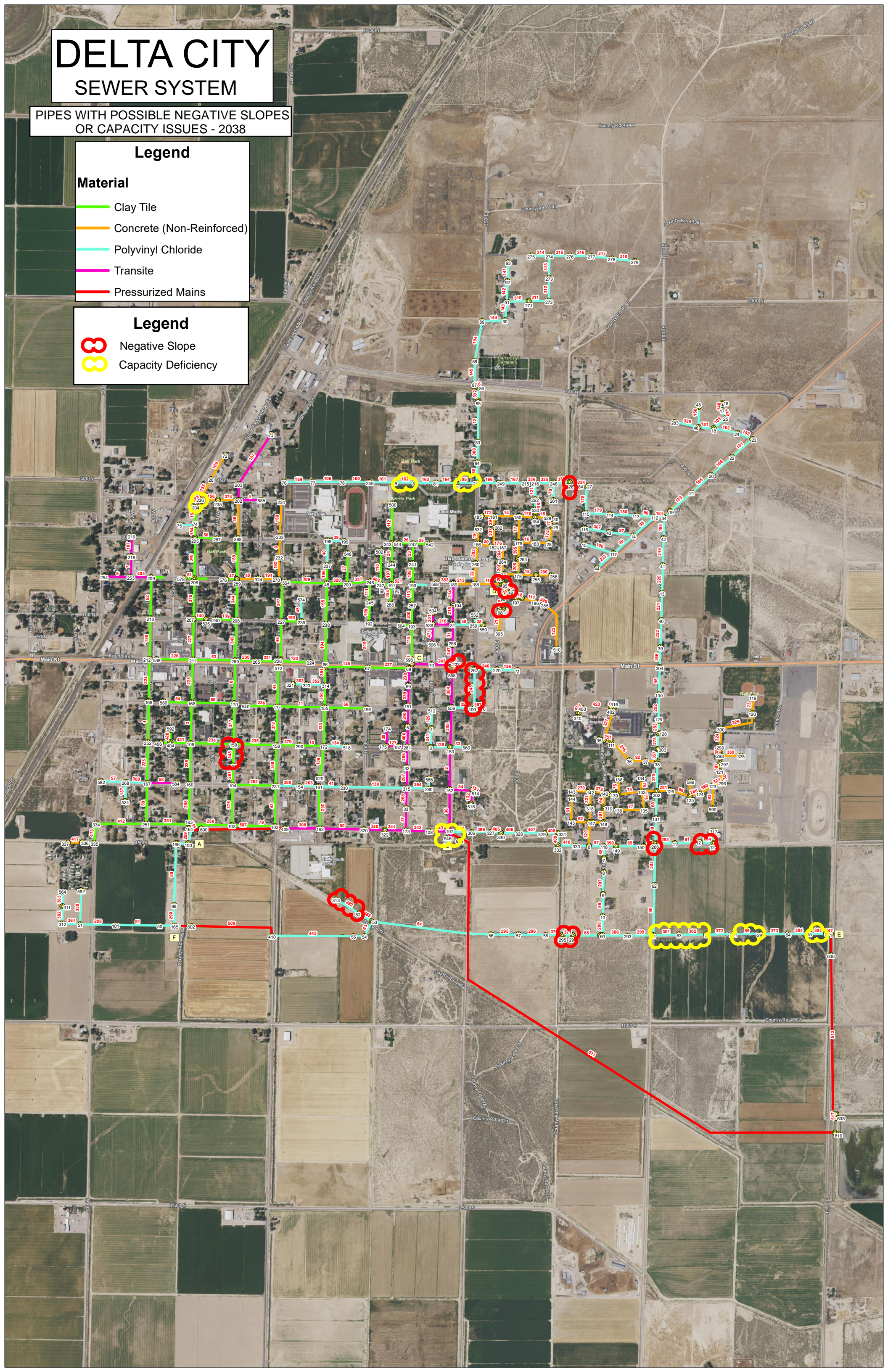
Legend

Material

- Clay Tile
- Concrete (Non-Reinforced)
- Polyvinyl Chloride
- Transite
- Pressurized Mains

Legend

- ⊗ Negative Slope
- ⊗ Capacity Deficiency



APPENDIX A:

Explanation of ERC Determinations

DETERMINATION OF ERC MULTIPLIER VALUES

Delta City provided the following table of connection types within the system in February 2018.

| | Connections |
|---------------------------|-------------|
| Residential | 908 |
| Commercial | 65 |
| Laundromat/Car Wash | 4 |
| Meat Shop | 2 |
| Café/Restaurant | 10 |
| Churches | 14 |
| Hospitals | 2 |
| Motels | 6 |
| Café, 2 Office | 1 |
| Government | 15 |
| School Sewer, Per Student | 5 |
| 5 Offices | 1 |
| 1 Café, 2 full 2 half | 1 |
| 1 Café, 1 full 1 half | 1 |
| School (Administrative) | 6 |
| Total | 1041 |

Utah Code R317-4 Table 3 provides average wastewater flows for various types of commercial establishments. Using the values from Table 3 and estimates for the numbers of washers, units, and students, the following estimates were made for commercial wastewater flows:

Laundromat

$$6 \text{ washers} \times \frac{580 \text{ gpd}}{\text{Washer}} = 3480 \text{ gpd}$$

Hospital

$$28 \text{ bedspaces} \times \frac{250 \text{ gpd}}{\text{Bed space}} = 7,000 \text{ gpd}$$

Motels

$$160 \text{ total units} \times \frac{125 \text{ gpd}}{\text{Unit}} = 20,000 \text{ gpd}$$

School

$$1889 \text{ total students} \times \frac{20 \text{ gpd}}{\text{Student}} = 37,780 \text{ gpd}$$

The average flow per ERC was estimated by dividing the 2018 population of 3580 by the 980 residential connections on the system, for an average of 4 residents per ERC. The average flows per ERC is therefore estimated to be 400 gpd based on 100 gpcpd.

Equivalent ERC multipliers were then established for each connection type based on the estimated wastewater flow from each type of establishment. The ERC multipliers and resulting ERC's are shown in the following table.

| | Connections | ERC/Connection | ERC's |
|---------------------------|-------------|----------------|-------------|
| Residential | 908 | 1 | 908 |
| Commercial | 65 | 1 | 65 |
| Laundromat/Car Wash | 4 | 2.25 | 9 |
| Meat Shop | 2 | 1 | 2 |
| Café/Restaurant | 10 | 1 | 10 |
| Churches | 14 | 1 | 14 |
| Hospitals | 2 | 9 | 18 |
| Motels | 6 | 8.5 | 51 |
| Café, 2 Office | 1 | 1 | 1 |
| Government | 15 | 1 | 15 |
| School Sewer, Per Student | 5 | 20 | 100 |
| 5 Offices | 1 | 1 | 1 |
| 1 Café, 2 full 2 half | 1 | 1 | 1 |
| 1 Café, 1 full 1 half | 1 | 1 | 1 |
| School (Administrative) | 6 | 1 | 6 |
| Total | 1041 | | 1202 |

The different types of establishments were then grouped into residential, commercial, and government/institutional connection types. The total number of ERC's for each connection group from the table above was divided by the total number of connections in that connection group to establish an average ERC per connection value. These average ERC/connection multipliers are shown in the table below.

| EXISTING | | | |
|--------------------------|-------------|----------------|-------------|
| | Connections | ERC/Connection | ERC's |
| Residential | 908 | 1 | 908 |
| Commercial | 105 | 1.5 | 158 |
| Government/Institutional | 28 | 5.0 | 140 |
| Total | 1041 | | 1206 |

APPENDIX B:

System Model Output

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 1 | Interceptor | 10 | 599 | 0.40% | 21.09 | 610.42 | 4% | 1.164 | 0.106 |
| 2 | Collector | 8 | 623 | 0.40% | 17.495 | 344.037 | 5% | 1.15 | 0.102 |
| 3 | Collector | 8 | 595 | 0.40% | 11.736 | 334.247 | 4% | 1 | 0.085 |
| 4 | Collector | 8 | 339 | 0.30% | 0 | 312.33 | 0% | 0 | 0 |
| 6 | Collector | 8 | 392 | 0.40% | 1.56 | 331.042 | 1% | 0.54 | 0.033 |
| 7 | Collector | 8 | 305 | 0.40% | 6.25 | 331.85 | 2% | 0.824 | 0.063 |
| 8 | Collector | 8 | 628 | 0.50% | 77.11 | 390.363 | 20% | 1.939 | 0.201 |
| 9 | Collector | 8 | 333 | 0.60% | 5.467 | 413.457 | 1% | 0.922 | 0.054 |
| 10 | Collector | 12 | 357 | 0.20% | 96.512 | 718.558 | 13% | 1.42 | 0.248 |
| 11 | Collector | 8 | 692 | 0.10% | 0.741 | 135.232 | 1% | 0.231 | 0.035 |
| 12 | Collector | 8 | 601 | 0.10% | 15.987 | 202.979 | 8% | 0.772 | 0.127 |
| 14 | Collector | 8 | 369 | 0.50% | 3.436 | 401.499 | 1% | 0.785 | 0.044 |
| 15 | Collector | 8 | 215 | 0.30% | 0 | 312.4 | 0% | 0 | 0 |
| 16 | Collector | 8 | 236 | 0.50% | 10.932 | 395.57 | 3% | 1.102 | 0.076 |
| 17 | Collector | 8 | 381 | 0.40% | 18.87 | 347.29 | 5% | 1.184 | 0.106 |
| 18 | Collector | 8 | 264 | 0.40% | 1.56 | 355.605 | 0% | 0.567 | 0.032 |
| 19 | Collector | 8 | 218 | 0.30% | 0 | 318.19 | 0% | 0 | 0 |
| 20 | Collector | 8 | 238 | 1.20% | 1.434 | 592.996 | 0% | 0.789 | 0.024 |
| 21 | Collector | 8 | 146 | 0.40% | 0 | 361.84 | 0% | 0 | 0 |
| 22 | Collector | 8 | 299 | 0.30% | 0.906 | 281.988 | 0% | 0.409 | 0.028 |
| 23 | Collector | 8 | 293 | 0.50% | 3.125 | 365.98 | 1% | 0.715 | 0.044 |
| 24 | Collector | 8 | 307 | 0.40% | 0 | 358.21 | 0% | 0 | 0 |
| 25 | Collector | 8 | 243 | 0.30% | 0 | 312.45 | 0% | 0 | 0 |
| 26 | Collector | 8 | 202 | 0.30% | 0 | 312.337 | 0% | 0 | 0 |
| 27 | Collector | 8 | 454 | 0.30% | 0 | 312.38 | 0% | 0 | 0 |
| 28 | Collector | 8 | 121 | 0.30% | 0 | 312.235 | 0% | 0 | 0 |
| 29 | Collector | 8 | 133 | 0.30% | 0 | 312.482 | 0% | 0 | 0 |
| 30 | Collector | 8 | 328 | 0.40% | 3.125 | 351.801 | 1% | 0.695 | 0.044 |
| 31 | Collector | 8 | 301 | 0.40% | 88.379 | 338.125 | 26% | 1.816 | 0.233 |
| 32 | Collector | 8 | 336 | 0.30% | 5.415 | 312.321 | 2% | 0.756 | 0.061 |
| 33 | Collector | 8 | 226 | 0.30% | 0 | 312.391 | 0% | 0 | 0 |
| 34 | Collector | 8 | 329 | 0.90% | 2.345 | 522.712 | 0% | 0.839 | 0.032 |
| 35 | Collector | 8 | 144 | 0.30% | 1.927 | 312.276 | 1% | 0.553 | 0.037 |
| 36 | Collector | 8 | 612 | 0.40% | 20.62 | 364.525 | 6% | 1.258 | 0.108 |
| 37 | Collector | 10 | 328 | 0.40% | 83.645 | 650.44 | 13% | 1.828 | 0.202 |
| 38 | Collector | 8 | 264 | 0.20% | 3.905 | 264.732 | 2% | 0.61 | 0.057 |
| 39 | Collector | 8 | 248 | 0.50% | 1.927 | 398.51 | 1% | 0.655 | 0.033 |
| 40 | Collector | 8 | 360 | 0.30% | 5.782 | 277.517 | 2% | 0.71 | 0.067 |
| 41 | Collector | 8 | 373 | 0.20% | 0.921 | 241.61 | 0% | 0.369 | 0.03 |
| 43 | Collector | 12 | 593 | 0.20% | 42.018 | 678.736 | 6% | 1.069 | 0.169 |
| 44 | Collector | 12 | 569 | 0.30% | 0 | 921.01 | 0% | 0 | 0 |
| 45 | Collector | 8 | 334 | 0.30% | 0 | 312.426 | 0% | 0 | 0 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 46 | Collector | 8 | 554 | 0.20% | 16.402 | 269.35 | 6% | 0.95 | 0.112 |
| 47 | Collector | 8 | 625 | 0.30% | 0 | 312.36 | 0% | 0 | 0 |
| 48 | Collector | 8 | 315 | 0.30% | 18.745 | 272.47 | 7% | 0.996 | 0.118 |
| 49 | Collector | 6 | 555 | 0.30% | 3.207 | 141.631 | 2% | 0.661 | 0.052 |
| 50 | Collector | 8 | 321 | 0.50% | 3.125 | 378.75 | 1% | 0.732 | 0.043 |
| 51 | Collector | 8 | 632 | 0.30% | 0 | 312.368 | 0% | 0 | 0 |
| 52 | Interceptor | 10 | 599 | 0.20% | 13.275 | 465.60 | 3% | 0.838 | 0.097 |
| 53 | Collector | 8 | 620 | 0.10% | 5.218 | 129.787 | 4% | 0.405 | 0.091 |
| 54 | Collector | 8 | 410 | 0.30% | 0 | 312.335 | 0% | 0 | 0 |
| 55 | Collector | 8 | 623 | 0.10% | 6.76 | 192.519 | 4% | 0.576 | 0.085 |
| 56 | Collector | 8 | 627 | 0.40% | 1.56 | 361.017 | 0% | 0.573 | 0.032 |
| 57 | Collector | 8 | 354 | 0.30% | 1.927 | 312.34 | 1% | 0.553 | 0.037 |
| 58 | Collector | 8 | 429 | 0.30% | 0 | 312.38 | 0% | 0 | 0 |
| 59 | Interceptor | 10 | 596 | 0.40% | 40.2 | 589.703 | 7% | 1.376 | 0.147 |
| 60 | Interceptor | 15 | 644 | 0.10% | 310.614 | 1060.321 | 29% | 1.672 | 0.463 |
| 61 | Collector | 8 | 349 | 0.40% | 0 | 361.014 | 0% | 0 | 0 |
| 62 | Collector | 8 | 271 | 0.40% | 7.032 | 345.836 | 2% | 0.878 | 0.066 |
| 64 | Collector | 8 | 157 | 0.40% | 2.345 | 351.35 | 1% | 0.637 | 0.039 |
| 65 | Collector | 8 | 401 | 0.40% | 26.547 | 344.74 | 8% | 1.303 | 0.125 |
| 66 | Collector | 8 | 169 | 0.60% | 28.107 | 408.962 | 7% | 1.495 | 0.118 |
| 67 | Interceptor | 10 | 41 | -0.10% | 143.32 | | 100% | 0.585 | 0.833 |
| 68 | Interceptor | 10 | 397 | 0.20% | 139.42 | 424.174 | 33% | 1.553 | 0.329 |
| 69 | Collector | 8 | 300 | 0.40% | 12.032 | 342.337 | 4% | 1.025 | 0.086 |
| 70 | Collector | 8 | 217 | 0.30% | 0 | 312.298 | 0% | 0 | 0 |
| 73 | Collector | 8 | 238 | 0.50% | 1.927 | 392.86 | 1% | 0.648 | 0.034 |
| 74 | Collector | 8 | 347 | 0.40% | 15.627 | 355.763 | 4% | 1.139 | 0.095 |
| 75 | Collector | 8 | 236 | 0.40% | 4.687 | 363.69 | 1% | 0.805 | 0.053 |
| 76 | Collector | 8 | 180 | 0.50% | 3.905 | 373.943 | 1% | 0.776 | 0.048 |
| 77 | Collector | 8 | 383 | 0.40% | 6.247 | 348.23 | 2% | 0.852 | 0.062 |
| 78 | Collector | 8 | 257 | 0.30% | 1.56 | 285.581 | 1% | 0.487 | 0.035 |
| 79 | Interceptor | 12 | 629 | 0.20% | 42.018 | 715.39 | 6% | 1.109 | 0.164 |
| 80 | Collector | 8 | 903 | 0.30% | 3.855 | 300.212 | 1% | 0.664 | 0.053 |
| 81 | Collector | 8 | 649 | 0.30% | 21.09 | 303.62 | 7% | 1.113 | 0.119 |
| 83 | Collector | 8 | 239 | 0.20% | 24.945 | 241.986 | 10% | 0.996 | 0.145 |
| 84 | Collector | 8 | 1391 | 0.30% | 24.945 | 289.02 | 9% | 1.13 | 0.132 |
| 85 | Collector | 8 | 400 | 0.30% | 24.945 | 314.036 | 8% | 1.198 | 0.127 |
| 86 | Collector | 8 | 327 | 0.40% | 3.12 | 343.03 | 1% | 0.683 | 0.045 |
| 87 | Collector | 8 | 223 | 0.40% | 23.427 | 343.997 | 7% | 1.254 | 0.118 |
| 88 | Collector | 8 | 173 | 0.70% | 1.56 | 459.78 | 0% | 0.678 | 0.028 |
| 89 | Interceptor | 10 | 400 | 0.00% | 204.183 | 180.373 | 113% | 0.834 | 0.833 |
| 90 | Interceptor | 10 | 741 | 0.20% | 172.993 | 436.00 | 40% | 1.678 | 0.365 |
| 91 | Collector | 8 | 373 | 0.70% | 0.78 | 445.816 | 0% | 0.537 | 0.021 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 92 | Collector | 8 | 240 | 0.40% | 9.685 | 360.92 | 3% | 0.997 | 0.075 |
| 93 | Collector | 8 | 340 | 0.30% | 0 | 312.65 | 0% | 0 | 0 |
| 94 | Collector | 8 | 217 | 0.50% | 3.125 | 367.781 | 1% | 0.717 | 0.044 |
| 95 | Interceptor | 10 | 398 | 0.20% | 73.963 | 430.716 | 17% | 1.316 | 0.234 |
| 96 | Collector | 8 | 262 | 0.20% | 48.976 | 243.084 | 20% | 1.214 | 0.203 |
| 97 | Collector | 8 | 361 | 0.40% | 7.03 | 338.932 | 2% | 0.866 | 0.066 |
| 98 | Collector | 8 | 417 | 0.30% | 11.715 | 298.777 | 4% | 0.924 | 0.09 |
| 99 | Collector | 8 | 390 | 0.20% | 3.905 | 226.433 | 2% | 0.547 | 0.061 |
| 100 | Collector | 8 | 449 | 0.40% | 3.125 | 338.22 | 1% | 0.677 | 0.045 |
| 101 | Collector | 8 | 399 | 1.90% | 0 | 746.248 | 0% | 0 | 0 |
| 102 | Collector | 8 | 353 | 0.50% | 0 | 379.902 | 0% | 0 | 0 |
| 103 | Collector | 8 | 235 | 2.80% | 0 | 908.81 | 0% | 0 | 0 |
| 104 | Collector | 8 | 588 | 2.00% | 12.082 | 770.885 | 2% | 1.81 | 0.058 |
| 105 | Collector | 8 | 301 | 0.00% | 2.34 | | 100% | 0.015 | 0.667 |
| 106 | Collector | 8 | 432 | 0.20% | 0.78 | 261.727 | 0% | 0.371 | 0.027 |
| 107 | Collector | 8 | 872 | 0.40% | 1.56 | 362.986 | 0% | 0.575 | 0.032 |
| 108 | Collector | 8 | 407 | 0.30% | 2.342 | 299.62 | 1% | 0.57 | 0.042 |
| 109 | Collector | 8 | 236 | 0.70% | 0 | 443.204 | 0% | 0 | 0 |
| 110 | Collector | 8 | 491 | 0.30% | 0 | 312.398 | 0% | 0 | 0 |
| 111 | Collector | 8 | 299 | 0.00% | 0.829 | 58.028 | 1% | 0.133 | 0.056 |
| 112 | Collector | 8 | 581 | 0.30% | 0 | 312.364 | 0% | 0 | 0 |
| 113 | Collector | 8 | 295 | 0.60% | 15.858 | 420.122 | 4% | 1.285 | 0.089 |
| 114 | Collector | 8 | 157 | 0.30% | 0 | 312.418 | 0% | 0 | 0 |
| 115 | Collector | 8 | 508 | 0.30% | 26.011 | 312.377 | 8% | 1.208 | 0.13 |
| 116 | Collector | 8 | 390 | 0.40% | 68.411 | 362.25 | 19% | 1.776 | 0.196 |
| 117 | Collector | 8 | 269 | 0.40% | 0 | 343.674 | 0% | 0 | 0 |
| 118 | Collector | 8 | 89 | 0.60% | 0 | 418.459 | 0% | 0 | 0 |
| 119 | Collector | 8 | 157 | 0.50% | 0 | 380.707 | 0% | 0 | 0 |
| 121 | Collector | 8 | 240 | 0.40% | 0.966 | 321.807 | 0% | 0.457 | 0.027 |
| 122 | Collector | 8 | 724 | 0.30% | 0 | 312.37 | 0% | 0 | 0 |
| 123 | Collector | 8 | 477 | 0.20% | 0.78 | 211.678 | 0% | 0.32 | 0.029 |
| 124 | Collector | 8 | 287 | 0.50% | 90.724 | 369.465 | 25% | 1.95 | 0.225 |
| 125 | Collector | 10 | 624 | 0.10% | 61.371 | 356.317 | 17% | 1.089 | 0.234 |
| 126 | Collector | 8 | 303 | 0.40% | 3.855 | 360.497 | 1% | 0.754 | 0.049 |
| 127 | Collector | 8 | 177 | 0.50% | 3.905 | 376.977 | 1% | 0.781 | 0.048 |
| 128 | Collector | 8 | 289 | 0.30% | 1.56 | 317.203 | 1% | 0.524 | 0.034 |
| 129 | Collector | 8 | 270 | 0.30% | 0 | 312.474 | 0% | 0 | 0 |
| 130 | Collector | 8 | 915 | 0.20% | 1.007 | 264.221 | 0% | 0.404 | 0.03 |
| 131 | Collector | 8 | 61 | 0.30% | 0 | 312.024 | 0% | 0 | 0 |
| 132 | Collector | 8 | 194 | 0.30% | 0 | 312.431 | 0% | 0 | 0 |
| 133 | Collector | 12 | 566 | 0.20% | 92.607 | 658.479 | 14% | 1.319 | 0.253 |
| 134 | Collector | 12 | 339 | 0.30% | 0 | 921.061 | 0% | 0 | 0 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 135 | Collector | 12 | 467 | 0.30% | 0 | 921.011 | 0% | 0 | 0 |
| 137 | Collector | 8 | 283 | 1.30% | 0 | 620.492 | 0% | 0 | 0 |
| 138 | Interceptor | 10 | 322 | 0.30% | 0 | 580.465 | 0% | 0 | 0 |
| 139 | Collector | 8 | 300 | 0.20% | 3.905 | 245.547 | 2% | 0.579 | 0.059 |
| 140 | Collector | 8 | 185 | 1.30% | 0 | 612.676 | 0% | 0 | 0 |
| 141 | Collector | 8 | 280 | 0.40% | 0.78 | 332.042 | 0% | 0.438 | 0.024 |
| 142 | Collector | 8 | 297 | 0.60% | 3.905 | 428.555 | 1% | 0.854 | 0.045 |
| 143 | Collector | 8 | 277 | 0.70% | 8.957 | 443.919 | 2% | 1.125 | 0.066 |
| 144 | Collector | 8 | 335 | 4.50% | 11.302 | 1156.831 | 1% | 2.354 | 0.047 |
| 145 | Collector | 8 | 343 | 0.30% | 12.082 | 285.816 | 4% | 0.904 | 0.093 |
| 146 | Collector | 8 | 60 | 2.50% | 14.427 | 864.173 | 2% | 2.068 | 0.06 |
| 147 | Collector | 8 | 46 | 5.30% | 14.427 | 1255.595 | 1% | 2.684 | 0.05 |
| 148 | Collector | 8 | 112 | 2.20% | 0 | 808.44 | 0% | 0 | 0 |
| 149 | Collector | 8 | 123 | 1.90% | 0 | 751.34 | 0% | 0 | 0 |
| 150 | Collector | 8 | 293 | 0.00% | 0 | 52.229 | 0% | 0 | 0 |
| 151 | Collector | 8 | 225 | 0.40% | 0 | 341.323 | 0% | 0 | 0 |
| 152 | Collector | 8 | 235 | 0.50% | 0 | 365.303 | 0% | 0 | 0 |
| 153 | Collector | 8 | 319 | 0.40% | 9.286 | 324.499 | 3% | 0.914 | 0.077 |
| 154 | Collector | 8 | 186 | 0.20% | 11.631 | 267.55 | 4% | 0.854 | 0.095 |
| 155 | Collector | 8 | 336 | 0.20% | 2.342 | 270.594 | 1% | 0.531 | 0.044 |
| 156 | Collector | 8 | 262 | 0.30% | 3.818 | 296.358 | 1% | 0.656 | 0.053 |
| 157 | Collector | 8 | 237 | 1.30% | 2.34 | 617.266 | 0% | 0.942 | 0.03 |
| 158 | Collector | 8 | 514 | 0.30% | 0.78 | 310.272 | 0% | 0.418 | 0.025 |
| 159 | Collector | 8 | 419 | 0.20% | 0 | 251.52 | 0% | 0 | 0 |
| 160 | Collector | 8 | 402 | 0.50% | 0.78 | 398.155 | 0% | 0.497 | 0.022 |
| 161 | Collector | 8 | 365 | 0.60% | 0.78 | 417.715 | 0% | 0.513 | 0.021 |
| 162 | Collector | 8 | 297 | 0.00% | 0.78 | | 100% | 0.005 | 0.667 |
| 163 | Collector | 8 | 302 | 0.30% | 0.78 | 314.579 | 0% | 0.422 | 0.024 |
| 164 | Collector | 8 | 301 | 0.20% | 0.78 | 270.026 | 0% | 0.379 | 0.026 |
| 165 | Collector | 8 | 301 | 0.20% | 20.677 | 254.265 | 8% | 0.977 | 0.129 |
| 166 | Collector | 8 | 352 | 0.20% | 24.577 | 225.773 | 11% | 0.945 | 0.149 |
| 167 | Collector | 8 | 398 | 0.20% | 26.922 | 212.095 | 13% | 0.928 | 0.16 |
| 170 | Collector | 8 | 358 | 0.30% | 8.407 | 277.099 | 3% | 0.794 | 0.08 |
| 172 | Collector | 8 | 173 | 0.40% | 1.56 | 360.338 | 0% | 0.572 | 0.032 |
| 173 | Collector | 8 | 114 | 0.50% | 0.78 | 392.856 | 0% | 0.492 | 0.022 |
| 174 | Collector | 8 | 247 | 0.50% | 2.34 | 384.931 | 1% | 0.678 | 0.037 |
| 175 | Collector | 8 | 210 | 0.40% | 5.465 | 359.876 | 2% | 0.837 | 0.057 |
| 176 | Collector | 8 | 133 | 0.20% | 8.151 | 270.831 | 3% | 0.774 | 0.079 |
| 178 | Collector | 8 | 397 | 0.20% | 34.133 | 257.801 | 13% | 1.142 | 0.164 |
| 179 | Collector | 8 | 352 | 0.30% | 38.038 | 291.284 | 13% | 1.285 | 0.163 |
| 180 | Collector | 8 | 395 | 0.30% | 41.943 | 278.183 | 15% | 1.279 | 0.175 |
| 181 | Collector | 8 | 137 | 0.60% | 61.471 | 414.016 | 15% | 1.895 | 0.174 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 182 | Collector | 8 | 128 | 1.10% | 0.78 | 576.353 | 0% | 0.642 | 0.018 |
| 183 | Collector | 8 | 416 | 0.60% | 0.78 | 423.617 | 0% | 0.518 | 0.021 |
| 184 | Interceptor | 10 | 307 | 0.20% | 62.251 | 425.244 | 15% | 1.241 | 0.215 |
| 185 | Collector | 8 | 384 | 0.50% | 0 | 397.73 | 0% | 0 | 0 |
| 186 | Collector | 8 | 400 | 0.50% | 0 | 399.091 | 0% | 0 | 0 |
| 187 | Collector | 8 | 298 | 0.50% | 3.125 | 372.303 | 1% | 0.723 | 0.043 |
| 188 | Interceptor | 10 | 595 | 0.10% | 15.62 | 323.105 | 5% | 0.681 | 0.125 |
| 189 | Collector | 10 | 601 | 0.60% | 9.454 | 775.365 | 1% | 1.08 | 0.065 |
| 191 | Collector | 8 | 298 | 0.30% | 12.497 | 319.011 | 4% | 0.987 | 0.09 |
| 192 | Collector | 8 | 295 | 0.30% | 9.372 | 294.242 | 3% | 0.855 | 0.082 |
| 193 | Collector | 8 | 295 | 0.20% | 9.372 | 262.021 | 4% | 0.789 | 0.086 |
| 194 | Collector | 8 | 627 | 0.20% | 26.59 | 240.211 | 11% | 1.01 | 0.15 |
| 195 | Collector | 8 | 592 | 0.40% | 21.123 | 348.304 | 6% | 1.227 | 0.111 |
| 196 | Collector | 8 | 270 | 0.30% | 13.595 | 281.961 | 5% | 0.928 | 0.1 |
| 197 | Collector | 8 | 298 | 0.80% | 0 | 471.48 | 0% | 0 | 0 |
| 198 | Collector | 8 | 310 | 0.80% | 8.592 | 487.041 | 2% | 1.185 | 0.062 |
| 199 | Collector | 8 | 307 | 0.40% | 0.829 | 345.43 | 0% | 0.458 | 0.024 |
| 200 | Collector | 8 | 306 | 0.30% | 19.763 | 316.37 | 6% | 1.124 | 0.113 |
| 201 | Collector | 8 | 169 | 0.30% | 0 | 312.46 | 0% | 0 | 0 |
| 202 | Collector | 8 | 58 | 0.30% | 0 | 312.13 | 0% | 0 | 0 |
| 203 | Collector | 8 | 293 | 0.00% | 0.126 | 52.22 | 0% | 0.069 | 0.024 |
| 204 | Collector | 8 | 211 | 0.50% | 11.276 | 368.20 | 3% | 1.058 | 0.08 |
| 205 | Collector | 8 | 234 | 0.30% | 39.955 | 295.70 | 14% | 1.317 | 0.166 |
| 206 | Collector | 8 | 226 | 0.40% | 0 | 363.856 | 0% | 0 | 0 |
| 207 | Collector | 8 | 231 | 0.40% | 45.42 | 325.67 | 14% | 1.464 | 0.168 |
| 208 | Collector | 8 | 189 | 1.50% | 14.401 | 656.916 | 2% | 1.707 | 0.068 |
| 209 | Collector | 8 | 111 | 0.50% | 63.726 | 373.85 | 17% | 1.78 | 0.186 |
| 210 | Collector | 8 | 66 | -3.60% | 66.851 | | 100% | 0.427 | 0.667 |
| 211 | Collector | 8 | 134 | 0.40% | 1.56 | 362.61 | 0% | 0.575 | 0.032 |
| 212 | Collector | 8 | 46 | 0.10% | 68.411 | 194.99 | 35% | 1.135 | 0.273 |
| 213 | Collector | 8 | 320 | 0.40% | 69.317 | 346.94 | 20% | 1.728 | 0.202 |
| 214 | Collector | 8 | 310 | 0.40% | 73.172 | 332.98 | 22% | 1.704 | 0.212 |
| 215 | Collector | 8 | 291 | 0.40% | 77.077 | 364.24 | 21% | 1.844 | 0.208 |
| 216 | Collector | 8 | 293 | 0.30% | 1.927 | 312.35 | 1% | 0.553 | 0.037 |
| 217 | Collector | 8 | 352 | 0.50% | 0 | 380.83 | 0% | 0 | 0 |
| 218 | Collector | 8 | 37 | -0.20% | 0 | | 0% | 0 | 0 |
| 219 | Interceptor | 10 | 400 | 0.30% | 63.811 | 522.29 | 12% | 1.446 | 0.197 |
| 220 | Interceptor | 10 | 400 | 0.10% | 64.591 | 357.523 | 18% | 1.108 | 0.24 |
| 221 | Interceptor | 10 | 399 | 0.20% | 64.591 | 439.33 | 15% | 1.283 | 0.216 |
| 222 | Interceptor | 10 | 401 | 0.10% | 66.151 | 285.27 | 23% | 0.948 | 0.273 |
| 223 | Collector | 8 | 321 | 0.30% | 0 | 283.86 | 0% | 0 | 0 |
| 224 | Interceptor | 10 | 625 | 0.10% | 17.965 | 323.93 | 6% | 0.711 | 0.133 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 225 | Interceptor | 10 | 597 | 0.30% | 27.337 | 580.45 | 5% | 1.214 | 0.123 |
| 226 | Collector | 8 | 525 | 0.30% | 0 | 312.359 | 0% | 0 | 0 |
| 227 | Collector | 8 | 597 | 0.20% | 16.683 | 240.27 | 7% | 0.881 | 0.119 |
| 228 | Collector | 8 | 630 | 0.40% | 14.59 | 362.92 | 4% | 1.131 | 0.091 |
| 229 | Collector | 8 | 595 | 0.40% | 10.659 | 342.18 | 3% | 0.988 | 0.081 |
| 230 | Collector | 8 | 312 | 0.20% | 28.12 | 240.64 | 12% | 1.028 | 0.154 |
| 231 | Collector | 8 | 319 | 0.30% | 24.215 | 289.66 | 8% | 1.122 | 0.13 |
| 232 | Collector | 8 | 51 | 2.10% | 23.435 | 788.276 | 3% | 2.245 | 0.079 |
| 234 | Collector | 8 | 628 | 0.20% | 8.107 | 260.26 | 3% | 0.752 | 0.081 |
| 235 | Collector | 8 | 628 | 0.20% | 40.644 | 235.203 | 17% | 1.124 | 0.188 |
| 236 | Collector | 8 | 460 | 0.30% | 0 | 312.39 | 0% | 0 | 0 |
| 237 | Collector | 10 | 602 | 0.20% | 54.764 | 459.591 | 12% | 1.263 | 0.194 |
| 238 | Collector | 10 | 250 | 0.30% | 63.531 | 533.17 | 12% | 1.466 | 0.194 |
| 239 | Collector | 10 | 298 | 0.10% | 65.096 | 361.575 | 18% | 1.119 | 0.239 |
| 240 | Collector | 10 | 302 | 0.60% | 66.656 | 768.51 | 9% | 1.925 | 0.166 |
| 241 | Collector | 8 | 278 | 0.20% | 1.56 | 219.507 | 1% | 0.406 | 0.04 |
| 242 | Collector | 8 | 124 | 0.40% | 3.905 | 336.82 | 1% | 0.722 | 0.05 |
| 243 | Collector | 8 | 297 | 0.40% | 88.379 | 349.273 | 25% | 1.859 | 0.229 |
| 245 | Collector | 8 | 577 | -0.80% | 3.855 | | 100% | 0.025 | 0.667 |
| 246 | Collector | 8 | 327 | 0.30% | 3.855 | 319.904 | 1% | 0.694 | 0.051 |
| 247 | Collector | 8 | 287 | 0.50% | 88.379 | 376.67 | 24% | 1.963 | 0.22 |
| 250 | Collector | 8 | 70 | 0.90% | 1.925 | 503.671 | 0% | 0.77 | 0.03 |
| 251 | Collector | 8 | 111 | 0.40% | 7.34 | 348.817 | 2% | 0.895 | 0.067 |
| 252 | Interceptor | 10 | 399 | 0.20% | 76.308 | 406.068 | 19% | 1.273 | 0.245 |
| 253 | Interceptor | 10 | 163 | 0.10% | 77.868 | 348.525 | 22% | 1.147 | 0.268 |
| 256 | Collector | 10 | 595 | 0.40% | 16.906 | 660.489 | 3% | 1.151 | 0.092 |
| 257 | Collector | 10 | 59 | 0.90% | 0 | 912.97 | 0% | 0 | 0 |
| 258 | Interceptor | 12 | 625 | 0.20% | 226.755 | 676.657 | 34% | 1.729 | 0.399 |
| 259 | Collector | 8 | 207 | 0.20% | 0 | 267.51 | 0% | 0 | 0 |
| 260 | Collector | 8 | 183 | 0.40% | 1.927 | 348.467 | 1% | 0.596 | 0.036 |
| 261 | Collector | 10 | 278 | 0.50% | 148.245 | 695.52 | 21% | 2.258 | 0.261 |
| 262 | Collector | 8 | 629 | 0.10% | 28.68 | 204.387 | 14% | 0.92 | 0.169 |
| 263 | Collector | 8 | 280 | 0.40% | 2.293 | 334.80 | 1% | 0.612 | 0.039 |
| 266 | Collector | 10 | 299 | 0.40% | 71.341 | 594.096 | 12% | 1.637 | 0.195 |
| 267 | Collector | 10 | 302 | 0.30% | 72.121 | 509.59 | 14% | 1.472 | 0.212 |
| 268 | Collector | 10 | 297 | 0.30% | 82.085 | 544.963 | 15% | 1.603 | 0.219 |
| 269 | Interceptor | 8 | 85 | 0.40% | 417.219 | 1,840.34 | 23% | 2.703 | 0.405 |
| 270 | Collector | 8 | 270 | 0.30% | 2.342 | 294.976 | 1% | 0.564 | 0.042 |
| 272 | Collector | 8 | 162 | 0.50% | 2.345 | 398.72 | 1% | 0.695 | 0.037 |
| 273 | Collector | 8 | 101 | 0.50% | 7.815 | 381.05 | 2% | 0.97 | 0.066 |
| 274 | Collector | 8 | 218 | 0.50% | 32.81 | 369.13 | 9% | 1.455 | 0.134 |
| 275 | Collector | 8 | 272 | 0.40% | 10.152 | 358.203 | 3% | 1.005 | 0.077 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 276 | Collector | 8 | 390 | 0.50% | 9.685 | 379.58 | 3% | 1.032 | 0.073 |
| 277 | Collector | 8 | 171 | 0.80% | 11.245 | 495.965 | 2% | 1.302 | 0.069 |
| 278 | Interceptor | 10 | 238 | 0.20% | 77.868 | 453.71 | 17% | 1.385 | 0.234 |
| 279 | Interceptor | 10 | 399 | 0.10% | 93.798 | 275.876 | 34% | 1.019 | 0.335 |
| 280 | Interceptor | 10 | 363 | 0.20% | 140.2 | 433.58 | 32% | 1.58 | 0.326 |
| 281 | Collector | 8 | 201 | 0.50% | 12.812 | 379.206 | 3% | 1.122 | 0.084 |
| 282 | Interceptor | 10 | 37 | 0.00% | 93.798 | 170.30 | 55% | 0.712 | 0.441 |
| 283 | Collector | 8 | 286 | 0.50% | 2.34 | 383.118 | 1% | 0.676 | 0.037 |
| 284 | Collector | 8 | 196 | -0.40% | 0.78 | | 100% | 0.005 | 0.667 |
| 285 | Collector | 8 | 181 | 0.40% | 0.78 | 357.953 | 0% | 0.461 | 0.023 |
| 286 | Collector | 8 | 141 | 0.40% | 9.687 | 350.15 | 3% | 0.976 | 0.076 |
| 288 | Collector | 8 | 517 | 0.30% | 21.09 | 303.728 | 7% | 1.114 | 0.119 |
| 289 | Collector | 8 | 216 | 0.30% | 21.09 | 316.27 | 7% | 1.146 | 0.117 |
| 290 | Collector | 8 | 301 | 0.40% | 3.855 | 333.829 | 1% | 0.715 | 0.05 |
| 291 | Collector | 8 | 106 | 0.30% | 24.945 | 314.01 | 8% | 1.198 | 0.127 |
| 292 | Collector | 8 | 399 | -0.10% | 0 | | 0% | 0 | 0 |
| 293 | Collector | 8 | 159 | 0.70% | 24.945 | 454.08 | 6% | 1.553 | 0.106 |
| 295 | Collector | 8 | 401 | 0.20% | 24.945 | 214.644 | 12% | 0.915 | 0.153 |
| 296 | Collector | 8 | 398 | 0.20% | 24.945 | 231.829 | 11% | 0.967 | 0.148 |
| 297 | Collector | 8 | 326 | 0.40% | 1.56 | 337.525 | 1% | 0.547 | 0.033 |
| 298 | Collector | 8 | 275 | 0.40% | 6.245 | 345.27 | 2% | 0.847 | 0.062 |
| 299 | Collector | 8 | 380 | 0.10% | 31.19 | 124.10 | 25% | 0.659 | 0.228 |
| 300 | Collector | 8 | 34 | 0.60% | 24.945 | 412.775 | 6% | 1.453 | 0.111 |
| 301 | Interceptor | 10 | 375 | 0.10% | 204.183 | 310.247 | 66% | 1.353 | 0.493 |
| 302 | Interceptor | 10 | 391 | 0.10% | 204.183 | 305.61 | 67% | 1.337 | 0.498 |
| 303 | Interceptor | 10 | 573 | 0.10% | 171.428 | 380.61 | 45% | 1.514 | 0.392 |
| 304 | Interceptor | 10 | 315 | 0.30% | 204.183 | 541.97 | 38% | 2.058 | 0.354 |
| 305 | Interceptor | 10 | 241 | 0.00% | 204.183 | 177.21 | 115% | 0.834 | 0.833 |
| 306 | Collector | 8 | 300 | 1.00% | 18.332 | 543.06 | 3% | 1.606 | 0.084 |
| 307 | Collector | 8 | 194 | 0.90% | 14.427 | 511.06 | 3% | 1.433 | 0.077 |
| 308 | Interceptor | 15 | 519 | 0.30% | 308.081 | 1,669.73 | 19% | 2.313 | 0.364 |
| 309 | Collector | 8 | 592 | 0.30% | 0 | 312.40 | 0% | 0 | 0 |
| 310 | Collector | 8 | 320 | 0.30% | 2.707 | 293.67 | 1% | 0.587 | 0.045 |
| 311 | Collector | 8 | 295 | 0.40% | 1.927 | 361.46 | 1% | 0.612 | 0.035 |
| 312 | Collector | 8 | 336 | 0.30% | 1.927 | 297.633 | 1% | 0.535 | 0.038 |
| 313 | Collector | 8 | 327 | 0.40% | 1.927 | 361.356 | 1% | 0.612 | 0.035 |
| 314 | Collector | 8 | 250 | 0.50% | 0 | 387.30 | 0% | 0 | 0 |
| 315 | Collector | 8 | 302 | 0.40% | 1.927 | 330.05 | 1% | 0.574 | 0.037 |
| 316 | Collector | 8 | 316 | 0.60% | 1.927 | 421.78 | 1% | 0.681 | 0.033 |
| 317 | Collector | 8 | 297 | 0.20% | 1.927 | 234.77 | 1% | 0.453 | 0.043 |
| 318 | Collector | 8 | 341 | 0.30% | 1.927 | 311.88 | 1% | 0.552 | 0.038 |
| 320 | Collector | 8 | 348 | 0.50% | 17.182 | 367.84 | 5% | 1.199 | 0.098 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 321 | Collector | 8 | 226 | 0.40% | 3.902 | 349.173 | 1% | 0.74 | 0.05 |
| 322 | Collector | 8 | 173 | 0.40% | 5.782 | 335.813 | 2% | 0.811 | 0.061 |
| 323 | Collector | 8 | 137 | 0.30% | 5.782 | 315.656 | 2% | 0.777 | 0.063 |
| 324 | Collector | 8 | 265 | 0.50% | 1.927 | 386.51 | 1% | 0.641 | 0.034 |
| 325 | Collector | 8 | 601 | 0.30% | 1.927 | 319.387 | 1% | 0.561 | 0.037 |
| 327 | Collector | 8 | 504 | 0.30% | 5.415 | 296.818 | 2% | 0.73 | 0.063 |
| 328 | Collector | 8 | 305 | 0.30% | 2.84 | 315.794 | 1% | 0.627 | 0.045 |
| 331 | Collector | 8 | 337 | 0.50% | 3.407 | 378.877 | 1% | 0.752 | 0.045 |
| 332 | Collector | 8 | 234 | 0.30% | 34.133 | 292.031 | 12% | 1.247 | 0.154 |
| 333 | Collector | 8 | 52 | 0.80% | 34.133 | 482.646 | 7% | 1.779 | 0.12 |
| 334 | Collector | 8 | 159 | 0.40% | 34.133 | 351.029 | 10% | 1.421 | 0.14 |
| 335 | Collector | 8 | 271 | 0.20% | 31.013 | 258.253 | 12% | 1.112 | 0.156 |
| 336 | Collector | 8 | 105 | 0.40% | 30.047 | 331.329 | 9% | 1.314 | 0.136 |
| 337 | Collector | 8 | 293 | 0.40% | 2.812 | 364.399 | 1% | 0.69 | 0.042 |
| 338 | Collector | 8 | 355 | 0.30% | 0 | 318.991 | 0% | 0 | 0 |
| 339 | Collector | 8 | 496 | 0.30% | 0 | 312.363 | 0% | 0 | 0 |
| 340 | Interceptor | 15 | 304 | 0.20% | 310.614 | 1341.543 | 23% | 1.982 | 0.409 |
| 341 | Interceptor | 15 | 312 | 0.10% | 311.394 | 1037.86 | 30% | 1.647 | 0.469 |
| 342 | Interceptor | 15 | 335 | 0.10% | 395.819 | 886.702 | 45% | 1.564 | 0.585 |
| 343 | Interceptor | 15 | 302 | 0.30% | 395.819 | 1542.364 | 26% | 2.345 | 0.432 |
| 344 | Collector | 8 | 594 | 0.20% | 28.199 | 212.457 | 13% | 0.941 | 0.164 |
| 345 | Collector | 8 | 595 | 0.20% | 39.917 | 255.154 | 16% | 1.186 | 0.178 |
| 346 | Collector | 8 | 594 | 0.30% | 14.756 | 320.165 | 5% | 1.039 | 0.097 |
| 347 | Collector | 8 | 548 | 0.30% | 3.905 | 312.41 | 1% | 0.685 | 0.052 |
| 348 | Collector | 10 | 319 | -0.10% | 145.12 | | 100% | 0.593 | 0.833 |
| 349 | Collector | 12 | 595 | 0.20% | 58.252 | 757.989 | 8% | 1.273 | 0.188 |
| 350 | Collector | 12 | 327 | 0.10% | 87.961 | 532.931 | 17% | 1.118 | 0.275 |
| 351 | Collector | 12 | 268 | 0.70% | 87.961 | 1373.928 | 6% | 2.186 | 0.171 |
| 352 | Collector | 8 | 269 | 0.90% | 0 | 512.067 | 0% | 0 | 0 |
| 353 | Collector | 8 | 196 | 0.30% | 0 | 300.69 | 0% | 0 | 0 |
| 354 | Collector | 8 | 281 | 1.10% | 0 | 572.91 | 0% | 0 | 0 |
| 355 | Collector | 8 | 62 | -0.80% | 0 | | 100% | 0 | 0 |
| 356 | Collector | 8 | 146 | 1.80% | 2.159 | 719.73 | 0% | 1.022 | 0.027 |
| 357 | Interceptor | 10 | 180 | 0.30% | 80.993 | 561.2 | 14% | 1.631 | 0.214 |
| 358 | Collector | 8 | 103 | 0.10% | 7.815 | 185.636 | 4% | 0.587 | 0.093 |
| 359 | Collector | 8 | 307 | 0.80% | 3.855 | 491.052 | 1% | 0.935 | 0.042 |
| 360 | Collector | 8 | 235 | 0.40% | 8.907 | 362.832 | 3% | 0.975 | 0.072 |
| 361 | Collector | 8 | 262 | 0.20% | 20.31 | 268.308 | 8% | 1.009 | 0.124 |
| 362 | Collector | 8 | 247 | 0.40% | 19.53 | 355.319 | 6% | 1.216 | 0.106 |
| 363 | Collector | 8 | 217 | 0.30% | 0 | 312.301 | 0% | 0 | 0 |
| 364 | Collector | 8 | 326 | 0.30% | 6.615 | 320.65 | 2% | 0.818 | 0.066 |
| 365 | Collector | 8 | 217 | 0.40% | 0 | 331.679 | 0% | 0 | 0 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 366 | Interceptor | 10 | 290 | 0.50% | 71.618 | 723.288 | 10% | 1.884 | 0.177 |
| 367 | Collector | 8 | 361 | 0.40% | 3.125 | 341.421 | 1% | 0.681 | 0.045 |
| 368 | Collector | 8 | 87 | 0.00% | 6.161 | | 100% | 0.039 | 0.667 |
| 369 | Collector | 8 | 315 | 1.50% | 8.175 | 655.284 | 1% | 1.436 | 0.052 |
| 370 | Collector | 8 | 248 | 0.30% | 24.945 | 291.422 | 9% | 1.136 | 0.132 |
| 371 | Collector | 8 | 151 | -0.40% | 24.945 | | 100% | 0.159 | 0.667 |
| 372 | Interceptor | 10 | 403 | 0.20% | 204.183 | 415.62 | 49% | 1.69 | 0.412 |
| 373 | Interceptor | 10 | 402 | 0.10% | 204.183 | 343.895 | 59% | 1.465 | 0.462 |
| 374 | Collector | 8 | 297 | 0.10% | 2.258 | 182.894 | 1% | 0.4 | 0.052 |
| 375 | Collector | 8 | 592 | 0.10% | 14.756 | 192.832 | 8% | 0.728 | 0.125 |
| 376 | Collector | 10 | 595 | 0.20% | 181.612 | 482.674 | 38% | 1.832 | 0.354 |
| 377 | Collector | 10 | 595 | 0.50% | 88.557 | 689.043 | 13% | 1.936 | 0.202 |
| 378 | Collector | 12 | 566 | 0.40% | 2.384 | 1036.113 | 0% | 0.603 | 0.035 |
| 379 | Collector | 12 | 338 | 0.10% | 96.512 | 448.86 | 22% | 1.015 | 0.315 |
| 380 | Collector | 8 | 350 | 0.70% | 8.541 | 453.8 | 2% | 1.126 | 0.063 |
| 381 | Interceptor | 10 | 629 | 0.50% | 64.42 | 684.205 | 9% | 1.756 | 0.173 |
| 382 | Collector | 12 | 617 | 0.30% | 2.532 | 879.003 | 0% | 0.548 | 0.039 |
| 383 | Collector | 8 | 205 | 0.30% | 0 | 287.423 | 0% | 0 | 0 |
| 384 | Collector | 8 | 480 | 0.30% | 1.927 | 312.354 | 1% | 0.553 | 0.037 |
| 385 | Collector | 8 | 589 | 0.60% | 7.342 | 412.265 | 2% | 1.006 | 0.062 |
| 386 | Collector | 8 | 367 | 0.20% | 31.19 | 216.811 | 14% | 0.983 | 0.171 |
| 387 | Collector | 8 | 110 | 0.40% | 5.782 | 342.504 | 2% | 0.823 | 0.06 |
| 388 | Collector | 8 | 123 | 0.60% | 5.782 | 430.713 | 1% | 0.965 | 0.054 |
| 389 | Collector | 8 | 126 | 0.20% | 1.927 | 231.95 | 1% | 0.449 | 0.043 |
| 390 | Collector | 8 | 176 | 0.40% | 24.987 | 340.564 | 7% | 1.269 | 0.122 |
| 391 | Collector | 8 | 215 | 0.50% | 3.125 | 382.659 | 1% | 0.737 | 0.043 |
| 392 | Collector | 8 | 225 | 0.40% | 8.59 | 342.809 | 3% | 0.927 | 0.073 |
| 393 | Collector | 8 | 87 | -0.10% | 34.133 | | 100% | 0.218 | 0.667 |
| 394 | Collector | 8 | 157 | 0.40% | 2.812 | 328.605 | 1% | 0.642 | 0.044 |
| 395 | Collector | 8 | 240 | 0.40% | 36.05 | 324.547 | 11% | 1.366 | 0.15 |
| 396 | Collector | 8 | 80 | 0.00% | 0 | | 0% | 0 | 0 |
| 397 | Collector | 8 | 110 | 5.80% | 0 | 1305.235 | 0% | 0 | 0 |
| 398 | Interceptor | 8 | 94 | 0.40% | 417.219 | 1840.809 | 23% | 2.703 | 0.405 |
| 399 | Collector | 10 | 279 | 0.30% | 1.56 | 536.195 | 0% | 0.483 | 0.033 |
| 400 | Collector | 10 | 299 | 0.30% | 67.436 | 502.848 | 13% | 1.43 | 0.206 |
| 401 | Collector | 8 | 160 | 2.00% | 2.578 | 774.803 | 0% | 1.136 | 0.028 |
| 402 | Collector | 8 | 158 | 0.10% | 2.578 | 180.403 | 1% | 0.412 | 0.056 |
| 403 | Collector | 8 | 298 | 0.40% | 11.715 | 364.02 | 3% | 1.062 | 0.082 |
| 404 | Collector | 8 | 116 | 0.40% | 0 | 348.065 | 0% | 0 | 0 |
| 405 | Collector | 8 | 151 | 0.30% | 1.56 | 295.79 | 1% | 0.499 | 0.035 |
| 406 | Collector | 8 | 246 | 0.30% | 1.56 | 295.64 | 1% | 0.499 | 0.035 |
| 407 | Collector | 8 | 405 | 0.30% | 1.56 | 295.722 | 1% | 0.499 | 0.035 |

MODEL SCENARIO 1A
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 408 | Collector | 8 | 181 | 0.30% | 1.56 | 295.76 | 1% | 0.499 | 0.035 |
| 409 | Collector | 8 | 177 | 0.30% | 1.56 | 295.71 | 1% | 0.499 | 0.035 |
| 410 | Collector | 8 | 257 | 0.30% | 1.56 | 295.809 | 1% | 0.499 | 0.035 |
| 411 | Collector | 8 | 199 | 0.30% | 3.12 | 295.76 | 1% | 0.616 | 0.048 |
| 412 | Collector | 8 | 716 | 0.30% | 21.875 | 315.07 | 7% | 1.155 | 0.119 |
| 413 | Collector | 8 | 284 | 0.30% | 21.875 | 312.361 | 7% | 1.148 | 0.119 |
| 414 | Collector | 8 | 174 | 0.30% | 19.53 | 312.38 | 6% | 1.11 | 0.113 |
| 417 | Collector | 8 | 206 | 0.30% | 19.53 | 312.78 | 6% | 1.111 | 0.113 |
| 420 | Collector | 8 | 80 | 1.10% | 3.855 | 560.71 | 1% | 1.025 | 0.039 |
| 421 | Collector | 8 | 105 | 0.30% | 3.855 | 312.47 | 1% | 0.682 | 0.052 |
| 423 | Collector | 8 | 375 | 0.30% | 3.855 | 312.35 | 1% | 0.682 | 0.052 |
| 424 | Collector | 8 | 79 | 2.40% | 4.635 | 836.631 | 1% | 1.433 | 0.036 |
| 425 | Collector | 8 | 16 | 1.00% | 0 | 544.782 | 0% | 0 | 0 |
| 426 | Collector | 8 | 9 | 0.30% | 0 | 312.421 | 0% | 0 | 0 |
| 428 | Collector | 8 | 185 | 0.30% | 0 | 312.395 | 0% | 0 | 0 |
| 430 | Collector | 8 | 201 | 0.30% | 3.125 | 312.472 | 1% | 0.64 | 0.047 |
| 431 | Collector | 8 | 297 | 0.30% | 3.125 | 297.775 | 1% | 0.619 | 0.048 |
| 433 | Collector | 8 | 54 | 0.30% | 92.284 | 312.284 | 30% | 1.735 | 0.248 |
| 443 | Collector | 8 | 1195 | 0.30% | 24.945 | 312.392 | 8% | 1.194 | 0.127 |
| 447 | Interceptor | 10 | 68 | 0.20% | 204.183 | 484.75 | 42% | 1.895 | 0.377 |
| 449 | Interceptor | 10 | 5 | 0.40% | 204.183 | 623.59 | 33% | 2.28 | 0.328 |
| 465 | Collector | 8 | 491 | 0.30% | 0 | 312.398 | 0% | 0 | 0 |
| 467 | Collector | 8 | 157 | 0.30% | 0 | 312.418 | 0% | 0 | 0 |
| 471 | Collector | 8 | 281 | 0.30% | 0 | 312.36 | 0% | 0 | 0 |
| 479 | Collector | 8 | 194 | 0.30% | 0 | 312.43 | 0% | 0 | 0 |
| 495 | Collector | 8 | 118 | 0.80% | 2.159 | 483.212 | 0% | 0.775 | 0.032 |
| 501 | Well Connection | 10 | 5 | 0.90% | 308.081 | 935.39 | 33% | 3.426 | 0.329 |
| 515 | Interceptor | 36 | 10 | 0.00% | 417.219 | 949.207 | 44% | 0.29 | 1.392 |
| 517 | Interceptor | 36 | 10 | 0.00% | 204.183 | 949.207 | 22% | 0.238 | 0.945 |
| 519 | Collector | 8 | 654 | 0.10% | 6.607 | 207.93 | 3% | 0.604 | 0.081 |
| 521 | Collector | 8 | 306 | 0.50% | 2.578 | 368.686 | 1% | 0.678 | 0.04 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 1 | Interceptor | 10 | 599 | 0.40% | 33.74 | 610.42 | 6% | 1.34 | 0.13 |
| 2 | Collector | 8 | 623 | 0.40% | 27.99 | 344.04 | 8% | 1.32 | 0.13 |
| 3 | Collector | 8 | 595 | 0.40% | 18.78 | 334.25 | 6% | 1.15 | 0.11 |
| 4 | Collector | 8 | 339 | 0.30% | 0.00 | 312.33 | 0% | 0.00 | 0.00 |
| 6 | Collector | 8 | 392 | 0.40% | 2.50 | 331.04 | 1% | 0.62 | 0.04 |
| 7 | Collector | 8 | 305 | 0.40% | 10.00 | 331.85 | 3% | 0.95 | 0.08 |
| 8 | Collector | 8 | 628 | 0.50% | 123.37 | 390.36 | 32% | 2.21 | 0.26 |
| 9 | Collector | 8 | 333 | 0.60% | 8.75 | 413.46 | 2% | 1.06 | 0.07 |
| 10 | Collector | 12 | 357 | 0.20% | 154.42 | 718.56 | 22% | 1.62 | 0.32 |
| 11 | Collector | 8 | 692 | 0.10% | 1.18 | 135.23 | 1% | 0.27 | 0.04 |
| 12 | Collector | 8 | 601 | 0.10% | 25.58 | 202.98 | 13% | 0.89 | 0.16 |
| 14 | Collector | 8 | 369 | 0.50% | 5.50 | 401.50 | 1% | 0.91 | 0.06 |
| 15 | Collector | 8 | 215 | 0.30% | 0.00 | 312.40 | 0% | 0.00 | 0.00 |
| 16 | Collector | 8 | 236 | 0.50% | 17.49 | 395.57 | 4% | 1.27 | 0.10 |
| 17 | Collector | 8 | 381 | 0.40% | 30.19 | 347.29 | 9% | 1.36 | 0.13 |
| 18 | Collector | 8 | 264 | 0.40% | 2.50 | 355.61 | 1% | 0.65 | 0.04 |
| 19 | Collector | 8 | 218 | 0.30% | 0.00 | 318.19 | 0% | 0.00 | 0.00 |
| 20 | Collector | 8 | 238 | 1.20% | 2.29 | 593.00 | 0% | 0.91 | 0.03 |
| 21 | Collector | 8 | 146 | 0.40% | 0.00 | 361.84 | 0% | 0.00 | 0.00 |
| 22 | Collector | 8 | 299 | 0.30% | 1.45 | 281.99 | 1% | 0.47 | 0.03 |
| 23 | Collector | 8 | 293 | 0.50% | 5.00 | 365.98 | 1% | 0.82 | 0.06 |
| 24 | Collector | 8 | 307 | 0.40% | 0.00 | 358.21 | 0% | 0.00 | 0.00 |
| 25 | Collector | 8 | 243 | 0.30% | 0.00 | 312.45 | 0% | 0.00 | 0.00 |
| 26 | Collector | 8 | 202 | 0.30% | 0.00 | 312.34 | 0% | 0.00 | 0.00 |
| 27 | Collector | 8 | 454 | 0.30% | 0.00 | 312.38 | 0% | 0.00 | 0.00 |
| 28 | Collector | 8 | 121 | 0.30% | 0.00 | 312.24 | 0% | 0.00 | 0.00 |
| 29 | Collector | 8 | 133 | 0.30% | 0.00 | 312.48 | 0% | 0.00 | 0.00 |
| 30 | Collector | 8 | 328 | 0.40% | 5.00 | 351.80 | 1% | 0.80 | 0.06 |
| 31 | Collector | 8 | 301 | 0.40% | 141.41 | 338.13 | 42% | 2.06 | 0.30 |
| 32 | Collector | 8 | 336 | 0.30% | 8.66 | 312.32 | 3% | 0.87 | 0.08 |
| 33 | Collector | 8 | 226 | 0.30% | 0.00 | 312.39 | 0% | 0.00 | 0.00 |
| 34 | Collector | 8 | 329 | 0.90% | 3.75 | 522.71 | 1% | 0.97 | 0.04 |
| 35 | Collector | 8 | 144 | 0.30% | 3.08 | 312.28 | 1% | 0.64 | 0.05 |
| 36 | Collector | 8 | 612 | 0.40% | 32.99 | 364.53 | 9% | 1.45 | 0.14 |
| 37 | Collector | 10 | 328 | 0.40% | 133.83 | 650.44 | 21% | 2.09 | 0.26 |
| 38 | Collector | 8 | 264 | 0.20% | 6.25 | 264.73 | 2% | 0.70 | 0.07 |
| 39 | Collector | 8 | 248 | 0.50% | 3.08 | 398.51 | 1% | 0.76 | 0.04 |
| 40 | Collector | 8 | 360 | 0.30% | 9.25 | 277.52 | 3% | 0.82 | 0.08 |
| 41 | Collector | 8 | 373 | 0.20% | 1.47 | 241.61 | 1% | 0.43 | 0.04 |
| 43 | Collector | 12 | 593 | 0.20% | 68.30 | 678.74 | 10% | 1.23 | 0.21 |
| 44 | Collector | 12 | 569 | 0.30% | 0.00 | 921.01 | 0% | 0.00 | 0.00 |
| 45 | Collector | 8 | 334 | 0.30% | 0.00 | 312.43 | 0% | 0.00 | 0.00 |
| 46 | Collector | 8 | 554 | 0.20% | 26.24 | 269.35 | 10% | 1.09 | 0.14 |
| 47 | Collector | 8 | 625 | 0.30% | 0.00 | 312.36 | 0% | 0.00 | 0.00 |
| 48 | Collector | 8 | 315 | 0.30% | 29.99 | 272.47 | 11% | 1.14 | 0.15 |
| 49 | Collector | 6 | 555 | 0.30% | 5.12 | 141.63 | 4% | 0.76 | 0.07 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 50 | Collector | 8 | 321 | 0.50% | 5.00 | 378.75 | 1% | 0.84 | 0.05 |
| 51 | Collector | 8 | 632 | 0.30% | 0.00 | 312.37 | 0% | 0.00 | 0.00 |
| 52 | Interceptor | 10 | 599 | 0.20% | 21.24 | 465.60 | 5% | 0.96 | 0.12 |
| 53 | Collector | 8 | 620 | 0.10% | 8.35 | 129.79 | 6% | 0.47 | 0.12 |
| 54 | Collector | 8 | 410 | 0.30% | 0.00 | 312.34 | 0% | 0.00 | 0.00 |
| 55 | Collector | 8 | 623 | 0.10% | 10.82 | 192.52 | 6% | 0.66 | 0.11 |
| 56 | Collector | 8 | 627 | 0.40% | 2.50 | 361.02 | 1% | 0.66 | 0.04 |
| 57 | Collector | 8 | 354 | 0.30% | 3.08 | 312.34 | 1% | 0.64 | 0.05 |
| 58 | Collector | 8 | 429 | 0.30% | 0.00 | 312.38 | 0% | 0.00 | 0.00 |
| 59 | Interceptor | 10 | 596 | 0.40% | 64.32 | 589.70 | 11% | 1.58 | 0.19 |
| 60 | Interceptor | 15 | 644 | 0.10% | 496.98 | 1060.32 | 47% | 1.89 | 0.60 |
| 61 | Collector | 8 | 349 | 0.40% | 0.00 | 361.01 | 0% | 0.00 | 0.00 |
| 62 | Collector | 8 | 271 | 0.40% | 11.25 | 345.84 | 3% | 1.01 | 0.08 |
| 64 | Collector | 8 | 157 | 0.40% | 3.75 | 351.35 | 1% | 0.74 | 0.05 |
| 65 | Collector | 8 | 401 | 0.40% | 42.48 | 344.74 | 12% | 1.50 | 0.16 |
| 66 | Collector | 8 | 169 | 0.60% | 44.97 | 408.96 | 11% | 1.72 | 0.15 |
| 67 | Interceptor | 10 | 41 | -0.10% | 229.31 | | 100% | 0.94 | 0.83 |
| 68 | Interceptor | 10 | 397 | 0.20% | 223.07 | 424.17 | 53% | 1.76 | 0.43 |
| 69 | Collector | 8 | 300 | 0.40% | 19.25 | 342.34 | 6% | 1.18 | 0.11 |
| 70 | Collector | 8 | 217 | 0.30% | 0.00 | 312.30 | 0% | 0.00 | 0.00 |
| 73 | Collector | 8 | 238 | 0.50% | 3.08 | 392.86 | 1% | 0.75 | 0.04 |
| 74 | Collector | 8 | 347 | 0.40% | 25.00 | 355.76 | 7% | 1.31 | 0.12 |
| 75 | Collector | 8 | 236 | 0.40% | 7.50 | 363.69 | 2% | 0.93 | 0.07 |
| 76 | Collector | 8 | 180 | 0.50% | 6.25 | 373.94 | 2% | 0.90 | 0.06 |
| 77 | Collector | 8 | 383 | 0.40% | 10.00 | 348.23 | 3% | 0.98 | 0.08 |
| 78 | Collector | 8 | 257 | 0.30% | 2.50 | 285.58 | 1% | 0.56 | 0.04 |
| 79 | Interceptor | 12 | 629 | 0.20% | 68.30 | 715.39 | 10% | 1.28 | 0.21 |
| 80 | Collector | 8 | 903 | 0.30% | 6.17 | 300.21 | 2% | 0.77 | 0.07 |
| 81 | Collector | 8 | 649 | 0.30% | 33.74 | 303.62 | 11% | 1.28 | 0.15 |
| 83 | Collector | 8 | 239 | 0.20% | 39.91 | 241.99 | 17% | 1.14 | 0.18 |
| 84 | Collector | 8 | 1391 | 0.30% | 39.91 | 289.02 | 14% | 1.30 | 0.17 |
| 85 | Collector | 8 | 400 | 0.30% | 39.91 | 314.04 | 13% | 1.37 | 0.16 |
| 86 | Collector | 8 | 327 | 0.40% | 4.99 | 343.03 | 2% | 0.79 | 0.06 |
| 87 | Collector | 8 | 223 | 0.40% | 37.48 | 344.00 | 11% | 1.44 | 0.15 |
| 88 | Collector | 8 | 173 | 0.70% | 2.50 | 459.78 | 1% | 0.78 | 0.04 |
| 89 | Interceptor | 10 | 400 | 0.00% | 326.69 | 180.37 | 181% | 1.34 | 0.83 |
| 90 | Interceptor | 10 | 741 | 0.20% | 276.79 | 436.00 | 64% | 1.89 | 0.48 |
| 91 | Collector | 8 | 373 | 0.70% | 1.25 | 445.82 | 0% | 0.62 | 0.03 |
| 92 | Collector | 8 | 240 | 0.40% | 15.50 | 360.92 | 4% | 1.15 | 0.09 |
| 93 | Collector | 8 | 340 | 0.30% | 0.00 | 312.65 | 0% | 0.00 | 0.00 |
| 94 | Collector | 8 | 217 | 0.50% | 5.00 | 367.78 | 1% | 0.83 | 0.05 |
| 95 | Interceptor | 10 | 398 | 0.20% | 118.34 | 430.72 | 28% | 1.50 | 0.30 |
| 96 | Collector | 8 | 262 | 0.20% | 78.36 | 243.08 | 32% | 1.38 | 0.26 |
| 97 | Collector | 8 | 361 | 0.40% | 11.25 | 338.93 | 3% | 1.00 | 0.08 |
| 98 | Collector | 8 | 417 | 0.30% | 18.74 | 298.78 | 6% | 1.06 | 0.11 |
| 99 | Collector | 8 | 390 | 0.20% | 6.25 | 226.43 | 3% | 0.63 | 0.08 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 100 | Collector | 8 | 449 | 0.40% | 5.00 | 338.22 | 2% | 0.78 | 0.06 |
| 101 | Collector | 8 | 399 | 1.90% | 0.00 | 746.25 | 0% | 0.00 | 0.00 |
| 102 | Collector | 8 | 353 | 0.50% | 0.00 | 379.90 | 0% | 0.00 | 0.00 |
| 103 | Collector | 8 | 235 | 2.80% | 0.00 | 908.81 | 0% | 0.00 | 0.00 |
| 104 | Collector | 8 | 588 | 2.00% | 19.33 | 770.89 | 3% | 2.09 | 0.07 |
| 105 | Collector | 8 | 301 | 0.00% | 3.74 | | 100% | 0.02 | 0.67 |
| 106 | Collector | 8 | 432 | 0.20% | 1.25 | 261.73 | 1% | 0.43 | 0.03 |
| 107 | Collector | 8 | 872 | 0.40% | 2.50 | 362.99 | 1% | 0.66 | 0.04 |
| 108 | Collector | 8 | 407 | 0.30% | 3.75 | 299.62 | 1% | 0.66 | 0.05 |
| 109 | Collector | 8 | 236 | 0.70% | 0.00 | 443.20 | 0% | 0.00 | 0.00 |
| 110 | Collector | 8 | 491 | 0.30% | 0.00 | 312.40 | 0% | 0.00 | 0.00 |
| 111 | Collector | 8 | 299 | 0.00% | 1.33 | 58.03 | 2% | 0.15 | 0.07 |
| 112 | Collector | 8 | 581 | 0.30% | 0.00 | 312.36 | 0% | 0.00 | 0.00 |
| 113 | Collector | 8 | 295 | 0.60% | 25.37 | 420.12 | 6% | 1.48 | 0.11 |
| 114 | Collector | 8 | 157 | 0.30% | 0.00 | 312.42 | 0% | 0.00 | 0.00 |
| 115 | Collector | 8 | 508 | 0.30% | 41.62 | 312.38 | 13% | 1.39 | 0.16 |
| 116 | Collector | 8 | 390 | 0.40% | 109.46 | 362.25 | 30% | 2.03 | 0.25 |
| 117 | Collector | 8 | 269 | 0.40% | 0.00 | 343.67 | 0% | 0.00 | 0.00 |
| 118 | Collector | 8 | 89 | 0.60% | 0.00 | 418.46 | 0% | 0.00 | 0.00 |
| 119 | Collector | 8 | 157 | 0.50% | 0.00 | 380.71 | 0% | 0.00 | 0.00 |
| 121 | Collector | 8 | 240 | 0.40% | 1.55 | 321.81 | 1% | 0.53 | 0.03 |
| 122 | Collector | 8 | 724 | 0.30% | 0.00 | 312.37 | 0% | 0.00 | 0.00 |
| 123 | Collector | 8 | 477 | 0.20% | 1.25 | 211.68 | 1% | 0.37 | 0.04 |
| 124 | Collector | 8 | 287 | 0.50% | 145.16 | 369.47 | 39% | 2.22 | 0.29 |
| 125 | Collector | 10 | 624 | 0.10% | 98.19 | 356.32 | 28% | 1.24 | 0.30 |
| 126 | Collector | 8 | 303 | 0.40% | 6.17 | 360.50 | 2% | 0.87 | 0.06 |
| 127 | Collector | 8 | 177 | 0.50% | 6.25 | 376.98 | 2% | 0.90 | 0.06 |
| 128 | Collector | 8 | 289 | 0.30% | 2.50 | 317.20 | 1% | 0.60 | 0.04 |
| 129 | Collector | 8 | 270 | 0.30% | 0.00 | 312.47 | 0% | 0.00 | 0.00 |
| 130 | Collector | 8 | 915 | 0.20% | 1.61 | 264.22 | 1% | 0.47 | 0.04 |
| 131 | Collector | 8 | 61 | 0.30% | 0.00 | 312.02 | 0% | 0.00 | 0.00 |
| 132 | Collector | 8 | 194 | 0.30% | 0.00 | 312.43 | 0% | 0.00 | 0.00 |
| 133 | Collector | 12 | 566 | 0.20% | 148.17 | 658.48 | 23% | 1.51 | 0.32 |
| 134 | Collector | 12 | 339 | 0.30% | 0.00 | 921.06 | 0% | 0.00 | 0.00 |
| 135 | Collector | 12 | 467 | 0.30% | 0.00 | 921.01 | 0% | 0.00 | 0.00 |
| 137 | Collector | 8 | 283 | 1.30% | 0.00 | 620.49 | 0% | 0.00 | 0.00 |
| 138 | Interceptor | 10 | 322 | 0.30% | 0.00 | 580.47 | 0% | 0.00 | 0.00 |
| 139 | Collector | 8 | 300 | 0.20% | 6.25 | 245.55 | 3% | 0.67 | 0.07 |
| 140 | Collector | 8 | 185 | 1.30% | 0.00 | 612.68 | 0% | 0.00 | 0.00 |
| 141 | Collector | 8 | 280 | 0.40% | 1.25 | 332.04 | 0% | 0.51 | 0.03 |
| 142 | Collector | 8 | 297 | 0.60% | 6.25 | 428.56 | 2% | 0.99 | 0.06 |
| 143 | Collector | 8 | 277 | 0.70% | 14.33 | 443.92 | 3% | 1.30 | 0.08 |
| 144 | Collector | 8 | 335 | 4.50% | 18.08 | 1156.83 | 2% | 2.71 | 0.06 |
| 145 | Collector | 8 | 343 | 0.30% | 19.33 | 285.82 | 7% | 1.04 | 0.12 |
| 146 | Collector | 8 | 60 | 2.50% | 23.08 | 864.17 | 3% | 2.38 | 0.08 |
| 147 | Collector | 8 | 46 | 5.30% | 23.08 | 1255.60 | 2% | 3.09 | 0.06 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 148 | Collector | 8 | 112 | 2.20% | 0.00 | 808.44 | 0% | 0.00 | 0.00 |
| 149 | Collector | 8 | 123 | 1.90% | 0.00 | 751.34 | 0% | 0.00 | 0.00 |
| 150 | Collector | 8 | 293 | 0.00% | 0.00 | 52.23 | 0% | 0.00 | 0.00 |
| 151 | Collector | 8 | 225 | 0.40% | 0.00 | 341.32 | 0% | 0.00 | 0.00 |
| 152 | Collector | 8 | 235 | 0.50% | 0.00 | 365.30 | 0% | 0.00 | 0.00 |
| 153 | Collector | 8 | 319 | 0.40% | 14.87 | 324.50 | 5% | 1.05 | 0.10 |
| 154 | Collector | 8 | 186 | 0.20% | 18.62 | 267.55 | 7% | 0.98 | 0.12 |
| 155 | Collector | 8 | 336 | 0.20% | 3.75 | 270.59 | 1% | 0.61 | 0.06 |
| 156 | Collector | 8 | 262 | 0.30% | 6.12 | 296.36 | 2% | 0.76 | 0.07 |
| 157 | Collector | 8 | 237 | 1.30% | 3.74 | 617.27 | 1% | 1.09 | 0.04 |
| 158 | Collector | 8 | 514 | 0.30% | 1.25 | 310.27 | 0% | 0.48 | 0.03 |
| 159 | Collector | 8 | 419 | 0.20% | 0.00 | 251.52 | 0% | 0.00 | 0.00 |
| 160 | Collector | 8 | 402 | 0.50% | 1.25 | 398.16 | 0% | 0.57 | 0.03 |
| 161 | Collector | 8 | 365 | 0.60% | 1.25 | 417.72 | 0% | 0.59 | 0.03 |
| 162 | Collector | 8 | 297 | 0.00% | 1.25 | | 100% | 0.01 | 0.67 |
| 163 | Collector | 8 | 302 | 0.30% | 1.25 | 314.58 | 0% | 0.49 | 0.03 |
| 164 | Collector | 8 | 301 | 0.20% | 1.25 | 270.03 | 1% | 0.44 | 0.03 |
| 165 | Collector | 8 | 301 | 0.20% | 33.08 | 254.27 | 13% | 1.12 | 0.16 |
| 166 | Collector | 8 | 352 | 0.20% | 39.32 | 225.77 | 17% | 1.08 | 0.19 |
| 167 | Collector | 8 | 398 | 0.20% | 43.08 | 212.10 | 20% | 1.06 | 0.20 |
| 170 | Collector | 8 | 358 | 0.30% | 13.45 | 277.10 | 5% | 0.91 | 0.10 |
| 172 | Collector | 8 | 173 | 0.40% | 2.50 | 360.34 | 1% | 0.66 | 0.04 |
| 173 | Collector | 8 | 114 | 0.50% | 1.25 | 392.86 | 0% | 0.57 | 0.03 |
| 174 | Collector | 8 | 247 | 0.50% | 3.74 | 384.93 | 1% | 0.78 | 0.05 |
| 175 | Collector | 8 | 210 | 0.40% | 8.74 | 359.88 | 2% | 0.96 | 0.07 |
| 176 | Collector | 8 | 133 | 0.20% | 13.04 | 270.83 | 5% | 0.89 | 0.10 |
| 178 | Collector | 8 | 397 | 0.20% | 54.61 | 257.80 | 21% | 1.31 | 0.21 |
| 179 | Collector | 8 | 352 | 0.30% | 60.86 | 291.28 | 21% | 1.47 | 0.21 |
| 180 | Collector | 8 | 395 | 0.30% | 67.11 | 278.18 | 24% | 1.46 | 0.22 |
| 181 | Collector | 8 | 137 | 0.60% | 98.35 | 414.02 | 24% | 2.17 | 0.22 |
| 182 | Collector | 8 | 128 | 1.10% | 1.25 | 576.35 | 0% | 0.74 | 0.02 |
| 183 | Collector | 8 | 416 | 0.60% | 1.25 | 423.62 | 0% | 0.60 | 0.03 |
| 184 | Interceptor | 10 | 307 | 0.20% | 99.60 | 425.24 | 23% | 1.42 | 0.27 |
| 185 | Collector | 8 | 384 | 0.50% | 0.00 | 397.73 | 0% | 0.00 | 0.00 |
| 186 | Collector | 8 | 400 | 0.50% | 0.00 | 399.09 | 0% | 0.00 | 0.00 |
| 187 | Collector | 8 | 298 | 0.50% | 5.00 | 372.30 | 1% | 0.83 | 0.05 |
| 188 | Interceptor | 10 | 595 | 0.10% | 24.99 | 323.11 | 8% | 0.78 | 0.16 |
| 189 | Collector | 10 | 601 | 0.60% | 15.12 | 775.37 | 2% | 1.25 | 0.08 |
| 191 | Collector | 8 | 298 | 0.30% | 20.00 | 319.01 | 6% | 1.14 | 0.11 |
| 192 | Collector | 8 | 295 | 0.30% | 15.00 | 294.24 | 5% | 0.98 | 0.10 |
| 193 | Collector | 8 | 295 | 0.20% | 15.00 | 262.02 | 6% | 0.91 | 0.11 |
| 194 | Collector | 8 | 627 | 0.20% | 42.54 | 240.21 | 18% | 1.16 | 0.19 |
| 195 | Collector | 8 | 592 | 0.40% | 33.80 | 348.30 | 10% | 1.41 | 0.14 |
| 196 | Collector | 8 | 270 | 0.30% | 21.75 | 281.96 | 8% | 1.07 | 0.13 |
| 197 | Collector | 8 | 298 | 0.80% | 0.00 | 471.48 | 0% | 0.00 | 0.00 |
| 198 | Collector | 8 | 310 | 0.80% | 13.75 | 487.04 | 3% | 1.37 | 0.08 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 199 | Collector | 8 | 307 | 0.40% | 1.33 | 345.43 | 0% | 0.53 | 0.03 |
| 200 | Collector | 8 | 306 | 0.30% | 31.62 | 316.37 | 10% | 1.29 | 0.14 |
| 201 | Collector | 8 | 169 | 0.30% | 0.00 | 312.46 | 0% | 0.00 | 0.00 |
| 202 | Collector | 8 | 58 | 0.30% | 0.00 | 312.13 | 0% | 0.00 | 0.00 |
| 203 | Collector | 8 | 293 | 0.00% | 0.20 | 52.22 | 0% | 0.08 | 0.03 |
| 204 | Collector | 8 | 211 | 0.50% | 18.04 | 368.20 | 5% | 1.22 | 0.10 |
| 205 | Collector | 8 | 234 | 0.30% | 63.93 | 295.70 | 22% | 1.51 | 0.21 |
| 206 | Collector | 8 | 226 | 0.40% | 0.00 | 363.86 | 0% | 0.00 | 0.00 |
| 207 | Collector | 8 | 231 | 0.40% | 72.67 | 325.67 | 22% | 1.67 | 0.21 |
| 208 | Collector | 8 | 189 | 1.50% | 23.04 | 656.92 | 4% | 1.97 | 0.09 |
| 209 | Collector | 8 | 111 | 0.50% | 101.96 | 373.85 | 27% | 2.03 | 0.24 |
| 210 | Collector | 8 | 66 | -3.60% | 106.96 | | 100% | 0.68 | 0.67 |
| 211 | Collector | 8 | 134 | 0.40% | 2.50 | 362.61 | 1% | 0.66 | 0.04 |
| 212 | Collector | 8 | 46 | 0.10% | 109.46 | 194.99 | 56% | 1.28 | 0.36 |
| 213 | Collector | 8 | 320 | 0.40% | 110.91 | 346.94 | 32% | 1.97 | 0.26 |
| 214 | Collector | 8 | 310 | 0.40% | 117.08 | 332.98 | 35% | 1.94 | 0.27 |
| 215 | Collector | 8 | 291 | 0.40% | 123.32 | 364.24 | 34% | 2.10 | 0.27 |
| 216 | Collector | 8 | 293 | 0.30% | 3.08 | 312.35 | 1% | 0.64 | 0.05 |
| 217 | Collector | 8 | 352 | 0.50% | 0.00 | 380.83 | 0% | 0.00 | 0.00 |
| 218 | Collector | 8 | 37 | -0.20% | 0.00 | | 100% | 0.00 | 0.00 |
| 219 | Interceptor | 10 | 400 | 0.30% | 102.10 | 522.29 | 20% | 1.66 | 0.25 |
| 220 | Interceptor | 10 | 400 | 0.10% | 103.35 | 357.52 | 29% | 1.26 | 0.31 |
| 221 | Interceptor | 10 | 399 | 0.20% | 103.35 | 439.33 | 24% | 1.47 | 0.28 |
| 222 | Interceptor | 10 | 401 | 0.10% | 105.84 | 285.27 | 37% | 1.08 | 0.35 |
| 223 | Collector | 8 | 321 | 0.30% | 0.00 | 283.86 | 0% | 0.00 | 0.00 |
| 224 | Interceptor | 10 | 625 | 0.10% | 28.74 | 323.93 | 9% | 0.82 | 0.17 |
| 225 | Interceptor | 10 | 597 | 0.30% | 43.74 | 580.45 | 8% | 1.40 | 0.16 |
| 226 | Collector | 8 | 525 | 0.30% | 0.00 | 312.36 | 0% | 0.00 | 0.00 |
| 227 | Collector | 8 | 597 | 0.20% | 26.70 | 240.27 | 11% | 1.01 | 0.15 |
| 228 | Collector | 8 | 630 | 0.40% | 23.35 | 362.92 | 6% | 1.30 | 0.12 |
| 229 | Collector | 8 | 595 | 0.40% | 17.06 | 342.18 | 5% | 1.14 | 0.10 |
| 230 | Collector | 8 | 312 | 0.20% | 44.99 | 240.64 | 19% | 1.18 | 0.20 |
| 231 | Collector | 8 | 319 | 0.30% | 38.74 | 289.66 | 13% | 1.29 | 0.17 |
| 232 | Collector | 8 | 51 | 2.10% | 37.50 | 788.28 | 5% | 2.58 | 0.10 |
| 234 | Collector | 8 | 628 | 0.20% | 12.97 | 260.26 | 5% | 0.87 | 0.10 |
| 235 | Collector | 8 | 628 | 0.20% | 64.15 | 235.20 | 27% | 1.28 | 0.24 |
| 236 | Collector | 8 | 460 | 0.30% | 0.00 | 312.39 | 0% | 0.00 | 0.00 |
| 237 | Collector | 10 | 602 | 0.20% | 87.62 | 459.59 | 19% | 1.45 | 0.25 |
| 238 | Collector | 10 | 250 | 0.30% | 101.65 | 533.17 | 19% | 1.68 | 0.25 |
| 239 | Collector | 10 | 298 | 0.10% | 104.15 | 361.58 | 29% | 1.28 | 0.31 |
| 240 | Collector | 10 | 302 | 0.60% | 106.65 | 768.51 | 14% | 2.21 | 0.21 |
| 241 | Collector | 8 | 278 | 0.20% | 2.50 | 219.51 | 1% | 0.47 | 0.05 |
| 242 | Collector | 8 | 124 | 0.40% | 6.25 | 336.82 | 2% | 0.83 | 0.06 |
| 243 | Collector | 8 | 297 | 0.40% | 141.41 | 349.27 | 41% | 2.11 | 0.30 |
| 245 | Collector | 8 | 577 | -0.80% | 6.17 | | 100% | 0.04 | 0.67 |
| 246 | Collector | 8 | 327 | 0.30% | 6.17 | 319.90 | 2% | 0.80 | 0.06 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 247 | Collector | 8 | 287 | 0.50% | 141.41 | 376.67 | 38% | 2.23 | 0.28 |
| 250 | Collector | 8 | 70 | 0.90% | 3.08 | 503.67 | 1% | 0.89 | 0.04 |
| 251 | Collector | 8 | 111 | 0.40% | 11.74 | 348.82 | 3% | 1.03 | 0.08 |
| 252 | Interceptor | 10 | 399 | 0.20% | 122.09 | 406.07 | 30% | 1.45 | 0.31 |
| 253 | Interceptor | 10 | 163 | 0.10% | 124.59 | 348.53 | 36% | 1.31 | 0.34 |
| 256 | Collector | 10 | 595 | 0.40% | 27.05 | 660.49 | 4% | 1.33 | 0.12 |
| 257 | Collector | 10 | 59 | 0.90% | 0.00 | 912.97 | 0% | 0.00 | 0.00 |
| 258 | Interceptor | 12 | 625 | 0.20% | 362.80 | 676.66 | 54% | 1.95 | 0.52 |
| 259 | Collector | 8 | 207 | 0.20% | 0.00 | 267.51 | 0% | 0.00 | 0.00 |
| 260 | Collector | 8 | 183 | 0.40% | 3.08 | 348.47 | 1% | 0.69 | 0.04 |
| 261 | Collector | 10 | 278 | 0.50% | 236.31 | 695.52 | 34% | 2.57 | 0.34 |
| 262 | Collector | 8 | 629 | 0.10% | 45.70 | 204.39 | 22% | 1.05 | 0.21 |
| 263 | Collector | 8 | 280 | 0.40% | 3.66 | 334.80 | 1% | 0.71 | 0.05 |
| 266 | Collector | 10 | 299 | 0.40% | 114.15 | 594.10 | 19% | 1.87 | 0.25 |
| 267 | Collector | 10 | 302 | 0.30% | 115.39 | 509.59 | 23% | 1.68 | 0.27 |
| 268 | Collector | 10 | 297 | 0.30% | 131.34 | 544.96 | 24% | 1.83 | 0.28 |
| 269 | Interceptor | 8 | 85 | 0.40% | 667.55 | 1840.34 | 36% | 3.08 | 0.52 |
| 270 | Collector | 8 | 270 | 0.30% | 3.75 | 294.98 | 1% | 0.65 | 0.05 |
| 272 | Collector | 8 | 162 | 0.50% | 3.75 | 398.72 | 1% | 0.80 | 0.05 |
| 273 | Collector | 8 | 101 | 0.50% | 12.50 | 381.05 | 3% | 1.12 | 0.08 |
| 274 | Collector | 8 | 218 | 0.50% | 52.50 | 369.13 | 14% | 1.67 | 0.17 |
| 275 | Collector | 8 | 272 | 0.40% | 16.24 | 358.20 | 5% | 1.16 | 0.10 |
| 276 | Collector | 8 | 390 | 0.50% | 15.50 | 379.58 | 4% | 1.19 | 0.09 |
| 277 | Collector | 8 | 171 | 0.80% | 17.99 | 495.97 | 4% | 1.50 | 0.09 |
| 278 | Interceptor | 10 | 238 | 0.20% | 124.59 | 453.71 | 28% | 1.58 | 0.30 |
| 279 | Interceptor | 10 | 399 | 0.10% | 150.08 | 275.88 | 54% | 1.15 | 0.44 |
| 280 | Interceptor | 10 | 363 | 0.20% | 224.32 | 433.58 | 52% | 1.79 | 0.43 |
| 281 | Collector | 8 | 201 | 0.50% | 20.50 | 379.21 | 5% | 1.29 | 0.11 |
| 282 | Interceptor | 10 | 37 | 0.00% | 150.08 | 170.30 | 88% | 0.79 | 0.61 |
| 283 | Collector | 8 | 286 | 0.50% | 3.74 | 383.12 | 1% | 0.78 | 0.05 |
| 284 | Collector | 8 | 196 | -0.40% | 1.25 | | 100% | 0.01 | 0.67 |
| 285 | Collector | 8 | 181 | 0.40% | 1.25 | 357.95 | 0% | 0.53 | 0.03 |
| 286 | Collector | 8 | 141 | 0.40% | 15.50 | 350.15 | 4% | 1.12 | 0.10 |
| 288 | Collector | 8 | 517 | 0.30% | 33.74 | 303.73 | 11% | 1.28 | 0.15 |
| 289 | Collector | 8 | 216 | 0.30% | 33.74 | 316.27 | 11% | 1.32 | 0.15 |
| 290 | Collector | 8 | 301 | 0.40% | 6.17 | 333.83 | 2% | 0.82 | 0.06 |
| 291 | Collector | 8 | 106 | 0.30% | 39.91 | 314.01 | 13% | 1.37 | 0.16 |
| 292 | Collector | 8 | 399 | -0.10% | 0.00 | | 100% | 0.00 | 0.00 |
| 293 | Collector | 8 | 159 | 0.70% | 39.91 | 454.08 | 9% | 1.79 | 0.13 |
| 295 | Collector | 8 | 401 | 0.20% | 39.91 | 214.64 | 19% | 1.05 | 0.20 |
| 296 | Collector | 8 | 398 | 0.20% | 39.91 | 231.83 | 17% | 1.11 | 0.19 |
| 297 | Collector | 8 | 326 | 0.40% | 2.50 | 337.53 | 1% | 0.63 | 0.04 |
| 298 | Collector | 8 | 275 | 0.40% | 9.99 | 345.27 | 3% | 0.98 | 0.08 |
| 299 | Collector | 8 | 380 | 0.10% | 49.90 | 124.10 | 40% | 0.75 | 0.29 |
| 300 | Collector | 8 | 34 | 0.60% | 39.91 | 412.78 | 10% | 1.67 | 0.14 |
| 301 | Interceptor | 10 | 375 | 0.10% | 326.69 | 310.25 | 105% | 1.34 | 0.83 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 302 | Interceptor | 10 | 391 | 0.10% | 326.69 | 305.61 | 107% | 1.34 | 0.83 |
| 303 | Interceptor | 10 | 573 | 0.10% | 274.29 | 380.61 | 72% | 1.69 | 0.52 |
| 304 | Interceptor | 10 | 315 | 0.30% | 326.69 | 541.97 | 60% | 2.32 | 0.47 |
| 305 | Interceptor | 10 | 241 | 0.00% | 326.69 | 177.21 | 184% | 1.34 | 0.83 |
| 306 | Collector | 8 | 300 | 1.00% | 29.33 | 543.06 | 5% | 1.85 | 0.11 |
| 307 | Collector | 8 | 194 | 0.90% | 23.08 | 511.06 | 5% | 1.65 | 0.10 |
| 308 | Interceptor | 15 | 519 | 0.30% | 492.92 | 1669.73 | 30% | 2.64 | 0.47 |
| 309 | Collector | 8 | 592 | 0.30% | 0.00 | 312.40 | 0% | 0.00 | 0.00 |
| 310 | Collector | 8 | 320 | 0.30% | 4.33 | 293.67 | 2% | 0.68 | 0.06 |
| 311 | Collector | 8 | 295 | 0.40% | 3.08 | 361.46 | 1% | 0.71 | 0.04 |
| 312 | Collector | 8 | 336 | 0.30% | 3.08 | 297.63 | 1% | 0.62 | 0.05 |
| 313 | Collector | 8 | 327 | 0.40% | 3.08 | 361.36 | 1% | 0.71 | 0.04 |
| 314 | Collector | 8 | 250 | 0.50% | 0.00 | 387.30 | 0% | 0.00 | 0.00 |
| 315 | Collector | 8 | 302 | 0.40% | 3.08 | 330.05 | 1% | 0.66 | 0.05 |
| 316 | Collector | 8 | 316 | 0.60% | 3.08 | 421.78 | 1% | 0.79 | 0.04 |
| 317 | Collector | 8 | 297 | 0.20% | 3.08 | 234.77 | 1% | 0.52 | 0.05 |
| 318 | Collector | 8 | 341 | 0.30% | 3.08 | 311.88 | 1% | 0.64 | 0.05 |
| 320 | Collector | 8 | 348 | 0.50% | 27.49 | 367.84 | 8% | 1.38 | 0.12 |
| 321 | Collector | 8 | 226 | 0.40% | 6.24 | 349.17 | 2% | 0.85 | 0.06 |
| 322 | Collector | 8 | 173 | 0.40% | 9.25 | 335.81 | 3% | 0.94 | 0.08 |
| 323 | Collector | 8 | 137 | 0.30% | 9.25 | 315.66 | 3% | 0.90 | 0.08 |
| 324 | Collector | 8 | 265 | 0.50% | 3.08 | 386.51 | 1% | 0.74 | 0.04 |
| 325 | Collector | 8 | 601 | 0.30% | 3.08 | 319.39 | 1% | 0.65 | 0.05 |
| 327 | Collector | 8 | 504 | 0.30% | 8.66 | 296.82 | 3% | 0.84 | 0.08 |
| 328 | Collector | 8 | 305 | 0.30% | 4.54 | 315.79 | 1% | 0.72 | 0.06 |
| 331 | Collector | 8 | 337 | 0.50% | 5.45 | 378.88 | 1% | 0.87 | 0.06 |
| 332 | Collector | 8 | 234 | 0.30% | 54.61 | 292.03 | 19% | 1.43 | 0.20 |
| 333 | Collector | 8 | 52 | 0.80% | 54.61 | 482.65 | 11% | 2.04 | 0.15 |
| 334 | Collector | 8 | 159 | 0.40% | 54.61 | 351.03 | 16% | 1.63 | 0.18 |
| 335 | Collector | 8 | 271 | 0.20% | 49.62 | 258.25 | 19% | 1.27 | 0.20 |
| 336 | Collector | 8 | 105 | 0.40% | 48.08 | 331.33 | 15% | 1.51 | 0.17 |
| 337 | Collector | 8 | 293 | 0.40% | 4.50 | 364.40 | 1% | 0.80 | 0.05 |
| 338 | Collector | 8 | 355 | 0.30% | 0.00 | 318.99 | 0% | 0.00 | 0.00 |
| 339 | Collector | 8 | 496 | 0.30% | 0.00 | 312.36 | 0% | 0.00 | 0.00 |
| 340 | Interceptor | 15 | 304 | 0.20% | 496.98 | 1341.54 | 37% | 2.25 | 0.53 |
| 341 | Interceptor | 15 | 312 | 0.10% | 498.23 | 1037.86 | 48% | 1.87 | 0.61 |
| 342 | Interceptor | 15 | 335 | 0.10% | 633.31 | 886.70 | 71% | 1.75 | 0.78 |
| 343 | Interceptor | 15 | 302 | 0.30% | 633.31 | 1542.36 | 41% | 2.66 | 0.56 |
| 344 | Collector | 8 | 594 | 0.20% | 45.11 | 212.46 | 21% | 1.08 | 0.21 |
| 345 | Collector | 8 | 595 | 0.20% | 63.86 | 255.15 | 25% | 1.35 | 0.23 |
| 346 | Collector | 8 | 594 | 0.30% | 23.62 | 320.17 | 7% | 1.20 | 0.12 |
| 347 | Collector | 8 | 548 | 0.30% | 6.25 | 312.41 | 2% | 0.79 | 0.07 |
| 348 | Collector | 10 | 319 | -0.10% | 231.31 | | 100% | 0.95 | 0.83 |
| 349 | Collector | 12 | 595 | 0.20% | 94.09 | 757.99 | 12% | 1.46 | 0.24 |
| 350 | Collector | 12 | 327 | 0.10% | 140.74 | 532.93 | 26% | 1.28 | 0.35 |
| 351 | Collector | 12 | 268 | 0.70% | 140.74 | 1373.93 | 10% | 2.51 | 0.22 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 352 | Collector | 8 | 269 | 0.90% | 0.00 | 512.07 | 0% | 0.00 | 0.00 |
| 353 | Collector | 8 | 196 | 0.30% | 0.00 | 300.69 | 0% | 0.00 | 0.00 |
| 354 | Collector | 8 | 281 | 1.10% | 0.00 | 572.91 | 0% | 0.00 | 0.00 |
| 355 | Collector | 8 | 62 | -0.80% | 0.00 | | 100% | 0.00 | 0.00 |
| 356 | Collector | 8 | 146 | 1.80% | 3.46 | 719.73 | 1% | 1.18 | 0.03 |
| 357 | Interceptor | 10 | 180 | 0.30% | 129.59 | 561.20 | 23% | 1.86 | 0.27 |
| 358 | Collector | 8 | 103 | 0.10% | 12.50 | 185.64 | 7% | 0.67 | 0.12 |
| 359 | Collector | 8 | 307 | 0.80% | 6.17 | 491.05 | 1% | 1.08 | 0.05 |
| 360 | Collector | 8 | 235 | 0.40% | 14.25 | 362.83 | 4% | 1.12 | 0.09 |
| 361 | Collector | 8 | 262 | 0.20% | 32.50 | 268.31 | 12% | 1.16 | 0.16 |
| 362 | Collector | 8 | 247 | 0.40% | 31.25 | 355.32 | 9% | 1.40 | 0.13 |
| 363 | Collector | 8 | 217 | 0.30% | 0.00 | 312.30 | 0% | 0.00 | 0.00 |
| 364 | Collector | 8 | 326 | 0.30% | 10.58 | 320.65 | 3% | 0.94 | 0.08 |
| 365 | Collector | 8 | 217 | 0.40% | 0.00 | 331.68 | 0% | 0.00 | 0.00 |
| 366 | Interceptor | 10 | 290 | 0.50% | 114.59 | 723.29 | 16% | 2.16 | 0.22 |
| 367 | Collector | 8 | 361 | 0.40% | 5.00 | 341.42 | 2% | 0.79 | 0.06 |
| 368 | Collector | 8 | 87 | 0.00% | 9.87 | | 100% | 0.06 | 0.67 |
| 369 | Collector | 8 | 315 | 1.50% | 13.08 | 655.28 | 2% | 1.66 | 0.07 |
| 370 | Collector | 8 | 248 | 0.30% | 39.91 | 291.42 | 14% | 1.30 | 0.17 |
| 371 | Collector | 8 | 151 | -0.40% | 39.91 | | 100% | 0.26 | 0.67 |
| 372 | Interceptor | 10 | 403 | 0.20% | 326.69 | 415.62 | 79% | 1.88 | 0.56 |
| 373 | Interceptor | 10 | 402 | 0.10% | 326.69 | 343.90 | 95% | 1.60 | 0.65 |
| 374 | Collector | 8 | 297 | 0.10% | 3.62 | 182.89 | 2% | 0.46 | 0.07 |
| 375 | Collector | 8 | 592 | 0.10% | 23.62 | 192.83 | 12% | 0.84 | 0.16 |
| 376 | Collector | 10 | 595 | 0.20% | 289.50 | 482.67 | 60% | 2.06 | 0.47 |
| 377 | Collector | 10 | 595 | 0.50% | 141.69 | 689.04 | 21% | 2.22 | 0.26 |
| 378 | Collector | 12 | 566 | 0.40% | 3.82 | 1036.11 | 0% | 0.70 | 0.04 |
| 379 | Collector | 12 | 338 | 0.10% | 154.42 | 448.86 | 34% | 1.16 | 0.41 |
| 380 | Collector | 8 | 350 | 0.70% | 13.66 | 453.80 | 3% | 1.30 | 0.08 |
| 381 | Interceptor | 10 | 629 | 0.50% | 103.07 | 684.21 | 15% | 2.01 | 0.22 |
| 382 | Collector | 12 | 617 | 0.30% | 4.06 | 879.00 | 1% | 0.63 | 0.05 |
| 383 | Collector | 8 | 205 | 0.30% | 0.00 | 287.42 | 0% | 0.00 | 0.00 |
| 384 | Collector | 8 | 480 | 0.30% | 3.08 | 312.35 | 1% | 0.64 | 0.05 |
| 385 | Collector | 8 | 589 | 0.60% | 11.75 | 412.27 | 3% | 1.16 | 0.08 |
| 386 | Collector | 8 | 367 | 0.20% | 49.90 | 216.81 | 23% | 1.12 | 0.22 |
| 387 | Collector | 8 | 110 | 0.40% | 9.25 | 342.50 | 3% | 0.95 | 0.08 |
| 388 | Collector | 8 | 123 | 0.60% | 9.25 | 430.71 | 2% | 1.11 | 0.07 |
| 389 | Collector | 8 | 126 | 0.20% | 3.08 | 231.95 | 1% | 0.52 | 0.05 |
| 390 | Collector | 8 | 176 | 0.40% | 39.98 | 340.56 | 12% | 1.46 | 0.15 |
| 391 | Collector | 8 | 215 | 0.50% | 5.00 | 382.66 | 1% | 0.85 | 0.05 |
| 392 | Collector | 8 | 225 | 0.40% | 13.74 | 342.81 | 4% | 1.07 | 0.09 |
| 393 | Collector | 8 | 87 | -0.10% | 54.61 | | 100% | 0.35 | 0.67 |
| 394 | Collector | 8 | 157 | 0.40% | 4.50 | 328.61 | 1% | 0.74 | 0.06 |
| 395 | Collector | 8 | 240 | 0.40% | 57.68 | 324.55 | 18% | 1.56 | 0.19 |
| 396 | Collector | 8 | 80 | 0.00% | 0.00 | | 0% | 0.00 | 0.00 |
| 397 | Collector | 8 | 110 | 5.80% | 0.00 | 1305.24 | 0% | 0.00 | 0.00 |

MODEL SCENARIO 1B
SEWER SYSTEM MODEL OUTPUT
2018 EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 398 | Interceptor | 8 | 94 | 0.40% | 667.55 | 1840.81 | 36% | 3.08 | 0.52 |
| 399 | Collector | 10 | 279 | 0.30% | 2.50 | 536.20 | 1% | 0.56 | 0.04 |
| 400 | Collector | 10 | 299 | 0.30% | 107.90 | 502.85 | 22% | 1.64 | 0.26 |
| 401 | Collector | 8 | 160 | 2.00% | 4.13 | 774.80 | 1% | 1.31 | 0.04 |
| 402 | Collector | 8 | 158 | 0.10% | 4.13 | 180.40 | 2% | 0.48 | 0.07 |
| 403 | Collector | 8 | 298 | 0.40% | 18.74 | 364.02 | 5% | 1.22 | 0.10 |
| 404 | Collector | 8 | 116 | 0.40% | 0.00 | 348.07 | 0% | 0.00 | 0.00 |
| 405 | Collector | 8 | 151 | 0.30% | 2.50 | 295.79 | 1% | 0.58 | 0.04 |
| 406 | Collector | 8 | 246 | 0.30% | 2.50 | 295.64 | 1% | 0.58 | 0.04 |
| 407 | Collector | 8 | 405 | 0.30% | 2.50 | 295.72 | 1% | 0.58 | 0.04 |
| 408 | Collector | 8 | 181 | 0.30% | 2.50 | 295.76 | 1% | 0.58 | 0.04 |
| 409 | Collector | 8 | 177 | 0.30% | 2.50 | 295.71 | 1% | 0.58 | 0.04 |
| 410 | Collector | 8 | 257 | 0.30% | 2.50 | 295.81 | 1% | 0.58 | 0.04 |
| 411 | Collector | 8 | 199 | 0.30% | 4.99 | 295.76 | 2% | 0.71 | 0.06 |
| 412 | Collector | 8 | 716 | 0.30% | 35.00 | 315.07 | 11% | 1.33 | 0.15 |
| 413 | Collector | 8 | 284 | 0.30% | 35.00 | 312.36 | 11% | 1.32 | 0.15 |
| 414 | Collector | 8 | 174 | 0.30% | 31.25 | 312.38 | 10% | 1.28 | 0.14 |
| 417 | Collector | 8 | 206 | 0.30% | 31.25 | 312.78 | 10% | 1.28 | 0.14 |
| 420 | Collector | 8 | 80 | 1.10% | 6.17 | 560.71 | 1% | 1.18 | 0.05 |
| 421 | Collector | 8 | 105 | 0.30% | 6.17 | 312.47 | 2% | 0.79 | 0.07 |
| 423 | Collector | 8 | 375 | 0.30% | 6.17 | 312.35 | 2% | 0.79 | 0.07 |
| 424 | Collector | 8 | 79 | 2.40% | 7.42 | 836.63 | 1% | 1.65 | 0.04 |
| 425 | Collector | 8 | 16 | 1.00% | 0.00 | 544.78 | 0% | 0.00 | 0.00 |
| 426 | Collector | 8 | 9 | 0.30% | 0.00 | 312.42 | 0% | 0.00 | 0.00 |
| 428 | Collector | 8 | 185 | 0.30% | 0.00 | 312.40 | 0% | 0.00 | 0.00 |
| 430 | Collector | 8 | 201 | 0.30% | 5.00 | 312.47 | 2% | 0.74 | 0.06 |
| 431 | Collector | 8 | 297 | 0.30% | 5.00 | 297.78 | 2% | 0.71 | 0.06 |
| 433 | Collector | 8 | 54 | 0.30% | 147.66 | 312.28 | 47% | 1.97 | 0.32 |
| 443 | Collector | 8 | 1195 | 0.30% | 39.91 | 312.39 | 13% | 1.37 | 0.16 |
| 447 | Interceptor | 10 | 68 | 0.20% | 326.69 | 484.75 | 67% | 2.13 | 0.50 |
| 449 | Interceptor | 10 | 5 | 0.40% | 326.69 | 623.59 | 52% | 2.58 | 0.43 |
| 465 | Collector | 8 | 491 | 0.30% | 0.00 | 312.40 | 0% | 0.00 | 0.00 |
| 467 | Collector | 8 | 157 | 0.30% | 0.00 | 312.42 | 0% | 0.00 | 0.00 |
| 471 | Collector | 8 | 281 | 0.30% | 0.00 | 312.36 | 0% | 0.00 | 0.00 |
| 479 | Collector | 8 | 194 | 0.30% | 0.00 | 312.43 | 0% | 0.00 | 0.00 |
| 495 | Collector | 8 | 118 | 0.80% | 3.46 | 483.21 | 1% | 0.89 | 0.04 |
| 501 | Well Connection | 10 | 5 | 0.90% | 492.92 | 935.39 | 53% | 3.87 | 0.43 |
| 515 | Interceptor | 36 | 10 | 0.00% | 667.55 | 949.21 | 70% | 0.32 | 1.86 |
| 517 | Interceptor | 36 | 10 | 0.00% | 326.69 | 949.21 | 34% | 0.27 | 1.21 |
| 519 | Collector | 8 | 654 | 0.10% | 10.57 | 207.93 | 5% | 0.70 | 0.10 |
| 521 | Collector, Assumed pipe | 8 | 306 | 0.50% | 4.13 | 368.69 | 1% | 0.78 | 0.05 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 1 | Interceptor | 10 | 599 | 0.40% | 25.725 | 610.42 | 4% | 1.235 | 0.117 |
| 2 | Collector | 8 | 623 | 0.40% | 21.345 | 344.037 | 6% | 1.22 | 0.113 |
| 3 | Collector | 8 | 595 | 0.40% | 14.316 | 334.247 | 4% | 1.062 | 0.094 |
| 4 | Collector | 8 | 339 | 0.30% | 0 | 312.33 | 0% | 0 | 0 |
| 6 | Collector | 8 | 392 | 0.40% | 1.902 | 331.042 | 1% | 0.573 | 0.036 |
| 7 | Collector | 8 | 305 | 0.40% | 7.625 | 331.85 | 2% | 0.875 | 0.07 |
| 8 | Collector | 8 | 628 | 0.50% | 94.048 | 390.363 | 24% | 2.05 | 0.223 |
| 9 | Collector | 8 | 333 | 0.60% | 6.672 | 413.457 | 2% | 0.979 | 0.059 |
| 10 | Collector | 12 | 357 | 0.20% | 117.729 | 718.558 | 16% | 1.504 | 0.274 |
| 11 | Collector | 8 | 692 | 0.10% | 0.903 | 135.232 | 1% | 0.245 | 0.039 |
| 12 | Collector | 8 | 601 | 0.10% | 19.46 | 202.979 | 10% | 0.818 | 0.139 |
| 14 | Collector | 8 | 369 | 0.50% | 4.192 | 401.499 | 1% | 0.834 | 0.048 |
| 15 | Collector | 8 | 215 | 0.30% | 0 | 312.4 | 0% | 0 | 0 |
| 16 | Collector | 8 | 236 | 0.50% | 13.322 | 395.57 | 3% | 1.169 | 0.084 |
| 17 | Collector | 8 | 381 | 0.40% | 23.024 | 347.29 | 7% | 1.256 | 0.116 |
| 18 | Collector | 8 | 264 | 0.40% | 1.902 | 355.605 | 1% | 0.603 | 0.035 |
| 19 | Collector | 8 | 218 | 0.30% | 0 | 318.19 | 0% | 0 | 0 |
| 20 | Collector | 8 | 238 | 1.20% | 1.749 | 592.996 | 0% | 0.838 | 0.027 |
| 21 | Collector | 8 | 146 | 0.40% | 0 | 361.84 | 0% | 0 | 0 |
| 22 | Collector | 8 | 299 | 0.30% | 1.091 | 281.988 | 0% | 0.433 | 0.03 |
| 23 | Collector | 8 | 293 | 0.50% | 3.812 | 365.98 | 1% | 0.759 | 0.048 |
| 24 | Collector | 8 | 307 | 0.40% | 0 | 358.21 | 0% | 0 | 0 |
| 25 | Collector | 8 | 243 | 0.30% | 0 | 312.45 | 0% | 0 | 0 |
| 26 | Collector | 8 | 202 | 0.30% | 0 | 312.337 | 0% | 0 | 0 |
| 27 | Collector | 8 | 454 | 0.30% | 0 | 312.38 | 0% | 0 | 0 |
| 28 | Collector | 8 | 121 | 0.30% | 0 | 312.235 | 0% | 0 | 0 |
| 29 | Collector | 8 | 133 | 0.30% | 0 | 312.482 | 0% | 0 | 0 |
| 30 | Collector | 8 | 328 | 0.40% | 3.812 | 351.801 | 1% | 0.739 | 0.049 |
| 31 | Collector | 8 | 301 | 0.40% | 107.79 | 338.125 | 32% | 1.918 | 0.259 |
| 32 | Collector | 8 | 336 | 0.30% | 6.605 | 312.321 | 2% | 0.803 | 0.067 |
| 33 | Collector | 8 | 226 | 0.30% | 0 | 312.391 | 0% | 0 | 0 |
| 34 | Collector | 8 | 329 | 0.90% | 2.86 | 522.712 | 1% | 0.892 | 0.035 |
| 35 | Collector | 8 | 144 | 0.30% | 2.352 | 312.276 | 1% | 0.587 | 0.041 |
| 36 | Collector | 8 | 612 | 0.40% | 25.142 | 364.525 | 7% | 1.334 | 0.119 |
| 37 | Collector | 10 | 328 | 0.40% | 102.002 | 650.44 | 16% | 1.936 | 0.223 |
| 38 | Collector | 8 | 264 | 0.20% | 4.762 | 264.732 | 2% | 0.648 | 0.062 |
| 39 | Collector | 8 | 248 | 0.50% | 2.352 | 398.51 | 1% | 0.696 | 0.037 |
| 40 | Collector | 8 | 360 | 0.30% | 7.055 | 277.517 | 3% | 0.754 | 0.073 |
| 41 | Collector | 8 | 373 | 0.20% | 1.124 | 241.61 | 1% | 0.392 | 0.033 |
| 43 | Collector | 12 | 593 | 0.20% | 51.564 | 678.736 | 8% | 1.136 | 0.186 |
| 44 | Collector | 12 | 569 | 0.30% | 0 | 921.01 | 0% | 0 | 0 |
| 45 | Collector | 8 | 334 | 0.30% | 0 | 312.426 | 0% | 0 | 0 |
| 46 | Collector | 8 | 554 | 0.20% | 20.01 | 269.35 | 7% | 1.007 | 0.123 |
| 47 | Collector | 8 | 625 | 0.30% | 0 | 312.36 | 0% | 0 | 0 |
| 48 | Collector | 8 | 315 | 0.30% | 22.87 | 272.47 | 8% | 1.056 | 0.131 |
| 49 | Collector | 6 | 555 | 0.30% | 3.901 | 141.631 | 3% | 0.701 | 0.057 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 50 | Collector | 8 | 321 | 0.50% | 3.812 | 378.75 | 1% | 0.778 | 0.047 |
| 51 | Collector | 8 | 632 | 0.30% | 0 | 312.368 | 0% | 0 | 0 |
| 52 | Interceptor | 10 | 599 | 0.20% | 16.192 | 465.60 | 4% | 0.889 | 0.106 |
| 53 | Collector | 8 | 620 | 0.10% | 6.365 | 129.787 | 5% | 0.429 | 0.1 |
| 54 | Collector | 8 | 410 | 0.30% | 0 | 312.335 | 0% | 0 | 0 |
| 55 | Collector | 8 | 623 | 0.10% | 8.246 | 192.519 | 4% | 0.612 | 0.094 |
| 56 | Collector | 8 | 627 | 0.40% | 1.902 | 361.017 | 1% | 0.609 | 0.035 |
| 57 | Collector | 8 | 354 | 0.30% | 2.352 | 312.34 | 1% | 0.587 | 0.041 |
| 58 | Collector | 8 | 429 | 0.30% | 0 | 312.38 | 0% | 0 | 0 |
| 59 | Interceptor | 10 | 596 | 0.40% | 49.042 | 589.703 | 8% | 1.459 | 0.162 |
| 60 | Interceptor | 15 | 644 | 0.10% | 378.907 | 1060.321 | 36% | 1.764 | 0.516 |
| 61 | Collector | 8 | 349 | 0.40% | 0 | 361.014 | 0% | 0 | 0 |
| 62 | Collector | 8 | 271 | 0.40% | 8.58 | 345.836 | 3% | 0.933 | 0.072 |
| 64 | Collector | 8 | 157 | 0.40% | 2.86 | 351.35 | 1% | 0.676 | 0.043 |
| 65 | Collector | 8 | 401 | 0.40% | 32.385 | 344.74 | 9% | 1.382 | 0.138 |
| 66 | Collector | 8 | 169 | 0.60% | 34.287 | 408.962 | 8% | 1.585 | 0.13 |
| 67 | Interceptor | 10 | 41 | -0.10% | 175.318 | | 100% | 0.716 | 0.833 |
| 68 | Interceptor | 10 | 397 | 0.20% | 170.603 | 424.174 | 40% | 1.639 | 0.368 |
| 69 | Collector | 8 | 300 | 0.40% | 14.68 | 342.337 | 4% | 1.088 | 0.094 |
| 70 | Collector | 8 | 217 | 0.30% | 0 | 312.298 | 0% | 0 | 0 |
| 73 | Collector | 8 | 238 | 0.50% | 2.352 | 392.86 | 1% | 0.689 | 0.037 |
| 74 | Collector | 8 | 347 | 0.40% | 19.05 | 355.763 | 5% | 1.208 | 0.105 |
| 75 | Collector | 8 | 236 | 0.40% | 5.72 | 363.69 | 2% | 0.855 | 0.058 |
| 76 | Collector | 8 | 180 | 0.50% | 4.762 | 373.943 | 1% | 0.825 | 0.053 |
| 77 | Collector | 8 | 383 | 0.40% | 7.622 | 348.23 | 2% | 0.904 | 0.068 |
| 78 | Collector | 8 | 257 | 0.30% | 1.902 | 285.581 | 1% | 0.517 | 0.039 |
| 79 | Interceptor | 12 | 629 | 0.20% | 51.564 | 715.39 | 7% | 1.179 | 0.182 |
| 80 | Collector | 8 | 903 | 0.30% | 4.705 | 300.212 | 2% | 0.705 | 0.058 |
| 81 | Collector | 8 | 649 | 0.30% | 25.705 | 303.62 | 9% | 1.18 | 0.131 |
| 83 | Collector | 8 | 239 | 0.20% | 30.735 | 241.986 | 13% | 1.059 | 0.16 |
| 84 | Collector | 8 | 1391 | 0.30% | 30.735 | 289.02 | 11% | 1.201 | 0.147 |
| 85 | Collector | 8 | 400 | 0.30% | 30.735 | 314.036 | 10% | 1.274 | 0.141 |
| 86 | Collector | 8 | 327 | 0.40% | 3.805 | 343.03 | 1% | 0.725 | 0.049 |
| 87 | Collector | 8 | 223 | 0.40% | 28.58 | 343.997 | 8% | 1.33 | 0.13 |
| 88 | Collector | 8 | 173 | 0.70% | 1.902 | 459.78 | 0% | 0.72 | 0.031 |
| 89 | Interceptor | 10 | 400 | 0.00% | 249.868 | 180.373 | 139% | 1.021 | 0.833 |
| 90 | Interceptor | 10 | 741 | 0.20% | 211.515 | 436.00 | 49% | 1.768 | 0.409 |
| 91 | Collector | 8 | 373 | 0.70% | 0.938 | 445.816 | 0% | 0.568 | 0.023 |
| 92 | Collector | 8 | 240 | 0.40% | 11.787 | 360.92 | 3% | 1.057 | 0.083 |
| 93 | Collector | 8 | 340 | 0.30% | 0 | 312.65 | 0% | 0 | 0 |
| 94 | Collector | 8 | 217 | 0.50% | 3.797 | 367.781 | 1% | 0.761 | 0.048 |
| 95 | Interceptor | 10 | 398 | 0.20% | 90.795 | 430.716 | 21% | 1.394 | 0.26 |
| 96 | Collector | 8 | 262 | 0.20% | 59.683 | 243.084 | 25% | 1.283 | 0.225 |
| 97 | Collector | 8 | 361 | 0.40% | 8.577 | 338.932 | 3% | 0.92 | 0.073 |
| 98 | Collector | 8 | 417 | 0.30% | 14.265 | 298.777 | 5% | 0.98 | 0.099 |
| 99 | Collector | 8 | 390 | 0.20% | 4.75 | 226.433 | 2% | 0.581 | 0.067 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 100 | Collector | 8 | 449 | 0.40% | 3.812 | 338.22 | 1% | 0.719 | 0.05 |
| 101 | Collector | 8 | 399 | 1.90% | 0.698 | 746.248 | 0% | 0.742 | 0.016 |
| 102 | Collector | 8 | 353 | 0.50% | 0.698 | 379.902 | 0% | 0.464 | 0.021 |
| 103 | Collector | 8 | 235 | 2.80% | 0.233 | 908.81 | 0% | 0.607 | 0.009 |
| 104 | Collector | 8 | 588 | 2.00% | 14.697 | 770.885 | 2% | 1.921 | 0.064 |
| 105 | Collector | 8 | 301 | 0.00% | 2.84 | | 100% | 0.018 | 0.667 |
| 106 | Collector | 8 | 432 | 0.20% | 0.938 | 261.727 | 0% | 0.392 | 0.029 |
| 107 | Collector | 8 | 872 | 0.40% | 1.902 | 362.986 | 1% | 0.611 | 0.035 |
| 108 | Collector | 8 | 407 | 0.30% | 2.857 | 299.62 | 1% | 0.605 | 0.046 |
| 109 | Collector | 8 | 236 | 0.70% | 0 | 443.204 | 0% | 0 | 0 |
| 110 | Collector | 8 | 491 | 0.30% | 0 | 312.398 | 0% | 0 | 0 |
| 111 | Collector | 8 | 299 | 0.00% | 1.012 | 58.028 | 2% | 0.141 | 0.061 |
| 112 | Collector | 8 | 581 | 0.30% | 0 | 312.364 | 0% | 0 | 0 |
| 113 | Collector | 8 | 295 | 0.60% | 19.351 | 420.122 | 5% | 1.364 | 0.097 |
| 114 | Collector | 8 | 157 | 0.30% | 0 | 312.418 | 0% | 0 | 0 |
| 115 | Collector | 8 | 508 | 0.30% | 31.736 | 312.377 | 10% | 1.281 | 0.144 |
| 116 | Collector | 8 | 390 | 0.40% | 83.441 | 362.25 | 23% | 1.879 | 0.218 |
| 117 | Collector | 8 | 269 | 0.40% | 0 | 343.674 | 0% | 0 | 0 |
| 118 | Collector | 8 | 89 | 0.60% | 0 | 418.459 | 0% | 0 | 0 |
| 119 | Collector | 8 | 157 | 0.50% | 0 | 380.707 | 0% | 0 | 0 |
| 121 | Collector | 8 | 240 | 0.40% | 1.178 | 321.807 | 0% | 0.486 | 0.029 |
| 122 | Collector | 8 | 724 | 0.30% | 0 | 312.37 | 0% | 0 | 0 |
| 123 | Collector | 8 | 477 | 0.20% | 0.938 | 211.678 | 0% | 0.339 | 0.032 |
| 124 | Collector | 8 | 287 | 0.50% | 110.649 | 369.465 | 30% | 2.061 | 0.25 |
| 125 | Collector | 10 | 624 | 0.10% | 74.856 | 356.317 | 21% | 1.152 | 0.259 |
| 126 | Collector | 8 | 303 | 0.40% | 4.702 | 360.497 | 1% | 0.801 | 0.053 |
| 127 | Collector | 8 | 177 | 0.50% | 4.762 | 376.977 | 1% | 0.829 | 0.053 |
| 128 | Collector | 8 | 289 | 0.30% | 1.902 | 317.203 | 1% | 0.557 | 0.037 |
| 129 | Collector | 8 | 270 | 0.30% | 0 | 312.474 | 0% | 0 | 0 |
| 130 | Collector | 8 | 915 | 0.20% | 1.229 | 264.221 | 1% | 0.429 | 0.033 |
| 131 | Collector | 8 | 61 | 0.30% | 0 | 312.024 | 0% | 0 | 0 |
| 132 | Collector | 8 | 194 | 0.30% | 0 | 312.431 | 0% | 0 | 0 |
| 133 | Collector | 12 | 566 | 0.20% | 112.967 | 658.479 | 17% | 1.396 | 0.28 |
| 134 | Collector | 12 | 339 | 0.30% | 0 | 921.061 | 0% | 0 | 0 |
| 135 | Collector | 12 | 467 | 0.30% | 0 | 921.011 | 0% | 0 | 0 |
| 137 | Collector | 8 | 283 | 1.30% | 0 | 620.492 | 0% | 0 | 0 |
| 138 | Interceptor | 10 | 322 | 0.30% | 0 | 580.465 | 0% | 0 | 0 |
| 139 | Collector | 8 | 300 | 0.20% | 4.762 | 245.547 | 2% | 0.615 | 0.064 |
| 140 | Collector | 8 | 185 | 1.30% | 0 | 612.676 | 0% | 0 | 0 |
| 141 | Collector | 8 | 280 | 0.40% | 0.938 | 332.042 | 0% | 0.463 | 0.026 |
| 142 | Collector | 8 | 297 | 0.60% | 4.75 | 428.555 | 1% | 0.906 | 0.049 |
| 143 | Collector | 8 | 277 | 0.70% | 10.9 | 443.919 | 3% | 1.194 | 0.072 |
| 144 | Collector | 8 | 335 | 4.50% | 13.76 | 1156.831 | 1% | 2.499 | 0.051 |
| 145 | Collector | 8 | 343 | 0.30% | 14.697 | 285.816 | 5% | 0.959 | 0.103 |
| 146 | Collector | 8 | 60 | 2.50% | 17.557 | 864.173 | 2% | 2.195 | 0.066 |
| 147 | Collector | 8 | 46 | 5.30% | 17.557 | 1255.595 | 1% | 2.848 | 0.055 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 148 | Collector | 8 | 112 | 2.20% | 0.233 | 808.44 | 0% | 0.56 | 0.009 |
| 149 | Collector | 8 | 123 | 1.90% | 0.233 | 751.34 | 0% | 0.532 | 0.009 |
| 150 | Collector | 8 | 293 | 0.00% | 0.233 | 52.229 | 0% | 0.084 | 0.032 |
| 151 | Collector | 8 | 225 | 0.40% | 0.465 | 341.323 | 0% | 0.381 | 0.019 |
| 152 | Collector | 8 | 235 | 0.50% | 0.698 | 365.303 | 0% | 0.452 | 0.022 |
| 153 | Collector | 8 | 319 | 0.40% | 11.324 | 324.499 | 4% | 0.97 | 0.085 |
| 154 | Collector | 8 | 186 | 0.20% | 14.184 | 267.55 | 5% | 0.906 | 0.104 |
| 155 | Collector | 8 | 336 | 0.20% | 2.857 | 270.594 | 1% | 0.564 | 0.048 |
| 156 | Collector | 8 | 262 | 0.30% | 4.654 | 296.358 | 2% | 0.696 | 0.058 |
| 157 | Collector | 8 | 237 | 1.30% | 2.84 | 617.266 | 1% | 0.999 | 0.033 |
| 158 | Collector | 8 | 514 | 0.30% | 0.938 | 310.272 | 0% | 0.442 | 0.027 |
| 159 | Collector | 8 | 419 | 0.20% | 0 | 251.52 | 0% | 0 | 0 |
| 160 | Collector | 8 | 402 | 0.50% | 0.938 | 398.155 | 0% | 0.525 | 0.024 |
| 161 | Collector | 8 | 365 | 0.60% | 0.938 | 417.715 | 0% | 0.543 | 0.023 |
| 162 | Collector | 8 | 297 | 0.00% | 0.938 | | 100% | 0.006 | 0.667 |
| 163 | Collector | 8 | 302 | 0.30% | 0.938 | 314.579 | 0% | 0.446 | 0.027 |
| 164 | Collector | 8 | 301 | 0.20% | 0.938 | 270.026 | 0% | 0.401 | 0.029 |
| 165 | Collector | 8 | 301 | 0.20% | 25.18 | 254.265 | 10% | 1.035 | 0.142 |
| 166 | Collector | 8 | 352 | 0.20% | 29.922 | 225.773 | 13% | 1 | 0.164 |
| 167 | Collector | 8 | 398 | 0.20% | 32.782 | 212.095 | 16% | 0.982 | 0.177 |
| 170 | Collector | 8 | 358 | 0.30% | 10.257 | 277.099 | 4% | 0.843 | 0.088 |
| 172 | Collector | 8 | 173 | 0.40% | 1.902 | 360.338 | 1% | 0.608 | 0.035 |
| 173 | Collector | 8 | 114 | 0.50% | 0.938 | 392.856 | 0% | 0.52 | 0.024 |
| 174 | Collector | 8 | 247 | 0.50% | 2.84 | 384.931 | 1% | 0.719 | 0.041 |
| 175 | Collector | 8 | 210 | 0.40% | 6.652 | 359.876 | 2% | 0.888 | 0.063 |
| 176 | Collector | 8 | 133 | 0.20% | 9.942 | 270.831 | 4% | 0.822 | 0.087 |
| 178 | Collector | 8 | 397 | 0.20% | 41.578 | 257.801 | 16% | 1.208 | 0.181 |
| 179 | Collector | 8 | 352 | 0.30% | 46.34 | 291.284 | 16% | 1.36 | 0.18 |
| 180 | Collector | 8 | 395 | 0.30% | 51.103 | 278.183 | 18% | 1.353 | 0.194 |
| 181 | Collector | 8 | 137 | 0.60% | 74.885 | 414.016 | 18% | 2.005 | 0.192 |
| 182 | Collector | 8 | 128 | 1.10% | 1.635 | 576.353 | 0% | 0.805 | 0.026 |
| 183 | Collector | 8 | 416 | 0.60% | 1.635 | 423.617 | 0% | 0.65 | 0.03 |
| 184 | Interceptor | 10 | 307 | 0.20% | 76.52 | 425.244 | 18% | 1.316 | 0.239 |
| 185 | Collector | 8 | 384 | 0.50% | 0.698 | 397.73 | 0% | 0.479 | 0.021 |
| 186 | Collector | 8 | 400 | 0.50% | 0.698 | 399.091 | 0% | 0.481 | 0.021 |
| 187 | Collector | 8 | 298 | 0.50% | 3.812 | 372.303 | 1% | 0.769 | 0.048 |
| 188 | Interceptor | 10 | 595 | 0.10% | 19.052 | 323.105 | 6% | 0.722 | 0.137 |
| 189 | Collector | 10 | 601 | 0.60% | 11.523 | 775.365 | 2% | 1.147 | 0.071 |
| 191 | Collector | 8 | 298 | 0.30% | 15.247 | 319.011 | 5% | 1.047 | 0.099 |
| 192 | Collector | 8 | 295 | 0.30% | 11.435 | 294.242 | 4% | 0.908 | 0.09 |
| 193 | Collector | 8 | 295 | 0.20% | 11.435 | 262.021 | 4% | 0.837 | 0.095 |
| 194 | Collector | 8 | 627 | 0.20% | 32.445 | 240.211 | 14% | 1.07 | 0.165 |
| 195 | Collector | 8 | 592 | 0.40% | 25.773 | 348.304 | 7% | 1.301 | 0.123 |
| 196 | Collector | 8 | 270 | 0.30% | 16.587 | 281.961 | 6% | 0.984 | 0.11 |
| 197 | Collector | 8 | 298 | 0.80% | 0 | 471.48 | 0% | 0 | 0 |
| 198 | Collector | 8 | 310 | 0.80% | 10.485 | 487.041 | 2% | 1.259 | 0.068 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 199 | Collector | 8 | 307 | 0.40% | 1.012 | 345.43 | 0% | 0.487 | 0.026 |
| 200 | Collector | 8 | 306 | 0.30% | 24.113 | 316.37 | 8% | 1.192 | 0.125 |
| 201 | Collector | 8 | 169 | 0.30% | 0 | 312.46 | 0% | 0 | 0 |
| 202 | Collector | 8 | 58 | 0.30% | 0 | 312.13 | 0% | 0 | 0 |
| 203 | Collector | 8 | 293 | 0.00% | 0.154 | 52.22 | 0% | 0.074 | 0.027 |
| 204 | Collector | 8 | 211 | 0.50% | 13.754 | 368.20 | 4% | 1.123 | 0.088 |
| 205 | Collector | 8 | 234 | 0.30% | 48.731 | 295.70 | 17% | 1.395 | 0.183 |
| 206 | Collector | 8 | 226 | 0.40% | 0 | 363.856 | 0% | 0 | 0 |
| 207 | Collector | 8 | 231 | 0.40% | 55.396 | 325.67 | 17% | 1.55 | 0.186 |
| 208 | Collector | 8 | 189 | 1.50% | 17.567 | 656.916 | 3% | 1.812 | 0.075 |
| 209 | Collector | 8 | 111 | 0.50% | 77.726 | 373.85 | 21% | 1.884 | 0.206 |
| 210 | Collector | 8 | 66 | -3.60% | 81.538 | | 100% | 0.52 | 0.667 |
| 211 | Collector | 8 | 134 | 0.40% | 1.902 | 362.61 | 1% | 0.611 | 0.035 |
| 212 | Collector | 8 | 46 | 0.10% | 83.441 | 194.99 | 43% | 1.196 | 0.305 |
| 213 | Collector | 8 | 320 | 0.40% | 84.532 | 346.94 | 24% | 1.828 | 0.224 |
| 214 | Collector | 8 | 310 | 0.40% | 89.237 | 332.98 | 27% | 1.801 | 0.236 |
| 215 | Collector | 8 | 291 | 0.40% | 94 | 364.24 | 26% | 1.95 | 0.231 |
| 216 | Collector | 8 | 293 | 0.30% | 2.352 | 312.35 | 1% | 0.587 | 0.041 |
| 217 | Collector | 8 | 352 | 0.50% | 0 | 380.83 | 0% | 0 | 0 |
| 218 | Collector | 8 | 37 | -0.20% | 0 | | 100% | 0 | 0 |
| 219 | Interceptor | 10 | 400 | 0.30% | 78.423 | 522.29 | 15% | 1.535 | 0.218 |
| 220 | Interceptor | 10 | 400 | 0.10% | 79.36 | 357.523 | 22% | 1.174 | 0.267 |
| 221 | Interceptor | 10 | 399 | 0.20% | 79.36 | 439.33 | 18% | 1.361 | 0.24 |
| 222 | Interceptor | 10 | 401 | 0.10% | 81.263 | 285.27 | 29% | 1.004 | 0.304 |
| 223 | Collector | 8 | 321 | 0.30% | 0 | 283.86 | 0% | 0 | 0 |
| 224 | Interceptor | 10 | 625 | 0.10% | 21.912 | 323.93 | 7% | 0.754 | 0.147 |
| 225 | Interceptor | 10 | 597 | 0.30% | 33.347 | 580.45 | 6% | 1.288 | 0.136 |
| 226 | Collector | 8 | 525 | 0.30% | 0 | 312.359 | 0% | 0 | 0 |
| 227 | Collector | 8 | 597 | 0.20% | 20.349 | 240.27 | 9% | 0.934 | 0.131 |
| 228 | Collector | 8 | 630 | 0.40% | 17.797 | 362.92 | 5% | 1.2 | 0.1 |
| 229 | Collector | 8 | 595 | 0.40% | 13.002 | 342.18 | 4% | 1.049 | 0.089 |
| 230 | Collector | 8 | 312 | 0.20% | 34.29 | 240.64 | 14% | 1.088 | 0.17 |
| 231 | Collector | 8 | 319 | 0.30% | 29.527 | 289.66 | 10% | 1.189 | 0.144 |
| 232 | Collector | 8 | 51 | 2.10% | 28.59 | 788.276 | 4% | 2.382 | 0.087 |
| 234 | Collector | 8 | 628 | 0.20% | 9.889 | 260.26 | 4% | 0.798 | 0.089 |
| 235 | Collector | 8 | 628 | 0.20% | 49.325 | 235.203 | 21% | 1.188 | 0.207 |
| 236 | Collector | 8 | 460 | 0.30% | 0 | 312.39 | 0% | 0 | 0 |
| 237 | Collector | 10 | 602 | 0.20% | 66.797 | 459.591 | 15% | 1.338 | 0.215 |
| 238 | Collector | 10 | 250 | 0.30% | 77.49 | 533.17 | 15% | 1.552 | 0.215 |
| 239 | Collector | 10 | 298 | 0.10% | 79.4 | 361.575 | 22% | 1.184 | 0.265 |
| 240 | Collector | 10 | 302 | 0.60% | 81.303 | 768.51 | 11% | 2.041 | 0.183 |
| 241 | Collector | 8 | 278 | 0.20% | 1.902 | 219.507 | 1% | 0.431 | 0.044 |
| 242 | Collector | 8 | 124 | 0.40% | 4.762 | 336.82 | 1% | 0.767 | 0.055 |
| 243 | Collector | 8 | 297 | 0.40% | 107.79 | 349.273 | 31% | 1.964 | 0.254 |
| 245 | Collector | 8 | 577 | -0.80% | 4.702 | | 100% | 0.03 | 0.667 |
| 246 | Collector | 8 | 327 | 0.30% | 4.702 | 319.904 | 2% | 0.737 | 0.056 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 247 | Collector | 8 | 287 | 0.50% | 107.79 | 376.67 | 29% | 2.075 | 0.244 |
| 250 | Collector | 8 | 70 | 0.90% | 2.35 | 503.671 | 1% | 0.819 | 0.033 |
| 251 | Collector | 8 | 111 | 0.40% | 8.927 | 348.817 | 3% | 0.95 | 0.073 |
| 252 | Interceptor | 10 | 399 | 0.20% | 93.655 | 406.068 | 23% | 1.348 | 0.272 |
| 253 | Interceptor | 10 | 163 | 0.10% | 95.558 | 348.525 | 27% | 1.214 | 0.298 |
| 256 | Collector | 10 | 595 | 0.40% | 20.625 | 660.489 | 3% | 1.222 | 0.101 |
| 257 | Collector | 10 | 59 | 0.90% | 0 | 912.97 | 0% | 0 | 0 |
| 258 | Interceptor | 12 | 625 | 0.20% | 276.6 | 676.657 | 41% | 1.823 | 0.445 |
| 259 | Collector | 8 | 207 | 0.20% | 0 | 267.51 | 0% | 0 | 0 |
| 260 | Collector | 8 | 183 | 0.40% | 2.352 | 348.467 | 1% | 0.634 | 0.039 |
| 261 | Collector | 10 | 278 | 0.50% | 180.573 | 695.52 | 26% | 2.387 | 0.29 |
| 262 | Collector | 8 | 629 | 0.10% | 34.93 | 204.387 | 17% | 0.974 | 0.186 |
| 263 | Collector | 8 | 280 | 0.40% | 2.795 | 334.80 | 1% | 0.65 | 0.043 |
| 266 | Collector | 10 | 299 | 0.40% | 87.003 | 594.096 | 15% | 1.734 | 0.215 |
| 267 | Collector | 10 | 302 | 0.30% | 87.94 | 509.59 | 17% | 1.558 | 0.234 |
| 268 | Collector | 10 | 297 | 0.30% | 100.099 | 544.963 | 18% | 1.697 | 0.242 |
| 269 | Interceptor | 8 | 85 | 0.40% | 508.877 | 344.26 | 148% | 3.248 | 0.667 |
| 270 | Collector | 8 | 270 | 0.30% | 2.857 | 294.976 | 1% | 0.599 | 0.046 |
| 272 | Collector | 8 | 162 | 0.50% | 2.86 | 398.72 | 1% | 0.739 | 0.04 |
| 273 | Collector | 8 | 101 | 0.50% | 9.517 | 381.05 | 3% | 1.03 | 0.073 |
| 274 | Collector | 8 | 218 | 0.50% | 40.01 | 369.13 | 11% | 1.542 | 0.148 |
| 275 | Collector | 8 | 272 | 0.40% | 12.385 | 358.203 | 4% | 1.067 | 0.085 |
| 276 | Collector | 8 | 390 | 0.50% | 11.787 | 379.58 | 3% | 1.095 | 0.081 |
| 277 | Collector | 8 | 171 | 0.80% | 13.69 | 495.965 | 3% | 1.381 | 0.076 |
| 278 | Interceptor | 10 | 238 | 0.20% | 95.558 | 453.71 | 21% | 1.468 | 0.26 |
| 279 | Interceptor | 10 | 399 | 0.10% | 114.963 | 275.876 | 42% | 1.076 | 0.375 |
| 280 | Interceptor | 10 | 363 | 0.20% | 171.54 | 433.58 | 40% | 1.668 | 0.364 |
| 281 | Collector | 8 | 201 | 0.50% | 15.63 | 379.206 | 4% | 1.191 | 0.092 |
| 282 | Interceptor | 10 | 37 | 0.00% | 114.963 | 170.30 | 68% | 0.747 | 0.502 |
| 283 | Collector | 8 | 286 | 0.50% | 2.84 | 383.118 | 1% | 0.717 | 0.041 |
| 284 | Collector | 8 | 196 | -0.40% | 0.938 | | 100% | 0.006 | 0.667 |
| 285 | Collector | 8 | 181 | 0.40% | 0.938 | 357.953 | 0% | 0.488 | 0.025 |
| 286 | Collector | 8 | 141 | 0.40% | 11.82 | 350.15 | 3% | 1.036 | 0.084 |
| 288 | Collector | 8 | 517 | 0.30% | 25.705 | 303.728 | 9% | 1.18 | 0.131 |
| 289 | Collector | 8 | 216 | 0.30% | 25.705 | 316.27 | 8% | 1.215 | 0.129 |
| 290 | Collector | 8 | 301 | 0.40% | 4.705 | 333.829 | 1% | 0.759 | 0.055 |
| 291 | Collector | 8 | 106 | 0.30% | 30.41 | 314.01 | 10% | 1.27 | 0.14 |
| 292 | Collector | 8 | 399 | -0.10% | 0 | | 100% | 0 | 0 |
| 293 | Collector | 8 | 159 | 0.70% | 30.735 | 454.08 | 7% | 1.652 | 0.117 |
| 295 | Collector | 8 | 401 | 0.20% | 30.735 | 214.644 | 14% | 0.972 | 0.17 |
| 296 | Collector | 8 | 398 | 0.20% | 30.735 | 231.829 | 13% | 1.027 | 0.164 |
| 297 | Collector | 8 | 326 | 0.40% | 1.902 | 337.525 | 1% | 0.581 | 0.036 |
| 298 | Collector | 8 | 275 | 0.40% | 7.617 | 345.27 | 2% | 0.899 | 0.068 |
| 299 | Collector | 8 | 380 | 0.10% | 38.352 | 124.10 | 31% | 0.698 | 0.254 |
| 300 | Collector | 8 | 34 | 0.60% | 30.735 | 412.775 | 7% | 1.545 | 0.123 |
| 301 | Interceptor | 10 | 375 | 0.10% | 249.868 | 310.247 | 81% | 1.41 | 0.567 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 302 | Interceptor | 10 | 391 | 0.10% | 249.868 | 305.61 | 82% | 1.392 | 0.573 |
| 303 | Interceptor | 10 | 573 | 0.10% | 209.605 | 380.61 | 55% | 1.592 | 0.441 |
| 304 | Interceptor | 10 | 315 | 0.30% | 249.868 | 541.97 | 46% | 2.169 | 0.397 |
| 305 | Interceptor | 10 | 241 | 0.00% | 249.868 | 177.21 | 141% | 1.021 | 0.833 |
| 306 | Collector | 8 | 300 | 1.00% | 22.32 | 543.06 | 4% | 1.704 | 0.092 |
| 307 | Collector | 8 | 194 | 0.90% | 17.557 | 511.06 | 3% | 1.52 | 0.085 |
| 308 | Interceptor | 15 | 519 | 0.30% | 375.817 | 1,669.73 | 23% | 2.447 | 0.403 |
| 309 | Collector | 8 | 592 | 0.30% | 0 | 312.40 | 0% | 0 | 0 |
| 310 | Collector | 8 | 320 | 0.30% | 3.29 | 293.67 | 1% | 0.623 | 0.05 |
| 311 | Collector | 8 | 295 | 0.40% | 2.352 | 361.46 | 1% | 0.65 | 0.038 |
| 312 | Collector | 8 | 336 | 0.30% | 2.352 | 297.633 | 1% | 0.568 | 0.042 |
| 313 | Collector | 8 | 327 | 0.40% | 2.352 | 361.356 | 1% | 0.65 | 0.038 |
| 314 | Collector | 8 | 250 | 0.50% | 0 | 387.30 | 0% | 0 | 0 |
| 315 | Collector | 8 | 302 | 0.40% | 2.352 | 330.05 | 1% | 0.61 | 0.04 |
| 316 | Collector | 8 | 316 | 0.60% | 2.352 | 421.78 | 1% | 0.724 | 0.036 |
| 317 | Collector | 8 | 297 | 0.20% | 2.352 | 234.77 | 1% | 0.481 | 0.047 |
| 318 | Collector | 8 | 341 | 0.30% | 2.352 | 311.88 | 1% | 0.587 | 0.041 |
| 320 | Collector | 8 | 348 | 0.50% | 20.962 | 367.84 | 6% | 1.272 | 0.108 |
| 321 | Collector | 8 | 226 | 0.40% | 4.76 | 349.173 | 1% | 0.786 | 0.054 |
| 322 | Collector | 8 | 173 | 0.40% | 7.057 | 335.813 | 2% | 0.862 | 0.067 |
| 323 | Collector | 8 | 137 | 0.30% | 7.057 | 315.656 | 2% | 0.825 | 0.069 |
| 324 | Collector | 8 | 265 | 0.50% | 2.352 | 386.51 | 1% | 0.681 | 0.037 |
| 325 | Collector | 8 | 601 | 0.30% | 2.352 | 319.387 | 1% | 0.597 | 0.041 |
| 327 | Collector | 8 | 504 | 0.30% | 6.577 | 296.818 | 2% | 0.774 | 0.069 |
| 328 | Collector | 8 | 305 | 0.30% | 3.465 | 315.794 | 1% | 0.666 | 0.049 |
| 331 | Collector | 8 | 337 | 0.50% | 4.157 | 378.877 | 1% | 0.799 | 0.049 |
| 332 | Collector | 8 | 234 | 0.30% | 41.578 | 292.031 | 14% | 1.321 | 0.17 |
| 333 | Collector | 8 | 52 | 0.80% | 41.578 | 482.646 | 9% | 1.886 | 0.132 |
| 334 | Collector | 8 | 159 | 0.40% | 41.578 | 351.029 | 12% | 1.505 | 0.155 |
| 335 | Collector | 8 | 271 | 0.20% | 37.773 | 258.253 | 15% | 1.177 | 0.172 |
| 336 | Collector | 8 | 105 | 0.40% | 36.595 | 331.329 | 11% | 1.392 | 0.15 |
| 337 | Collector | 8 | 293 | 0.40% | 3.431 | 364.399 | 1% | 0.733 | 0.046 |
| 338 | Collector | 8 | 355 | 0.30% | 0.233 | 318.991 | 0% | 0.294 | 0.014 |
| 339 | Collector | 8 | 496 | 0.30% | 0 | 312.363 | 0% | 0 | 0 |
| 340 | Interceptor | 15 | 304 | 0.20% | 378.907 | 1341.543 | 28% | 2.094 | 0.454 |
| 341 | Interceptor | 15 | 312 | 0.10% | 379.845 | 1037.86 | 37% | 1.738 | 0.523 |
| 342 | Interceptor | 15 | 335 | 0.10% | 482.784 | 886.702 | 54% | 1.644 | 0.658 |
| 343 | Interceptor | 15 | 302 | 0.30% | 482.784 | 1542.364 | 31% | 2.476 | 0.48 |
| 344 | Collector | 8 | 594 | 0.20% | 34.393 | 212.457 | 16% | 0.997 | 0.181 |
| 345 | Collector | 8 | 595 | 0.20% | 48.688 | 255.154 | 19% | 1.255 | 0.197 |
| 346 | Collector | 8 | 594 | 0.30% | 17.997 | 320.165 | 6% | 1.103 | 0.107 |
| 347 | Collector | 8 | 548 | 0.30% | 4.762 | 312.41 | 2% | 0.727 | 0.057 |
| 348 | Collector | 10 | 319 | -0.10% | 176.76 | | 100% | 0.722 | 0.833 |
| 349 | Collector | 12 | 595 | 0.20% | 71.314 | 757.989 | 9% | 1.351 | 0.207 |
| 350 | Collector | 12 | 327 | 0.10% | 107.301 | 532.931 | 20% | 1.183 | 0.304 |
| 351 | Collector | 12 | 268 | 0.70% | 107.301 | 1373.928 | 8% | 2.318 | 0.189 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|---------------------|
| 352 | Collector | 8 | 269 | 0.90% | 0 | 512.067 | 0% | 0 | 0 |
| 353 | Collector | 8 | 196 | 0.30% | 0 | 300.69 | 0% | 0 | 0 |
| 354 | Collector | 8 | 281 | 1.10% | 0 | 572.91 | 0% | 0 | 0 |
| 355 | Collector | 8 | 62 | -0.80% | 0 | | 100% | 0 | 0 |
| 356 | Collector | 8 | 146 | 1.80% | 2.635 | 719.73 | 0% | 1.086 | 0.029 |
| 357 | Interceptor | 10 | 180 | 0.30% | 99.37 | 561.2 | 18% | 1.729 | 0.237 |
| 358 | Collector | 8 | 103 | 0.10% | 9.517 | 185.636 | 5% | 0.622 | 0.103 |
| 359 | Collector | 8 | 307 | 0.80% | 4.705 | 491.052 | 1% | 0.993 | 0.046 |
| 360 | Collector | 8 | 235 | 0.40% | 10.87 | 362.832 | 3% | 1.036 | 0.079 |
| 361 | Collector | 8 | 262 | 0.20% | 24.767 | 268.308 | 9% | 1.07 | 0.137 |
| 362 | Collector | 8 | 247 | 0.40% | 23.83 | 355.319 | 7% | 1.289 | 0.117 |
| 363 | Collector | 8 | 217 | 0.30% | 0 | 312.301 | 0% | 0 | 0 |
| 364 | Collector | 8 | 326 | 0.30% | 8.072 | 320.65 | 3% | 0.869 | 0.073 |
| 365 | Collector | 8 | 217 | 0.40% | 0 | 331.679 | 0% | 0 | 0 |
| 366 | Interceptor | 10 | 290 | 0.50% | 87.935 | 723.288 | 12% | 2 | 0.196 |
| 367 | Collector | 8 | 361 | 0.40% | 3.812 | 341.421 | 1% | 0.724 | 0.05 |
| 368 | Collector | 8 | 87 | 0.00% | 7.512 | | 100% | 0.048 | 0.667 |
| 369 | Collector | 8 | 315 | 1.50% | 9.975 | 655.284 | 2% | 1.525 | 0.057 |
| 370 | Collector | 8 | 248 | 0.30% | 30.735 | 291.422 | 11% | 1.208 | 0.146 |
| 371 | Collector | 8 | 151 | -0.40% | 30.735 | | 100% | 0.196 | 0.667 |
| 372 | Interceptor | 10 | 403 | 0.20% | 249.868 | 415.62 | 60% | 1.775 | 0.466 |
| 373 | Interceptor | 10 | 402 | 0.10% | 249.868 | 343.895 | 73% | 1.532 | 0.527 |
| 374 | Collector | 8 | 297 | 0.10% | 2.752 | 182.894 | 2% | 0.424 | 0.057 |
| 375 | Collector | 8 | 592 | 0.10% | 17.997 | 192.832 | 9% | 0.771 | 0.138 |
| 376 | Collector | 10 | 595 | 0.20% | 221.223 | 482.674 | 46% | 1.929 | 0.396 |
| 377 | Collector | 10 | 595 | 0.50% | 108.014 | 689.043 | 16% | 2.05 | 0.223 |
| 378 | Collector | 12 | 566 | 0.40% | 2.91 | 1036.113 | 0% | 0.641 | 0.039 |
| 379 | Collector | 12 | 338 | 0.10% | 117.729 | 448.86 | 26% | 1.073 | 0.35 |
| 380 | Collector | 8 | 350 | 0.70% | 10.418 | 453.8 | 2% | 1.196 | 0.07 |
| 381 | Interceptor | 10 | 629 | 0.50% | 78.592 | 684.205 | 12% | 1.861 | 0.191 |
| 382 | Collector | 12 | 617 | 0.30% | 3.091 | 879.003 | 0% | 0.582 | 0.043 |
| 383 | Collector | 8 | 205 | 0.30% | 0 | 287.423 | 0% | 0 | 0 |
| 384 | Collector | 8 | 480 | 0.30% | 2.352 | 312.354 | 1% | 0.587 | 0.041 |
| 385 | Collector | 8 | 589 | 0.60% | 8.957 | 412.265 | 2% | 1.068 | 0.068 |
| 386 | Collector | 8 | 367 | 0.20% | 38.352 | 216.811 | 18% | 1.043 | 0.19 |
| 387 | Collector | 8 | 110 | 0.40% | 7.057 | 342.504 | 2% | 0.873 | 0.066 |
| 388 | Collector | 8 | 123 | 0.60% | 7.057 | 430.713 | 2% | 1.025 | 0.059 |
| 389 | Collector | 8 | 126 | 0.20% | 2.352 | 231.95 | 1% | 0.477 | 0.047 |
| 390 | Collector | 8 | 176 | 0.40% | 30.482 | 340.563 | 9% | 1.345 | 0.135 |
| 391 | Collector | 8 | 215 | 0.50% | 3.797 | 382.659 | 1% | 0.782 | 0.047 |
| 392 | Collector | 8 | 225 | 0.40% | 10.48 | 342.809 | 3% | 0.984 | 0.08 |
| 393 | Collector | 8 | 87 | -0.10% | 41.578 | | 100% | 0.265 | 0.667 |
| 394 | Collector | 8 | 157 | 0.40% | 3.431 | 328.605 | 1% | 0.682 | 0.048 |
| 395 | Collector | 8 | 240 | 0.40% | 43.969 | 324.547 | 14% | 1.447 | 0.166 |
| 396 | Collector | 8 | 80 | 0.00% | 0 | | 0% | 0 | 0 |
| 397 | Collector | 8 | 110 | 5.80% | 0 | 1305.235 | 0% | 0 | 0 |

MODEL SCENARIO 2A
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 2.5 (INTERCEPTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|---------------------|
| 398 | Interceptor | 8 | 94 | 0.40% | 508.877 | 344.346 | 148% | 3.248 | 0.667 |
| 399 | Collector | 10 | 279 | 0.30% | 1.902 | 536.13 | 0% | 0.513 | 0.036 |
| 400 | Collector | 10 | 299 | 0.30% | 82.24 | 502.848 | 16% | 1.515 | 0.228 |
| 401 | Collector | 8 | 160 | 2.00% | 3.146 | 774.803 | 0% | 1.207 | 0.031 |
| 402 | Collector | 8 | 158 | 0.10% | 3.146 | 180.403 | 2% | 0.437 | 0.061 |
| 403 | Collector | 8 | 298 | 0.40% | 14.29 | 364.02 | 4% | 1.127 | 0.09 |
| 404 | Collector | 8 | 116 | 0.40% | 0 | 348.065 | 0% | 0 | 0 |
| 405 | Collector | 8 | 151 | 0.30% | 1.902 | 295.856 | 1% | 0.53 | 0.038 |
| 406 | Collector | 8 | 246 | 0.30% | 1.902 | 295.64 | 1% | 0.53 | 0.038 |
| 407 | Collector | 8 | 405 | 0.30% | 1.902 | 295.722 | 1% | 0.53 | 0.038 |
| 408 | Collector | 8 | 181 | 0.30% | 1.902 | 295.76 | 1% | 0.53 | 0.038 |
| 409 | Collector | 8 | 177 | 0.30% | 1.902 | 295.71 | 1% | 0.53 | 0.038 |
| 410 | Collector | 8 | 257 | 0.30% | 1.902 | 295.809 | 1% | 0.53 | 0.038 |
| 411 | Collector | 8 | 199 | 0.30% | 3.805 | 295.76 | 1% | 0.654 | 0.053 |
| 412 | Collector | 8 | 716 | 0.30% | 26.69 | 315.07 | 9% | 1.225 | 0.131 |
| 413 | Collector | 8 | 284 | 0.30% | 26.69 | 312.361 | 9% | 1.217 | 0.132 |
| 414 | Collector | 8 | 174 | 0.30% | 23.83 | 312.38 | 8% | 1.178 | 0.125 |
| 417 | Collector | 8 | 206 | 0.30% | 23.83 | 312.78 | 8% | 1.179 | 0.124 |
| 420 | Collector | 8 | 80 | 1.10% | 4.702 | 560.71 | 1% | 1.089 | 0.043 |
| 421 | Collector | 8 | 105 | 0.30% | 4.702 | 312.47 | 2% | 0.725 | 0.057 |
| 423 | Collector | 8 | 375 | 0.30% | 4.702 | 312.35 | 2% | 0.725 | 0.057 |
| 424 | Collector | 8 | 79 | 2.40% | 5.64 | 836.631 | 1% | 1.521 | 0.039 |
| 425 | Collector | 8 | 16 | 1.00% | 0 | 544.782 | 0% | 0 | 0 |
| 426 | Collector | 8 | 9 | 0.30% | 0 | 312.421 | 0% | 0 | 0 |
| 428 | Collector | 8 | 185 | 0.30% | 0 | 312.395 | 0% | 0 | 0 |
| 430 | Collector | 8 | 201 | 0.30% | 3.812 | 312.472 | 1% | 0.68 | 0.052 |
| 431 | Collector | 8 | 297 | 0.30% | 3.812 | 297.775 | 1% | 0.658 | 0.053 |
| 433 | Collector | 8 | 54 | 0.30% | 112.552 | 312.284 | 36% | 1.831 | 0.277 |
| 443 | Collector | 8 | 1195 | 0.30% | 30.735 | 312.392 | 10% | 1.269 | 0.141 |
| 447 | Interceptor | 10 | 68 | 0.20% | 249.868 | 484.75 | 52% | 1.995 | 0.424 |
| 449 | Interceptor | 10 | 5 | 0.40% | 249.868 | 623.59 | 40% | 2.407 | 0.367 |
| 465 | Collector | 8 | 491 | 0.30% | 0 | 312.398 | 0% | 0 | 0 |
| 467 | Collector | 8 | 157 | 0.30% | 0 | 312.418 | 0% | 0 | 0 |
| 471 | Collector | 8 | 281 | 0.30% | 0 | 312.36 | 0% | 0 | 0 |
| 479 | Collector | 8 | 194 | 0.30% | 0 | 312.43 | 0% | 0 | 0 |
| 495 | Collector | 8 | 118 | 0.80% | 2.635 | 483.212 | 1% | 0.824 | 0.035 |
| 501 | Well Connection | 10 | 5 | 0.90% | 375.817 | 935.39 | 40% | 3.613 | 0.367 |
| 515 | Interceptor | 36 | 10 | 0.00% | 508.877 | 949.207 | 54% | 0.304 | 1.564 |
| 517 | Interceptor | 36 | 10 | 0.00% | 249.868 | 949.207 | 26% | 0.252 | 1.051 |
| 519 | Collector | 8 | 654 | 0.10% | 8.059 | 207.93 | 4% | 0.641 | 0.09 |
| 521 | Collector | 8 | 306 | 0.50% | 3.146 | 368.686 | 1% | 0.72 | 0.044 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|------------------------|
| 1 | Interceptor | 10 | 599.03 | 0.40% | 41.16 | 610.42 | 7% | 1.420 | 0.147 |
| 2 | Collector | 8 | 622.61 | 0.40% | 34.15 | 344.04 | 10% | 1.401 | 0.142 |
| 3 | Collector | 8 | 595.29 | 0.40% | 22.91 | 334.25 | 7% | 1.221 | 0.118 |
| 4 | Collector | 8 | 338.92 | 0.30% | 0.00 | 312.33 | 0% | 0.000 | 0.000 |
| 6 | Collector | 8 | 391.81 | 0.40% | 3.04 | 331.04 | 1% | 0.661 | 0.045 |
| 7 | Collector | 8 | 304.52 | 0.40% | 12.20 | 331.85 | 4% | 1.007 | 0.087 |
| 8 | Collector | 8 | 627.79 | 0.50% | 150.47 | 390.36 | 39% | 2.330 | 0.287 |
| 9 | Collector | 8 | 333.35 | 0.60% | 10.68 | 413.46 | 3% | 1.129 | 0.074 |
| 10 | Collector | 12 | 356.98 | 0.20% | 188.36 | 718.56 | 26% | 1.717 | 0.349 |
| 11 | Collector | 8 | 692.09 | 0.10% | 1.44 | 135.23 | 1% | 0.283 | 0.048 |
| 12 | Collector | 8 | 600.76 | 0.10% | 31.14 | 202.98 | 15% | 0.938 | 0.176 |
| 14 | Collector | 8 | 369.46 | 0.50% | 6.71 | 401.50 | 2% | 0.961 | 0.060 |
| 15 | Collector | 8 | 214.53 | 0.30% | 0.00 | 312.40 | 0% | 0.000 | 0.000 |
| 16 | Collector | 8 | 236.42 | 0.50% | 21.32 | 395.57 | 5% | 1.345 | 0.105 |
| 17 | Collector | 8 | 380.77 | 0.40% | 36.84 | 347.29 | 11% | 1.442 | 0.147 |
| 18 | Collector | 8 | 264.49 | 0.40% | 3.04 | 355.61 | 1% | 0.695 | 0.044 |
| 19 | Collector | 8 | 217.60 | 0.30% | 0.00 | 318.19 | 0% | 0.000 | 0.000 |
| 20 | Collector | 8 | 237.91 | 1.20% | 2.80 | 593.00 | 1% | 0.967 | 0.033 |
| 21 | Collector | 8 | 145.91 | 0.40% | 0.00 | 361.84 | 0% | 0.000 | 0.000 |
| 22 | Collector | 8 | 298.63 | 0.30% | 1.75 | 281.99 | 1% | 0.500 | 0.038 |
| 23 | Collector | 8 | 293.43 | 0.50% | 6.10 | 365.98 | 2% | 0.876 | 0.060 |
| 24 | Collector | 8 | 306.75 | 0.40% | 0.00 | 358.21 | 0% | 0.000 | 0.000 |
| 25 | Collector | 8 | 242.64 | 0.30% | 0.00 | 312.45 | 0% | 0.000 | 0.000 |
| 26 | Collector | 8 | 201.89 | 0.30% | 0.00 | 312.34 | 0% | 0.000 | 0.000 |
| 27 | Collector | 8 | 453.98 | 0.30% | 0.00 | 312.38 | 0% | 0.000 | 0.000 |
| 28 | Collector | 8 | 121.33 | 0.30% | 0.00 | 312.24 | 0% | 0.000 | 0.000 |
| 29 | Collector | 8 | 132.65 | 0.30% | 0.00 | 312.48 | 0% | 0.000 | 0.000 |
| 30 | Collector | 8 | 328.30 | 0.40% | 6.10 | 351.80 | 2% | 0.852 | 0.061 |
| 31 | Collector | 8 | 301.08 | 0.40% | 172.46 | 338.13 | 51% | 2.169 | 0.337 |
| 32 | Collector | 8 | 335.60 | 0.30% | 10.57 | 312.32 | 3% | 0.925 | 0.084 |
| 33 | Collector | 8 | 225.76 | 0.30% | 0.00 | 312.39 | 0% | 0.000 | 0.000 |
| 34 | Collector | 8 | 328.59 | 0.90% | 4.58 | 522.71 | 1% | 1.029 | 0.044 |
| 35 | Collector | 8 | 144.04 | 0.30% | 3.76 | 312.28 | 1% | 0.677 | 0.051 |
| 36 | Collector | 8 | 612.23 | 0.40% | 40.23 | 364.53 | 11% | 1.531 | 0.150 |
| 37 | Collector | 10 | 327.90 | 0.40% | 163.20 | 650.44 | 25% | 2.211 | 0.285 |
| 38 | Collector | 8 | 264.14 | 0.20% | 7.62 | 264.73 | 3% | 0.747 | 0.078 |
| 39 | Collector | 8 | 247.66 | 0.50% | 3.76 | 398.51 | 1% | 0.803 | 0.046 |
| 40 | Collector | 8 | 360.17 | 0.30% | 11.29 | 277.52 | 4% | 0.868 | 0.092 |
| 41 | Collector | 8 | 373.36 | 0.20% | 1.80 | 241.61 | 1% | 0.453 | 0.041 |
| 43 | Collector | 12 | 593.16 | 0.20% | 84.04 | 678.74 | 12% | 1.310 | 0.238 |
| 44 | Collector | 12 | 569.13 | 0.30% | 0.00 | 921.01 | 0% | 0.000 | 0.000 |
| 45 | Collector | 8 | 334.47 | 0.30% | 0.00 | 312.43 | 0% | 0.000 | 0.000 |
| 46 | Collector | 8 | 553.55 | 0.20% | 32.02 | 269.35 | 12% | 1.156 | 0.155 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT
2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 47 | Collector | 8 | 624.97 | 0.30% | 0.00 | 312.36 | 0% | 0.000 | 0.000 |
| 48 | Collector | 8 | 314.68 | 0.30% | 36.59 | 272.47 | 13% | 1.212 | 0.165 |
| 49 | Collector | 6 | 555.28 | 0.30% | 6.23 | 141.63 | 4% | 0.806 | 0.071 |
| 50 | Collector | 8 | 320.56 | 0.50% | 6.10 | 378.75 | 2% | 0.897 | 0.059 |
| 51 | Collector | 8 | 631.90 | 0.30% | 0.00 | 312.37 | 0% | 0.000 | 0.000 |
| 52 | Interceptor | 10 | 599.13 | 0.20% | 25.91 | 465.60 | 6% | 1.023 | 0.133 |
| 53 | Collector | 8 | 619.71 | 0.10% | 10.19 | 129.79 | 8% | 0.493 | 0.126 |
| 54 | Collector | 8 | 409.84 | 0.30% | 0.00 | 312.34 | 0% | 0.000 | 0.000 |
| 55 | Collector | 8 | 623.13 | 0.10% | 13.20 | 192.52 | 7% | 0.703 | 0.118 |
| 56 | Collector | 8 | 627.36 | 0.40% | 3.04 | 361.02 | 1% | 0.702 | 0.043 |
| 57 | Collector | 8 | 354.37 | 0.30% | 3.76 | 312.34 | 1% | 0.677 | 0.051 |
| 58 | Collector | 8 | 429.13 | 0.30% | 0.00 | 312.38 | 0% | 0.000 | 0.000 |
| 59 | Interceptor | 10 | 596.02 | 0.40% | 78.47 | 589.70 | 13% | 1.674 | 0.205 |
| 60 | Interceptor | 15 | 644.18 | 0.10% | 606.25 | 1060.32 | 57% | 1.989 | 0.677 |
| 61 | Collector | 8 | 348.74 | 0.40% | 0.00 | 361.01 | 0% | 0.000 | 0.000 |
| 62 | Collector | 8 | 270.74 | 0.40% | 13.73 | 345.84 | 4% | 1.074 | 0.091 |
| 64 | Collector | 8 | 156.91 | 0.40% | 4.58 | 351.35 | 1% | 0.780 | 0.053 |
| 65 | Collector | 8 | 401.11 | 0.40% | 51.82 | 344.74 | 15% | 1.583 | 0.175 |
| 66 | Collector | 8 | 168.86 | 0.60% | 54.86 | 408.96 | 13% | 1.818 | 0.165 |
| 67 | Interceptor | 10 | 40.97 | -0.10% | 280.51 | | 100% | 1.146 | 0.833 |
| 68 | Interceptor | 10 | 396.59 | 0.20% | 272.97 | 424.17 | 64% | 1.841 | 0.486 |
| 69 | Collector | 8 | 299.77 | 0.40% | 23.49 | 342.34 | 7% | 1.251 | 0.118 |
| 70 | Collector | 8 | 216.79 | 0.30% | 0.00 | 312.30 | 0% | 0.000 | 0.000 |
| 73 | Collector | 8 | 238.17 | 0.50% | 3.76 | 392.86 | 1% | 0.795 | 0.046 |
| 74 | Collector | 8 | 346.96 | 0.40% | 30.48 | 355.76 | 9% | 1.388 | 0.132 |
| 75 | Collector | 8 | 235.87 | 0.40% | 9.15 | 363.69 | 3% | 0.985 | 0.073 |
| 76 | Collector | 8 | 180.39 | 0.50% | 7.62 | 373.94 | 2% | 0.950 | 0.066 |
| 77 | Collector | 8 | 383.36 | 0.40% | 12.20 | 348.23 | 4% | 1.041 | 0.085 |
| 78 | Collector | 8 | 256.72 | 0.30% | 3.04 | 285.58 | 1% | 0.597 | 0.048 |
| 79 | Interceptor | 12 | 629.37 | 0.20% | 84.04 | 715.39 | 12% | 1.360 | 0.231 |
| 80 | Collector | 8 | 902.97 | 0.30% | 7.53 | 300.21 | 3% | 0.812 | 0.073 |
| 81 | Collector | 8 | 648.65 | 0.30% | 41.13 | 303.62 | 14% | 1.353 | 0.166 |
| 83 | Collector | 8 | 239.37 | 0.20% | 49.18 | 241.99 | 20% | 1.211 | 0.204 |
| 84 | Collector | 8 | 1390.60 | 0.30% | 49.18 | 289.02 | 17% | 1.376 | 0.186 |
| 85 | Collector | 8 | 399.71 | 0.30% | 49.18 | 314.04 | 16% | 1.460 | 0.178 |
| 86 | Collector | 8 | 326.71 | 0.40% | 6.09 | 343.03 | 2% | 0.836 | 0.062 |
| 87 | Collector | 8 | 222.66 | 0.40% | 45.73 | 344.00 | 13% | 1.525 | 0.164 |
| 88 | Collector | 8 | 172.62 | 0.70% | 3.04 | 459.78 | 1% | 0.831 | 0.039 |
| 89 | Interceptor | 10 | 400.41 | 0.00% | 399.79 | 180.37 | 222% | 1.633 | 0.833 |
| 90 | Interceptor | 10 | 740.52 | 0.20% | 338.43 | 436.00 | 78% | 1.968 | 0.552 |
| 91 | Collector | 8 | 373.31 | 0.70% | 1.50 | 445.82 | 0% | 0.656 | 0.028 |
| 92 | Collector | 8 | 239.96 | 0.40% | 18.86 | 360.92 | 5% | 1.216 | 0.104 |
| 93 | Collector | 8 | 340.04 | 0.30% | 0.00 | 312.65 | 0% | 0.000 | 0.000 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT
2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|------------------------|
| 94 | Collector | 8 | 217.09 | 0.50% | 6.08 | 367.78 | 2% | 0.877 | 0.060 |
| 95 | Interceptor | 10 | 397.74 | 0.20% | 145.27 | 430.72 | 34% | 1.588 | 0.334 |
| 96 | Collector | 8 | 262.24 | 0.20% | 95.49 | 243.08 | 39% | 1.458 | 0.290 |
| 97 | Collector | 8 | 361.43 | 0.40% | 13.72 | 338.93 | 4% | 1.059 | 0.092 |
| 98 | Collector | 8 | 417.07 | 0.30% | 22.82 | 298.78 | 8% | 1.127 | 0.125 |
| 99 | Collector | 8 | 389.89 | 0.20% | 7.60 | 226.43 | 3% | 0.669 | 0.084 |
| 100 | Collector | 8 | 449.30 | 0.40% | 6.10 | 338.22 | 2% | 0.829 | 0.062 |
| 101 | Collector | 8 | 399.01 | 1.90% | 1.12 | 746.25 | 0% | 0.857 | 0.019 |
| 102 | Collector | 8 | 353.45 | 0.50% | 1.12 | 379.90 | 0% | 0.536 | 0.026 |
| 103 | Collector | 8 | 234.66 | 2.80% | 0.37 | 908.81 | 0% | 0.702 | 0.011 |
| 104 | Collector | 8 | 588.44 | 2.00% | 23.52 | 770.89 | 3% | 2.212 | 0.080 |
| 105 | Collector | 8 | 300.50 | 0.00% | 4.54 | | 100% | 0.029 | 0.667 |
| 106 | Collector | 8 | 432.13 | 0.20% | 1.50 | 261.73 | 1% | 0.453 | 0.036 |
| 107 | Collector | 8 | 871.72 | 0.40% | 3.04 | 362.99 | 1% | 0.705 | 0.043 |
| 108 | Collector | 8 | 407.47 | 0.30% | 4.57 | 299.62 | 2% | 0.698 | 0.057 |
| 109 | Collector | 8 | 236.21 | 0.70% | 0.00 | 443.20 | 0% | 0.000 | 0.000 |
| 110 | Collector | 8 | 491.49 | 0.30% | 0.00 | 312.40 | 0% | 0.000 | 0.000 |
| 111 | Collector | 8 | 298.60 | 0.00% | 1.62 | 58.03 | 3% | 0.162 | 0.077 |
| 112 | Collector | 8 | 581.30 | 0.30% | 0.00 | 312.36 | 0% | 0.000 | 0.000 |
| 113 | Collector | 8 | 295.38 | 0.60% | 30.96 | 420.12 | 7% | 1.568 | 0.122 |
| 114 | Collector | 8 | 157.24 | 0.30% | 0.00 | 312.42 | 0% | 0.000 | 0.000 |
| 115 | Collector | 8 | 507.62 | 0.30% | 50.78 | 312.38 | 16% | 1.467 | 0.182 |
| 116 | Collector | 8 | 390.31 | 0.40% | 133.51 | 362.25 | 37% | 2.137 | 0.280 |
| 117 | Collector | 8 | 269.15 | 0.40% | 0.00 | 343.67 | 0% | 0.000 | 0.000 |
| 118 | Collector | 8 | 89.34 | 0.60% | 0.00 | 418.46 | 0% | 0.000 | 0.000 |
| 119 | Collector | 8 | 156.90 | 0.50% | 0.00 | 380.71 | 0% | 0.000 | 0.000 |
| 121 | Collector | 8 | 239.87 | 0.40% | 1.89 | 321.81 | 1% | 0.561 | 0.037 |
| 122 | Collector | 8 | 723.73 | 0.30% | 0.00 | 312.37 | 0% | 0.000 | 0.000 |
| 123 | Collector | 8 | 476.50 | 0.20% | 1.50 | 211.68 | 1% | 0.391 | 0.040 |
| 124 | Collector | 8 | 287.48 | 0.50% | 177.04 | 369.47 | 48% | 2.333 | 0.325 |
| 125 | Collector | 10 | 624.05 | 0.10% | 119.77 | 356.32 | 34% | 1.312 | 0.333 |
| 126 | Collector | 8 | 302.87 | 0.40% | 7.52 | 360.50 | 2% | 0.923 | 0.067 |
| 127 | Collector | 8 | 177.29 | 0.50% | 7.62 | 376.98 | 2% | 0.956 | 0.066 |
| 128 | Collector | 8 | 289.20 | 0.30% | 3.04 | 317.20 | 1% | 0.642 | 0.046 |
| 129 | Collector | 8 | 269.55 | 0.30% | 0.00 | 312.47 | 0% | 0.000 | 0.000 |
| 130 | Collector | 8 | 914.53 | 0.20% | 1.97 | 264.22 | 1% | 0.495 | 0.041 |
| 131 | Collector | 8 | 60.75 | 0.30% | 0.00 | 312.02 | 0% | 0.000 | 0.000 |
| 132 | Collector | 8 | 194.19 | 0.30% | 0.00 | 312.43 | 0% | 0.000 | 0.000 |
| 133 | Collector | 12 | 566.19 | 0.20% | 180.74 | 658.48 | 27% | 1.593 | 0.358 |
| 134 | Collector | 12 | 338.77 | 0.30% | 0.00 | 921.06 | 0% | 0.000 | 0.000 |
| 135 | Collector | 12 | 466.70 | 0.30% | 0.00 | 921.01 | 0% | 0.000 | 0.000 |
| 137 | Collector | 8 | 282.96 | 1.30% | 0.00 | 620.49 | 0% | 0.000 | 0.000 |
| 138 | Interceptor | 10 | 322.28 | 0.30% | 0.00 | 580.47 | 0% | 0.000 | 0.000 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|------------------------|
| 139 | Collector | 8 | 300.17 | 0.20% | 7.62 | 245.55 | 3% | 0.708 | 0.081 |
| 140 | Collector | 8 | 185.45 | 1.30% | 0.00 | 612.68 | 0% | 0.000 | 0.000 |
| 141 | Collector | 8 | 280.29 | 0.40% | 1.50 | 332.04 | 1% | 0.534 | 0.032 |
| 142 | Collector | 8 | 297.23 | 0.60% | 7.60 | 428.56 | 2% | 1.045 | 0.062 |
| 143 | Collector | 8 | 277.01 | 0.70% | 17.44 | 443.92 | 4% | 1.374 | 0.090 |
| 144 | Collector | 8 | 335.33 | 4.50% | 22.02 | 1156.83 | 2% | 2.881 | 0.064 |
| 145 | Collector | 8 | 342.81 | 0.30% | 23.52 | 285.82 | 8% | 1.102 | 0.129 |
| 146 | Collector | 8 | 59.64 | 2.50% | 28.09 | 864.17 | 3% | 2.528 | 0.082 |
| 147 | Collector | 8 | 46.39 | 5.30% | 28.09 | 1255.60 | 2% | 3.283 | 0.069 |
| 148 | Collector | 8 | 111.89 | 2.20% | 0.37 | 808.44 | 0% | 0.647 | 0.011 |
| 149 | Collector | 8 | 122.84 | 1.90% | 0.37 | 751.34 | 0% | 0.615 | 0.012 |
| 150 | Collector | 8 | 292.70 | 0.00% | 0.37 | 52.23 | 1% | 0.097 | 0.040 |
| 151 | Collector | 8 | 224.64 | 0.40% | 0.74 | 341.32 | 0% | 0.440 | 0.023 |
| 152 | Collector | 8 | 235.12 | 0.50% | 1.12 | 365.30 | 0% | 0.522 | 0.027 |
| 153 | Collector | 8 | 319.03 | 0.40% | 18.13 | 324.50 | 6% | 1.116 | 0.107 |
| 154 | Collector | 8 | 185.90 | 0.20% | 22.71 | 267.55 | 9% | 1.041 | 0.131 |
| 155 | Collector | 8 | 336.42 | 0.20% | 4.57 | 270.59 | 2% | 0.650 | 0.060 |
| 156 | Collector | 8 | 261.95 | 0.30% | 7.46 | 296.36 | 3% | 0.803 | 0.073 |
| 157 | Collector | 8 | 237.50 | 1.30% | 4.54 | 617.27 | 1% | 1.153 | 0.041 |
| 158 | Collector | 8 | 513.61 | 0.30% | 1.50 | 310.27 | 1% | 0.510 | 0.033 |
| 159 | Collector | 8 | 418.83 | 0.20% | 0.00 | 251.52 | 0% | 0.000 | 0.000 |
| 160 | Collector | 8 | 401.81 | 0.50% | 1.50 | 398.16 | 0% | 0.606 | 0.030 |
| 161 | Collector | 8 | 365.06 | 0.60% | 1.50 | 417.72 | 0% | 0.627 | 0.029 |
| 162 | Collector | 8 | 297.32 | 0.00% | 1.50 | | | 0.010 | 0.667 |
| 163 | Collector | 8 | 302.41 | 0.30% | 1.50 | 314.58 | 1% | 0.515 | 0.033 |
| 164 | Collector | 8 | 301.34 | 0.20% | 1.50 | 270.03 | 1% | 0.463 | 0.036 |
| 165 | Collector | 8 | 300.98 | 0.20% | 40.29 | 254.27 | 16% | 1.186 | 0.179 |
| 166 | Collector | 8 | 351.57 | 0.20% | 47.88 | 225.77 | 21% | 1.144 | 0.208 |
| 167 | Collector | 8 | 398.37 | 0.20% | 52.45 | 212.10 | 25% | 1.122 | 0.226 |
| 170 | Collector | 8 | 358.17 | 0.30% | 16.41 | 277.10 | 6% | 0.969 | 0.110 |
| 172 | Collector | 8 | 173.32 | 0.40% | 3.04 | 360.34 | 1% | 0.702 | 0.043 |
| 173 | Collector | 8 | 114.20 | 0.50% | 1.50 | 392.86 | 0% | 0.601 | 0.030 |
| 174 | Collector | 8 | 247.08 | 0.50% | 4.54 | 384.93 | 1% | 0.830 | 0.051 |
| 175 | Collector | 8 | 209.84 | 0.40% | 10.64 | 359.88 | 3% | 1.023 | 0.079 |
| 176 | Collector | 8 | 132.64 | 0.20% | 15.91 | 270.83 | 6% | 0.945 | 0.110 |
| 178 | Collector | 8 | 397.34 | 0.20% | 66.53 | 257.80 | 26% | 1.380 | 0.231 |
| 179 | Collector | 8 | 352.02 | 0.30% | 74.15 | 291.28 | 26% | 1.553 | 0.229 |
| 180 | Collector | 8 | 394.74 | 0.30% | 81.77 | 278.18 | 29% | 1.543 | 0.248 |
| 181 | Collector | 8 | 137.33 | 0.60% | 119.82 | 414.02 | 29% | 2.287 | 0.246 |
| 182 | Collector | 8 | 128.46 | 1.10% | 2.62 | 576.35 | 1% | 0.929 | 0.032 |
| 183 | Collector | 8 | 415.93 | 0.60% | 2.62 | 423.62 | 1% | 0.750 | 0.038 |
| 184 | Interceptor | 10 | 306.97 | 0.20% | 122.43 | 425.24 | 29% | 1.501 | 0.306 |
| 185 | Collector | 8 | 383.97 | 0.50% | 1.12 | 397.73 | 0% | 0.554 | 0.026 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT
2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 186 | Collector | 8 | 399.93 | 0.50% | 1.12 | 399.09 | 0% | 0.555 | 0.026 |
| 187 | Collector | 8 | 298.47 | 0.50% | 6.10 | 372.30 | 2% | 0.886 | 0.059 |
| 188 | Interceptor | 10 | 595.05 | 0.10% | 30.48 | 323.11 | 9% | 0.830 | 0.173 |
| 189 | Collector | 10 | 601.22 | 0.60% | 18.42 | 775.37 | 2% | 1.321 | 0.089 |
| 191 | Collector | 8 | 298.14 | 0.30% | 24.40 | 319.01 | 8% | 1.203 | 0.125 |
| 192 | Collector | 8 | 294.77 | 0.30% | 18.30 | 294.24 | 6% | 1.044 | 0.113 |
| 193 | Collector | 8 | 294.62 | 0.20% | 18.30 | 262.02 | 7% | 0.962 | 0.119 |
| 194 | Collector | 8 | 627.30 | 0.20% | 51.91 | 240.21 | 22% | 1.224 | 0.210 |
| 195 | Collector | 8 | 592.09 | 0.40% | 41.24 | 348.30 | 12% | 1.493 | 0.155 |
| 196 | Collector | 8 | 269.67 | 0.30% | 26.54 | 281.96 | 9% | 1.131 | 0.138 |
| 197 | Collector | 8 | 298.12 | 0.80% | 0.00 | 471.48 | 0% | 0.000 | 0.000 |
| 198 | Collector | 8 | 309.92 | 0.80% | 16.78 | 487.04 | 3% | 1.449 | 0.085 |
| 199 | Collector | 8 | 307.07 | 0.40% | 1.62 | 345.43 | 1% | 0.562 | 0.033 |
| 200 | Collector | 8 | 306.09 | 0.30% | 38.58 | 316.37 | 12% | 1.368 | 0.157 |
| 201 | Collector | 8 | 168.71 | 0.30% | 0.00 | 312.46 | 0% | 0.000 | 0.000 |
| 202 | Collector | 8 | 57.67 | 0.30% | 0.00 | 312.13 | 0% | 0.000 | 0.000 |
| 203 | Collector | 8 | 292.81 | 0.00% | 0.25 | 52.22 | 1% | 0.085 | 0.033 |
| 204 | Collector | 8 | 210.72 | 0.50% | 22.01 | 368.20 | 6% | 1.291 | 0.111 |
| 205 | Collector | 8 | 234.04 | 0.30% | 77.97 | 295.70 | 26% | 1.592 | 0.234 |
| 206 | Collector | 8 | 226.50 | 0.40% | 0.00 | 363.86 | 0% | 0.000 | 0.000 |
| 207 | Collector | 8 | 230.58 | 0.40% | 88.63 | 325.67 | 27% | 1.769 | 0.238 |
| 208 | Collector | 8 | 188.93 | 1.50% | 28.11 | 656.92 | 4% | 2.086 | 0.094 |
| 209 | Collector | 8 | 111.08 | 0.50% | 124.36 | 373.85 | 33% | 2.145 | 0.265 |
| 210 | Collector | 8 | 66.12 | -3.60% | 130.46 | | 100% | 0.833 | 0.667 |
| 211 | Collector | 8 | 134.27 | 0.40% | 3.04 | 362.61 | 1% | 0.705 | 0.043 |
| 212 | Collector | 8 | 45.89 | 0.10% | 133.51 | 194.99 | 69% | 1.340 | 0.405 |
| 213 | Collector | 8 | 319.88 | 0.40% | 135.25 | 346.94 | 39% | 2.077 | 0.289 |
| 214 | Collector | 8 | 309.65 | 0.40% | 142.78 | 332.98 | 43% | 2.044 | 0.305 |
| 215 | Collector | 8 | 290.66 | 0.40% | 150.40 | 364.24 | 41% | 2.214 | 0.299 |
| 216 | Collector | 8 | 292.79 | 0.30% | 3.76 | 312.35 | 1% | 0.677 | 0.051 |
| 217 | Collector | 8 | 352.34 | 0.50% | 0.00 | 380.83 | 0% | 0.000 | 0.000 |
| 218 | Collector | 8 | 37.39 | -0.20% | 0.00 | | 100% | 0.000 | 0.000 |
| 219 | Interceptor | 10 | 399.50 | 0.30% | 125.48 | 522.29 | 24% | 1.754 | 0.278 |
| 220 | Interceptor | 10 | 400.05 | 0.10% | 126.98 | 357.52 | 36% | 1.336 | 0.343 |
| 221 | Interceptor | 10 | 398.91 | 0.20% | 126.98 | 439.33 | 29% | 1.553 | 0.307 |
| 222 | Interceptor | 10 | 401.39 | 0.10% | 130.02 | 285.27 | 46% | 1.138 | 0.395 |
| 223 | Collector | 8 | 321.12 | 0.30% | 0.00 | 283.86 | 0% | 0.000 | 0.000 |
| 224 | Interceptor | 10 | 625.38 | 0.10% | 35.06 | 323.93 | 11% | 0.866 | 0.185 |
| 225 | Interceptor | 10 | 596.70 | 0.30% | 53.36 | 580.45 | 9% | 1.479 | 0.171 |
| 226 | Collector | 8 | 524.65 | 0.30% | 0.00 | 312.36 | 0% | 0.000 | 0.000 |
| 227 | Collector | 8 | 596.77 | 0.20% | 32.57 | 240.27 | 14% | 1.071 | 0.166 |
| 228 | Collector | 8 | 630.23 | 0.40% | 28.49 | 362.92 | 8% | 1.380 | 0.126 |
| 229 | Collector | 8 | 595.03 | 0.40% | 20.81 | 342.18 | 6% | 1.206 | 0.111 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 230 | Collector | 8 | 311.51 | 0.20% | 54.86 | 240.64 | 23% | 1.244 | 0.216 |
| 231 | Collector | 8 | 318.62 | 0.30% | 47.24 | 289.66 | 16% | 1.362 | 0.182 |
| 232 | Collector | 8 | 51.40 | 2.10% | 45.74 | 788.28 | 6% | 2.741 | 0.109 |
| 234 | Collector | 8 | 628.25 | 0.20% | 15.83 | 260.26 | 6% | 0.917 | 0.111 |
| 235 | Collector | 8 | 628.10 | 0.20% | 77.65 | 235.20 | 33% | 1.347 | 0.264 |
| 236 | Collector | 8 | 460.30 | 0.30% | 0.00 | 312.39 | 0% | 0.000 | 0.000 |
| 237 | Collector | 10 | 602.01 | 0.20% | 106.88 | 459.59 | 23% | 1.529 | 0.273 |
| 238 | Collector | 10 | 249.65 | 0.30% | 123.99 | 533.17 | 23% | 1.774 | 0.273 |
| 239 | Collector | 10 | 298.19 | 0.10% | 127.04 | 361.58 | 35% | 1.348 | 0.341 |
| 240 | Collector | 10 | 302.21 | 0.60% | 130.09 | 768.51 | 17% | 2.338 | 0.232 |
| 241 | Collector | 8 | 278.02 | 0.20% | 3.04 | 219.51 | 1% | 0.497 | 0.055 |
| 242 | Collector | 8 | 124.08 | 0.40% | 7.62 | 336.82 | 2% | 0.884 | 0.069 |
| 243 | Collector | 8 | 297.44 | 0.40% | 172.46 | 349.27 | 49% | 2.222 | 0.331 |
| 245 | Collector | 8 | 576.99 | -0.80% | 7.52 | | 100% | 0.048 | 0.667 |
| 246 | Collector | 8 | 327.10 | 0.30% | 7.52 | 319.90 | 2% | 0.849 | 0.071 |
| 247 | Collector | 8 | 286.59 | 0.50% | 172.46 | 376.67 | 46% | 2.351 | 0.317 |
| 250 | Collector | 8 | 70.41 | 0.90% | 3.76 | 503.67 | 1% | 0.944 | 0.041 |
| 251 | Collector | 8 | 111.07 | 0.40% | 14.28 | 348.82 | 4% | 1.093 | 0.092 |
| 252 | Interceptor | 10 | 399.14 | 0.20% | 149.85 | 406.07 | 37% | 1.533 | 0.350 |
| 253 | Interceptor | 10 | 163.27 | 0.10% | 152.89 | 348.53 | 44% | 1.377 | 0.386 |
| 256 | Collector | 10 | 594.56 | 0.40% | 33.00 | 660.49 | 5% | 1.406 | 0.127 |
| 257 | Collector | 10 | 59.02 | 0.90% | 0.00 | 912.97 | 0% | 0.000 | 0.000 |
| 258 | Interceptor | 12 | 625.45 | 0.20% | 442.55 | 676.66 | 65% | 2.046 | 0.590 |
| 259 | Collector | 8 | 206.62 | 0.20% | 0.00 | 267.51 | 0% | 0.000 | 0.000 |
| 260 | Collector | 8 | 182.89 | 0.40% | 3.76 | 348.47 | 1% | 0.731 | 0.049 |
| 261 | Collector | 10 | 277.94 | 0.50% | 287.64 | 695.52 | 41% | 2.707 | 0.373 |
| 262 | Collector | 8 | 629.32 | 0.10% | 55.61 | 204.39 | 27% | 1.110 | 0.238 |
| 263 | Collector | 8 | 280.18 | 0.40% | 4.46 | 334.80 | 1% | 0.749 | 0.054 |
| 266 | Collector | 10 | 298.85 | 0.40% | 139.21 | 594.10 | 23% | 1.981 | 0.274 |
| 267 | Collector | 10 | 302.49 | 0.30% | 140.71 | 509.59 | 28% | 1.779 | 0.299 |
| 268 | Collector | 10 | 297.23 | 0.30% | 160.16 | 544.96 | 29% | 1.935 | 0.309 |
| 269 | Interceptor | 8 | 84.59 | 0.40% | 814.20 | 344.26 | 237% | 5.197 | 0.667 |
| 270 | Collector | 8 | 270.19 | 0.30% | 4.57 | 294.98 | 2% | 0.690 | 0.058 |
| 272 | Collector | 8 | 162.39 | 0.50% | 4.58 | 398.72 | 1% | 0.852 | 0.050 |
| 273 | Collector | 8 | 101.42 | 0.50% | 15.23 | 381.05 | 4% | 1.186 | 0.091 |
| 274 | Collector | 8 | 218.11 | 0.50% | 64.02 | 369.13 | 17% | 1.766 | 0.188 |
| 275 | Collector | 8 | 271.96 | 0.40% | 19.82 | 358.20 | 6% | 1.228 | 0.106 |
| 276 | Collector | 8 | 389.96 | 0.50% | 18.86 | 379.58 | 5% | 1.260 | 0.101 |
| 277 | Collector | 8 | 171.31 | 0.80% | 21.90 | 495.97 | 4% | 1.590 | 0.095 |
| 278 | Interceptor | 10 | 238.02 | 0.20% | 152.89 | 453.71 | 34% | 1.672 | 0.333 |
| 279 | Interceptor | 10 | 398.53 | 0.10% | 183.94 | 275.88 | 67% | 1.207 | 0.498 |
| 280 | Interceptor | 10 | 363.03 | 0.20% | 274.47 | 433.58 | 63% | 1.874 | 0.481 |
| 281 | Collector | 8 | 201.13 | 0.50% | 25.01 | 379.21 | 7% | 1.369 | 0.116 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT
2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 282 | Interceptor | 10 | 36.87 | 0.00% | 183.94 | 170.30 | 108% | 0.751 | 0.833 |
| 283 | Collector | 8 | 286.29 | 0.50% | 4.54 | 383.12 | 1% | 0.827 | 0.051 |
| 284 | Collector | 8 | 196.27 | -0.40% | 1.50 | | 100% | 0.010 | 0.667 |
| 285 | Collector | 8 | 180.71 | 0.40% | 1.50 | 357.95 | 0% | 0.563 | 0.031 |
| 286 | Collector | 8 | 140.86 | 0.40% | 18.91 | 350.15 | 5% | 1.192 | 0.105 |
| 288 | Collector | 8 | 517.38 | 0.30% | 41.13 | 303.73 | 14% | 1.354 | 0.166 |
| 289 | Collector | 8 | 216.12 | 0.30% | 41.13 | 316.27 | 13% | 1.393 | 0.162 |
| 290 | Collector | 8 | 301.18 | 0.40% | 7.53 | 333.83 | 2% | 0.875 | 0.069 |
| 291 | Collector | 8 | 105.57 | 0.30% | 48.66 | 314.01 | 16% | 1.455 | 0.177 |
| 292 | Collector | 8 | 399.19 | -0.10% | 0.00 | | 100% | 0.000 | 0.000 |
| 293 | Collector | 8 | 158.91 | 0.70% | 49.18 | 454.08 | 11% | 1.897 | 0.148 |
| 295 | Collector | 8 | 401.16 | 0.20% | 49.18 | 214.64 | 23% | 1.111 | 0.217 |
| 296 | Collector | 8 | 398.36 | 0.20% | 49.18 | 231.83 | 21% | 1.175 | 0.208 |
| 297 | Collector | 8 | 325.51 | 0.40% | 3.04 | 337.53 | 1% | 0.670 | 0.045 |
| 298 | Collector | 8 | 275.35 | 0.40% | 12.19 | 345.27 | 4% | 1.035 | 0.086 |
| 299 | Collector | 8 | 380.20 | 0.10% | 61.36 | 124.10 | 49% | 0.790 | 0.331 |
| 300 | Collector | 8 | 34.37 | 0.60% | 49.18 | 412.78 | 12% | 1.773 | 0.155 |
| 301 | Interceptor | 10 | 374.71 | 0.10% | 399.79 | 310.25 | 129% | 1.633 | 0.833 |
| 302 | Interceptor | 10 | 391.37 | 0.10% | 399.79 | 305.61 | 131% | 1.633 | 0.833 |
| 303 | Interceptor | 10 | 573.11 | 0.10% | 335.37 | 380.61 | 88% | 1.755 | 0.607 |
| 304 | Interceptor | 10 | 315.08 | 0.30% | 399.79 | 541.97 | 74% | 2.422 | 0.532 |
| 305 | Interceptor | 10 | 241.48 | 0.00% | 399.79 | 177.21 | 226% | 1.633 | 0.833 |
| 306 | Collector | 8 | 300.12 | 1.00% | 35.71 | 543.06 | 7% | 1.959 | 0.116 |
| 307 | Collector | 8 | 193.95 | 0.90% | 28.09 | 511.06 | 6% | 1.748 | 0.106 |
| 308 | Interceptor | 15 | 519.24 | 0.30% | 601.30 | 1669.73 | 36% | 2.784 | 0.519 |
| 309 | Collector | 8 | 591.78 | 0.30% | 0.00 | 312.40 | 0% | 0.000 | 0.000 |
| 310 | Collector | 8 | 320.26 | 0.30% | 5.26 | 293.67 | 2% | 0.718 | 0.062 |
| 311 | Collector | 8 | 294.92 | 0.40% | 3.76 | 361.46 | 1% | 0.750 | 0.048 |
| 312 | Collector | 8 | 336.16 | 0.30% | 3.76 | 297.63 | 1% | 0.655 | 0.053 |
| 313 | Collector | 8 | 327.47 | 0.40% | 3.76 | 361.36 | 1% | 0.750 | 0.048 |
| 314 | Collector | 8 | 249.58 | 0.50% | 0.00 | 387.30 | 0% | 0.000 | 0.000 |
| 315 | Collector | 8 | 301.61 | 0.40% | 3.76 | 330.05 | 1% | 0.704 | 0.050 |
| 316 | Collector | 8 | 316.50 | 0.60% | 3.76 | 421.78 | 1% | 0.835 | 0.045 |
| 317 | Collector | 8 | 296.69 | 0.20% | 3.76 | 234.77 | 2% | 0.555 | 0.059 |
| 318 | Collector | 8 | 341.12 | 0.30% | 3.76 | 311.88 | 1% | 0.677 | 0.051 |
| 320 | Collector | 8 | 347.72 | 0.50% | 33.54 | 367.84 | 9% | 1.461 | 0.136 |
| 321 | Collector | 8 | 225.81 | 0.40% | 7.62 | 349.17 | 2% | 0.906 | 0.068 |
| 322 | Collector | 8 | 172.55 | 0.40% | 11.29 | 335.81 | 3% | 0.992 | 0.084 |
| 323 | Collector | 8 | 137.41 | 0.30% | 11.29 | 315.66 | 4% | 0.950 | 0.086 |
| 324 | Collector | 8 | 265.46 | 0.50% | 3.76 | 386.51 | 1% | 0.786 | 0.046 |
| 325 | Collector | 8 | 600.96 | 0.30% | 3.76 | 319.39 | 1% | 0.688 | 0.051 |
| 327 | Collector | 8 | 503.82 | 0.30% | 10.52 | 296.82 | 4% | 0.891 | 0.086 |
| 328 | Collector | 8 | 304.84 | 0.30% | 5.54 | 315.79 | 2% | 0.767 | 0.061 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 331 | Collector | 8 | 337.23 | 0.50% | 6.65 | 378.88 | 2% | 0.921 | 0.061 |
| 332 | Collector | 8 | 234.41 | 0.30% | 66.53 | 292.03 | 23% | 1.510 | 0.216 |
| 333 | Collector | 8 | 52.05 | 0.80% | 66.53 | 482.65 | 14% | 2.162 | 0.167 |
| 334 | Collector | 8 | 159.11 | 0.40% | 66.53 | 351.03 | 19% | 1.723 | 0.197 |
| 335 | Collector | 8 | 270.91 | 0.20% | 60.44 | 258.25 | 23% | 1.345 | 0.219 |
| 336 | Collector | 8 | 104.79 | 0.40% | 58.55 | 331.33 | 18% | 1.594 | 0.190 |
| 337 | Collector | 8 | 293.08 | 0.40% | 5.49 | 364.40 | 2% | 0.845 | 0.057 |
| 338 | Collector | 8 | 354.55 | 0.30% | 0.37 | 318.99 | 0% | 0.339 | 0.017 |
| 339 | Collector | 8 | 496.45 | 0.30% | 0.00 | 312.36 | 0% | 0.000 | 0.000 |
| 340 | Interceptor | 15 | 304.28 | 0.20% | 606.25 | 1341.54 | 45% | 2.374 | 0.589 |
| 341 | Interceptor | 15 | 312.25 | 0.10% | 607.75 | 1037.86 | 59% | 1.958 | 0.687 |
| 342 | Interceptor | 15 | 335.35 | 0.10% | 772.45 | 886.70 | 87% | 1.814 | 0.903 |
| 343 | Interceptor | 15 | 301.60 | 0.30% | 772.45 | 1542.36 | 50% | 2.801 | 0.626 |
| 344 | Collector | 8 | 594.21 | 0.20% | 55.02 | 212.46 | 26% | 1.138 | 0.231 |
| 345 | Collector | 8 | 595.49 | 0.20% | 77.89 | 255.15 | 31% | 1.430 | 0.253 |
| 346 | Collector | 8 | 594.29 | 0.30% | 28.81 | 320.17 | 9% | 1.267 | 0.135 |
| 347 | Collector | 8 | 547.50 | 0.30% | 7.62 | 312.41 | 2% | 0.838 | 0.072 |
| 348 | Collector | 10 | 319.46 | -0.10% | 281.54 | | 100% | 1.150 | 0.833 |
| 349 | Collector | 12 | 595.07 | 0.20% | 115.37 | 757.99 | 15% | 1.553 | 0.264 |
| 350 | Collector | 12 | 326.74 | 0.10% | 171.68 | 532.93 | 32% | 1.347 | 0.390 |
| 351 | Collector | 12 | 267.73 | 0.70% | 171.68 | 1373.93 | 13% | 2.659 | 0.239 |
| 352 | Collector | 8 | 268.75 | 0.90% | 0.00 | 512.07 | 0% | 0.000 | 0.000 |
| 353 | Collector | 8 | 195.92 | 0.30% | 0.00 | 300.69 | 0% | 0.000 | 0.000 |
| 354 | Collector | 8 | 280.56 | 1.10% | 0.00 | 572.91 | 0% | 0.000 | 0.000 |
| 355 | Collector | 8 | 62.10 | -0.80% | 0.00 | | 100% | 0.000 | 0.000 |
| 356 | Collector | 8 | 145.86 | 1.80% | 4.22 | 719.73 | 1% | 1.254 | 0.037 |
| 357 | Interceptor | 10 | 180.27 | 0.30% | 158.99 | 561.20 | 28% | 1.973 | 0.303 |
| 358 | Collector | 8 | 102.98 | 0.10% | 15.23 | 185.64 | 8% | 0.715 | 0.129 |
| 359 | Collector | 8 | 306.96 | 0.80% | 7.53 | 491.05 | 2% | 1.145 | 0.058 |
| 360 | Collector | 8 | 235.41 | 0.40% | 17.39 | 362.83 | 5% | 1.192 | 0.099 |
| 361 | Collector | 8 | 262.08 | 0.20% | 39.63 | 268.31 | 15% | 1.226 | 0.173 |
| 362 | Collector | 8 | 247.11 | 0.40% | 38.13 | 355.32 | 11% | 1.480 | 0.147 |
| 363 | Collector | 8 | 217.40 | 0.30% | 0.00 | 312.30 | 0% | 0.000 | 0.000 |
| 364 | Collector | 8 | 326.16 | 0.30% | 12.92 | 320.65 | 4% | 1.000 | 0.091 |
| 365 | Collector | 8 | 216.66 | 0.40% | 0.00 | 331.68 | 0% | 0.000 | 0.000 |
| 366 | Interceptor | 10 | 290.27 | 0.50% | 140.70 | 723.29 | 20% | 2.289 | 0.249 |
| 367 | Collector | 8 | 361.00 | 0.40% | 6.10 | 341.42 | 2% | 0.834 | 0.062 |
| 368 | Collector | 8 | 86.95 | 0.00% | 12.03 | | 100% | 0.077 | 0.667 |
| 369 | Collector | 8 | 314.73 | 1.50% | 15.96 | 655.28 | 2% | 1.757 | 0.072 |
| 370 | Collector | 8 | 247.57 | 0.30% | 49.18 | 291.42 | 17% | 1.384 | 0.185 |
| 371 | Collector | 8 | 151.21 | -0.40% | 49.18 | | 100% | 0.314 | 0.667 |
| 372 | Interceptor | 10 | 402.96 | 0.20% | 399.79 | 415.62 | 96% | 1.934 | 0.656 |
| 373 | Interceptor | 10 | 401.97 | 0.10% | 399.79 | 343.90 | 116% | 1.633 | 0.833 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT
2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|--------|---------------|--------------------|------------------|--------------------|------------------------|
| 374 | Collector | 8 | 297.04 | 0.10% | 4.42 | 182.89 | 2% | 0.489 | 0.071 |
| 375 | Collector | 8 | 592.49 | 0.10% | 28.81 | 192.83 | 15% | 0.884 | 0.174 |
| 376 | Collector | 10 | 595.46 | 0.20% | 352.41 | 482.67 | 73% | 2.152 | 0.529 |
| 377 | Collector | 10 | 595.24 | 0.50% | 172.82 | 689.04 | 25% | 2.342 | 0.284 |
| 378 | Collector | 12 | 566.32 | 0.40% | 4.66 | 1036.11 | 0% | 0.740 | 0.048 |
| 379 | Collector | 12 | 338.12 | 0.10% | 188.36 | 448.86 | 42% | 1.218 | 0.452 |
| 380 | Collector | 8 | 350.38 | 0.70% | 16.66 | 453.80 | 4% | 1.377 | 0.087 |
| 381 | Interceptor | 10 | 629.02 | 0.50% | 125.75 | 684.21 | 18% | 2.131 | 0.242 |
| 382 | Collector | 12 | 616.84 | 0.30% | 4.95 | 879.00 | 1% | 0.673 | 0.054 |
| 383 | Collector | 8 | 205.11 | 0.30% | 0.00 | 287.42 | 0% | 0.000 | 0.000 |
| 384 | Collector | 8 | 479.50 | 0.30% | 3.76 | 312.35 | 1% | 0.677 | 0.051 |
| 385 | Collector | 8 | 588.61 | 0.60% | 14.33 | 412.27 | 4% | 1.230 | 0.085 |
| 386 | Collector | 8 | 367.39 | 0.20% | 61.36 | 216.81 | 28% | 1.190 | 0.243 |
| 387 | Collector | 8 | 110.16 | 0.40% | 11.29 | 342.50 | 3% | 1.006 | 0.083 |
| 388 | Collector | 8 | 123.22 | 0.60% | 11.29 | 430.71 | 3% | 1.181 | 0.074 |
| 389 | Collector | 8 | 125.87 | 0.20% | 3.76 | 231.95 | 2% | 0.550 | 0.059 |
| 390 | Collector | 8 | 176.18 | 0.40% | 48.77 | 340.56 | 14% | 1.543 | 0.170 |
| 391 | Collector | 8 | 215.49 | 0.50% | 6.08 | 382.66 | 2% | 0.902 | 0.059 |
| 392 | Collector | 8 | 224.71 | 0.40% | 16.77 | 342.81 | 5% | 1.133 | 0.100 |
| 393 | Collector | 8 | 86.72 | -0.10% | 66.53 | | 100% | 0.425 | 0.667 |
| 394 | Collector | 8 | 156.92 | 0.40% | 5.49 | 328.61 | 2% | 0.787 | 0.060 |
| 395 | Collector | 8 | 240.04 | 0.40% | 70.35 | 324.55 | 22% | 1.655 | 0.211 |
| 396 | Collector | 8 | 79.99 | 0.00% | 0.00 | | 0% | 0.000 | 0.000 |
| 397 | Collector | 8 | 110.48 | 5.80% | 0.00 | 1305.24 | 0% | 0.000 | 0.000 |
| 398 | Interceptor | 8 | 93.77 | 0.40% | 814.20 | 344.35 | 236% | 5.197 | 0.667 |
| 399 | Collector | 10 | 279.37 | 0.30% | 3.04 | 536.13 | 1% | 0.592 | 0.045 |
| 400 | Collector | 10 | 298.73 | 0.30% | 131.59 | 502.85 | 26% | 1.729 | 0.291 |
| 401 | Collector | 8 | 159.95 | 2.00% | 5.03 | 774.80 | 1% | 1.393 | 0.038 |
| 402 | Collector | 8 | 158.10 | 0.10% | 5.03 | 180.40 | 3% | 0.504 | 0.077 |
| 403 | Collector | 8 | 297.93 | 0.40% | 22.86 | 364.02 | 6% | 1.296 | 0.113 |
| 404 | Collector | 8 | 116.19 | 0.40% | 0.00 | 348.07 | 0% | 0.000 | 0.000 |
| 405 | Collector | 8 | 150.68 | 0.30% | 3.04 | 295.86 | 1% | 0.612 | 0.048 |
| 406 | Collector | 8 | 246.31 | 0.30% | 3.04 | 295.64 | 1% | 0.611 | 0.048 |
| 407 | Collector | 8 | 404.77 | 0.30% | 3.04 | 295.72 | 1% | 0.611 | 0.048 |
| 408 | Collector | 8 | 181.21 | 0.30% | 3.04 | 295.76 | 1% | 0.611 | 0.048 |
| 409 | Collector | 8 | 176.87 | 0.30% | 3.04 | 295.71 | 1% | 0.611 | 0.048 |
| 410 | Collector | 8 | 257.18 | 0.30% | 3.04 | 295.81 | 1% | 0.611 | 0.048 |
| 411 | Collector | 8 | 198.79 | 0.30% | 6.09 | 295.76 | 2% | 0.754 | 0.066 |
| 412 | Collector | 8 | 716.15 | 0.30% | 42.70 | 315.07 | 14% | 1.405 | 0.166 |
| 413 | Collector | 8 | 283.99 | 0.30% | 42.70 | 312.36 | 14% | 1.396 | 0.167 |
| 414 | Collector | 8 | 173.95 | 0.30% | 38.13 | 312.38 | 12% | 1.351 | 0.157 |
| 417 | Collector | 8 | 206.45 | 0.30% | 38.13 | 312.78 | 12% | 1.352 | 0.157 |
| 420 | Collector | 8 | 80.14 | 1.10% | 7.52 | 560.71 | 1% | 1.256 | 0.054 |

MODEL SCENARIO 2B
SEWER SYSTEM MODEL OUTPUT

2038 DESIGN FLOW WITH THE EXISTING SYSTEM - PEAKING FACTOR OF 4.0 (COLLECTOR)

| Pipe # | Collector/ Interceptor | Diameter (in) | Length (ft) | Slope | Flow (gpm) | Full Flow (gpm) | % of Capacity | Velocity (ft/s) | Water Depth (ft) |
|--------|---------------------------|------------------|----------------|-------|---------------|--------------------|------------------|--------------------|------------------------|
| 421 | Collector | 8 | 105.40 | 0.30% | 7.52 | 312.47 | 2% | 0.835 | 0.071 |
| 423 | Collector | 8 | 375.25 | 0.30% | 7.52 | 312.35 | 2% | 0.835 | 0.071 |
| 424 | Collector | 8 | 78.92 | 2.40% | 9.02 | 836.63 | 1% | 1.754 | 0.049 |
| 425 | Collector | 8 | 16.04 | 1.00% | 0.00 | 544.78 | 0% | 0.000 | 0.000 |
| 426 | Collector | 8 | 9.39 | 0.30% | 0.00 | 312.42 | 0% | 0.000 | 0.000 |
| 428 | Collector | 8 | 184.84 | 0.30% | 0.00 | 312.40 | 0% | 0.000 | 0.000 |
| 430 | Collector | 8 | 200.50 | 0.30% | 6.10 | 312.47 | 2% | 0.784 | 0.065 |
| 431 | Collector | 8 | 296.82 | 0.30% | 6.10 | 297.78 | 2% | 0.758 | 0.066 |
| 433 | Collector | 8 | 54.28 | 0.30% | 180.08 | 312.28 | 58% | 2.064 | 0.363 |
| 443 | Collector | 8 | 1195.13 | 0.30% | 49.18 | 312.39 | 16% | 1.454 | 0.179 |
| 447 | Interceptor | 10 | 68.26 | 0.20% | 399.79 | 484.75 | 83% | 2.212 | 0.577 |
| 449 | Interceptor | 10 | 5.00 | 0.40% | 399.79 | 623.59 | 64% | 2.704 | 0.485 |
| 465 | Collector | 8 | 491.49 | 0.30% | 0.00 | 312.40 | 0% | 0.000 | 0.000 |
| 467 | Collector | 8 | 157.24 | 0.30% | 0.00 | 312.42 | 0% | 0.000 | 0.000 |
| 471 | Collector | 8 | 280.67 | 0.30% | 0.00 | 312.36 | 0% | 0.000 | 0.000 |
| 479 | Collector | 8 | 194.19 | 0.30% | 0.00 | 312.43 | 0% | 0.000 | 0.000 |
| 495 | Collector | 8 | 117.78 | 0.80% | 4.22 | 483.21 | 1% | 0.950 | 0.044 |
| 501 | Well Connection | 10 | 5.00 | 0.90% | 601.30 | 935.39 | 64% | 4.058 | 0.486 |
| 515 | Interceptor | 36 | 10.00 | 0.00% | 814.20 | 949.21 | 86% | 0.336 | 2.140 |
| 517 | Interceptor | 36 | 10.00 | 0.00% | 399.79 | 949.21 | 42% | 0.286 | 1.358 |
| 519 | Collector | 8 | 653.89 | 0.10% | 12.90 | 207.93 | 6% | 0.737 | 0.113 |
| 521 | Collector | 8 | 306.32 | 0.50% | 5.03 | 368.69 | 1% | 0.830 | 0.054 |

APPENDIX C:

Engineer's Opinion of Probable Cost

SUNRISE ENGINEERING, INC.
CONSULTING ENGINEERS AND SURVEYORS
Opinion of Probable Costs



Project: Delta WW Masterplan OPC

By: JR
Date: Mar-19

| ITEM NO. | ITEM | QUANTITY | UNIT | UNIT PRICE | TOTAL |
|---|--|----------|---------|---------------|--------------|
| 1 | MOBILIZATION (5%) | 1 | LS | \$ 810,000.00 | \$ 810,000 |
| NEW GRAVITY MAIN - STATION A TO STATION F | | | | | |
| 2 | 10" (ASTM 3034) PVC Sewer Pipe & Fittings (Station A to Station F) | 1,670 | Ln. Ft. | \$ 43.00 | \$ 71,810 |
| 3 | Import Pipe Bedding | 1,670 | Ln. Ft. | \$ 1.00 | \$ 1,670 |
| 4 | Service Connections | 15 | EA | \$ 800.00 | \$ 12,000 |
| 5 | Replace Laterals to Property Line - 4" Sewer Pipe | 750 | Ln. Ft. | \$ 32.00 | \$ 24,000 |
| 6 | Cleanout | 15 | EA | \$ 300.00 | \$ 4,500 |
| 7 | New Manholes | 5 | EA | \$ 4,500.00 | \$ 22,500 |
| 8 | Pavement Sawcut/Rotomill Exist Pavement | 900 | Ln. Ft. | \$ 2.00 | \$ 1,800 |
| 9 | Import UBC | 200 | CY | \$ 35.00 | \$ 7,000 |
| 10 | 3" HMA Surfacing | 1,000 | SY | \$ 30.00 | \$ 30,000 |
| 11 | Decommission & Demo Station A | 1 | LS | \$ 40,000.00 | \$ 40,000 |
| Subtotal - New Gravity Main from Station A to Station F | | | | | \$ 215,280 |
| LIFT STATION F UPGRADES | | | | | |
| 12 | Replace Primary Wet Well | 1 | LS | \$ 25,000.00 | \$ 25,000 |
| 13 | Install Backup Wet Well | 1 | Ln. Ft. | \$ 15,000.00 | \$ 15,000 |
| 14 | Install Duplex Primary Pumps & Controls (Assume 20 HP Pumps) | 1 | LS | \$ 100,000.00 | \$ 100,000 |
| 15 | Install Backup Simplex Pump & Controls (Assume 20 HP Pump) | 1 | LS | \$ 50,000.00 | \$ 50,000 |
| 16 | Instrumentation & Controls | 1 | LS | \$ 20,000.00 | \$ 20,000 |
| 17 | Lift Station Piping & Valves | 1 | LS | \$ 25,000.00 | \$ 25,000 |
| 18 | New Backup Generator w/Enclosure | 1 | LS | \$ 50,000.00 | \$ 50,000 |
| 19 | Demo Station A | 1 | LS | \$ 20,000.00 | \$ 20,000 |
| Subtotal - Lift Station F Upgrades | | | | | \$ 305,000 |
| NEW FORCE MAIN FROM STATION F TO STATION B | | | | | |
| 20 | 12" AWWA C900 PVC Force Main | 5,000 | Ln. Ft. | \$ 36.00 | \$ 180,000 |
| 21 | Pipe Bedding | 5,000 | Ln. Ft. | \$ 1.00 | \$ 5,000 |
| 22 | 2" Combination Air Valve Assemblies | 4 | EA | \$ 4,500.00 | \$ 18,000 |
| 23 | 12" Plug Valves | 4 | EA | \$ 5,000.00 | \$ 20,000 |
| Subtotal - New Force Main, Station F to Station B | | | | | \$ 223,000 |
| SEWER REPLACEMENT - ZONE A | | | | | |
| 24 | 8" (ASTM 3034) PVC Sewer Pipe & Fittings | 29,690 | Ln. Ft. | \$ 36.00 | \$ 1,068,840 |
| 25 | 10" (ASTM 3034) PVC Sewer Pipe & Fittings | 8,457 | Ln. Ft. | \$ 43.00 | \$ 363,651 |
| 26 | 12" (ASTM 3034) PVC Sewer Pipe & Fittings | 5,015 | Ln. Ft. | \$ 50.00 | \$ 250,750 |
| 27 | Import Pipe Bedding | 43,162 | Ln. Ft. | \$ 1.00 | \$ 43,162 |
| 28 | Service Connections | 531 | EA | \$ 800.00 | \$ 424,800 |
| 29 | Replace Laterals to Property Line - 4" Sewer Pipe | 26,550 | Ln. Ft. | \$ 32.00 | \$ 849,600 |
| 30 | Cleanout | 531 | EA | \$ 300.00 | \$ 159,300 |
| 31 | New Manholes | 102 | EA | \$ 4,500.00 | \$ 459,000 |
| 32 | Pavement Sawcut/Rotomill Exist Pavement | 43,162 | Ln. Ft. | \$ 2.00 | \$ 86,324 |
| 33 | Import UBC | 9,500 | CY | \$ 35.00 | \$ 332,500 |
| 34 | 3" HMA Surfacing | 50,000 | SY | \$ 30.00 | \$ 1,500,000 |
| 35 | Import Granular Borrow (UDOT) | 7,000 | CY | \$ 25.00 | \$ 175,000 |
| 36 | 8" HMA Surfacing (UDOT) | 4,000 | SY | \$ 50.00 | \$ 200,000 |
| 37 | Flowable Fill (UDOT Crossings & Services) | 1,500 | CY | \$ 110.00 | \$ 165,000 |
| 38 | 2" Mill & Overlay | 9,000 | SY | \$ 25.00 | \$ 225,000 |
| Subtotal 2 - Sewer Replacement for Zone A | | | | | \$ 6,302,927 |
| NEW FORCE MAIN FROM STATION B TO LAGOONS | | | | | |
| 39 | 12" AWWA C900 PVC Force Main | 8,300 | Ln. Ft. | \$ 36.00 | \$ 298,800 |
| 40 | Pipe Bedding | 8,300 | Ln. Ft. | \$ 1.00 | \$ 8,300 |
| 41 | 2" Combination Air Valve Assemblies | 4 | EA | \$ 4,500.00 | \$ 18,000 |
| 42 | 12" Plug Valves | 4 | EA | \$ 5,000.00 | \$ 20,000 |
| Subtotal - New Force Main for Station B to Lagoons | | | | | \$ 345,100 |
| LIFT STATION C UPGRADES | | | | | |
| 43 | Replace Primary Wet Well | 1 | LS | \$ 20,000.00 | \$ 20,000 |

APPENDIX D:

Sample Financing Plans

Delta City Proposed WW Improvements Recommended System Improvements

March-19

Total Project Cost **\$ 18,882,336.00**

Proposed Funding:

| | % of Project | |
|--------------------|--------------|---------------|
| Self Participation | 0% | - |
| DWQ Loan | 0% | - |
| DWQ Grant | 0% | - |
| CIB Loan | 0% | - |
| CIB Grant | 0% | - |
| USDA RD Loan | 55% | 10,385,284.80 |
| USDA RD Grant | 45% | 8,497,051.20 |
| | 100% | |

Total Project Funding **\$ 18,882,336.00**

Annual Expenses: (Projected)

| | |
|--|------------|
| 2017 Expenses Less Depreciation (See Attached Expense Sheet) | 272,827.00 |
| Total Operation and Maintenance | 272,827.00 |

Existing Debt Service:

| | |
|-----------------------------|---|
| None Known | - |
| Total Existing Debt Service | - |

New Debt Service:

| | | |
|----------------------------------|---|--------------|
| DDW Loan | | |
| CIB Loan | - | \$0.00 |
| USDA RD Loan | (2.75% for 40 Yrs; Loan Amount: 10,385,284.80 | \$431,316.59 |
| 10% Debt Reserve | | \$43,131.66 |
| Total Estimated New Debt Service | | \$474,448.25 |

Total Annual Income Required **\$747,275.25**

Annual Income:

| | | |
|---|-----------|--------------|
| Total Number of Active ERC's Billed | | 1,206 |
| Total Annual Income Required | | 747,275.25 |
| Total Annual Income Required w/ 1.25% debt service coverage | | 865,887.31 |
| Average Monthly Sewer User Rate | \$ | 59.83 |
| Average Monthly Overages | | |
| Average Monthly Total Sewer User Rate | \$ | 59.83 |
| Median Adjusted Gross Income (2017 MAGI) | | 43,944.00 |
| 1.40% of MAGI Per Month | \$ | 51.27 |
| % of MAGI Per Month Projected | | 1.63% |

Delta City Proposed WW Improvements Recommended System Improvements

March-19

Total Project Cost **\$ 18,882,336.00**

Proposed Funding:

| | % of Project | |
|--------------------|--------------|--------------|
| Self Participation | 0% | - |
| DWQ Loan | 10% | 1,888,233.60 |
| DWQ Grant | 20% | 3,776,467.20 |
| CIB Loan | 0% | - |
| CIB Grant | 0% | - |
| USDA RD Loan | 39% | 7,269,699.36 |
| USDA RD Grant | 32% | 5,947,935.84 |
| USACE Grant | 0% | - |
| | 100% | |

Total Project Funding **\$ 18,882,336.00**

Annual Expenses: (Projected)

2017 Expenses Less Depreciation (See Attached Expense Sheet) 272,827.00

Total Operation and Maintenance 272,827.00

Existing Debt Service:

None Known -

Total Existing Debt Service -

New Debt Service:

| | | |
|--|--------------|--------------|
| DWQ Loan | 1,888,233.60 | \$73,165.46 |
| CIB Loan | - | \$0.00 |
| USDA RD Loan (2.75% for 40 Yrs; Loan Amount: | 7,269,699.36 | \$301,921.61 |
| 10% Debt Reserve | | \$37,508.71 |

Total Estimated New Debt Service \$412,595.78

Total Annual Income Required **\$685,422.78**

Annual Income:

| | | |
|---|-----------|--------------|
| Total Number of Active ERC's Billed | | 1,206 |
| Total Annual Income Required | | 685,422.78 |
| Total Annual Income Required w/ 1.25% debt service coverage | | 788,571.72 |
| Average Monthly Sewer User Rate | \$ | 54.49 |
| Average Monthly Overages | | |
| Average Monthly Total Sewer User Rate | \$ | 54.49 |

Median Adjusted Gross Income (2017 MAGI) 43,944.00

1.40% of MAGI Per Month **\$ 51.27**

% of MAGI Per Month Projected 1.49%